| MEASURAND : | AC Voltage ratio |
| :--- | :--- |
| NOMINAL VALUES : | Ten decimal ratio values : 0.01, and 0.1 to 0.9 by step of $0.1 ;$ |
|  | Ten elevenths ratio values : $1 / 11$ to $10 / 11$ by step of $1 / 11$ |
| FREQUENCY: | 1 kHz |

The measurements of this key comparison were made of twenty AC voltage ratios at two possible frequencies: 1 kHz and 55 Hz . The in-phase and quadrature components of each voltage ratio were reported separately giving a total of 80 possible measurement results for each participant. The 1 kHz measurements were compulsory and all the 17 participating laboratories made these measurements. The 55 Hz measurements were optional, with 7 laboratories contributing.

The measurement results reported by the laboratories participating in CCEM-K7 can be found in section 4 on page 188 of the Final Report, Part 2.

| Lab i | Year of <br> measurement |
| :--- | :---: |
|  |  |
| NMIJ | 2000 |
| CEM | 2003 |
| NMIA | 2001 |
| INRIM | 2002 |
| KRISS | 2002 |
| LNE | 2002 |
| METAS | 2000 |
| NIM | 2001 |
| NIST | 2003 |
| NPL | 2003 |
| NPLI | 2001 |
| NRC | 2003 |
| PTB | 2000 |
| SP | 2001 |
| UME | 2002 |
| VNIIM | 2002 |
| VSL | 1999 |

## AC Voltage ratio

NOMINAL VALUES: Ten decimal ratio values : 0.01 , and 0.1 to 0.9 by step of 0.1 ;
Ten elevenths ratio values : 1/11 to 10/11 by step of 1/11

## FREQUENCY:

1 kHz

For the in phase and the quadrature components of each voltage ratio, the key comparison reference value, $x_{R}$, is calculated as the weighted mean of the particapants' results after exclusion of outliers. Its expanded uncertainty $(k=2), U_{R}$, is calculated as explained in section 1.3 of the Final Report, Part 2.

|  | In phase |  | Quadrature |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $X_{\mathrm{R}}$ | $U_{\mathrm{R}}$ | $X_{\mathrm{R}}$ | $U_{\mathrm{R}}$ |
|  | $I(\mathrm{nV} / \mathrm{V})$ | $I(\mathrm{nV} / \mathrm{V})$ | $I(\mathrm{nV} / \mathrm{V})$ | $I(\mathrm{nV} / \mathrm{V})$ |
|  | 58.3 | 5.1 | -71.6 | 3.9 |
| 0.8 | 71.5 | 5.3 | -110.2 | 4.1 |
| 0.7 | 64.0 | 5.8 | -137.0 | 4.5 |
| 0.6 | 39.0 | 5.7 | -132.5 | 4.4 |
| 0.5 | 9.8 | 5.4 | -130.3 | 4.5 |
| 0.4 | -22.9 | 5.4 | -97.0 | 4.4 |
| 0.3 | -38.6 | 5.1 | -51.0 | 4.3 |
| 0.2 | -45.9 | 5.1 | -15.4 | 4.1 |
| 0.1 | -43.6 | 4.8 | 8.9 | 3.5 |
| 0.01 | -1160.5 | 8.4 | 422.5 | 5.0 |
| $10 / 11$ | 53.2 | 5.1 | -123.5 | 3.9 |
| $9 / 11$ | 21.8 | 5.2 | -176.9 | 4.1 |
| $8 / 11$ | 9.4 | 5.3 | -200.9 | 4.0 |
| $7 / 11$ | -6.2 | 5.3 | -186.6 | 4.5 |
| $6 / 11$ | -17.1 | 5.3 | -156.5 | 4.3 |
| $5 / 11$ | -2.2 | 5.4 | -124.9 | 4.6 |
| $4 / 11$ | -31.1 | 5.4 | -46.8 | 4.3 |
| $3 / 11$ | -24.5 | 5.3 | -1.6 | 4.1 |
| $2 / 11$ | -46.2 | 5.1 | 48.9 | 4.1 |
| $1 / 11$ | -49.7 | 5.0 | 59.6 | 3.7 |

For the in phase and the quadrature components of each voltage ratio, the degree of equivalence of each laboratory with respect to the key comparison reference value is given by a pair of terms:
$D_{i}$ and $U_{i}$, its expanded uncertainty $(k=2)$, both expressed in $\mathrm{nV} / \mathrm{V}$.
The degree of equivalence between two laboratories is given by a pair of terms: $D_{i j}$ and $U_{i j}$, its expanded uncertainty $(k=2)$, both expressed in nV/V, and can be found in section 3 of the Final Report, Part 2.

The BIPM key comparison database, June 2012

MEASURAND : AC Voltage ratio
NOMINAL VALUES : Ten decimal ratio values : 0.01 , and 0.1 to 0.9 by step of 0.1 ; Ten elevenths ratio values : 1/11 to 10/11 by step of $1 / 11$
FREQUENCY: 1 kHz

Table of Degrees of equivalence

| Voltage ratio <br> Lab i | 0.9 |  |  |  | 0.8 |  |  |  | 0.7 |  |  |  | 0.6 |  |  |  | 0.5 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  |
|  | $\begin{array}{cc} \hline D_{i} & U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \end{array}$ |  | $\begin{array}{cc} D_{i} & U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \\ \hline \end{array}$ |  | $\begin{array}{cc} \hline D_{i} & U_{i} \\ I(n \mathrm{n} / \mathrm{V}) \\ \hline \end{array}$ |  | $\begin{array}{cc} \hline D_{i} & U_{i} \\ I(n \mathrm{~V} / \mathrm{V}) \\ \hline \end{array}$ |  | $\begin{array}{cc} \hline D_{i} & U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \\ \hline \end{array}$ |  | $\begin{array}{cc} \hline D_{i} & U_{i} \\ I(n \mathrm{~V} / \mathrm{V}) \\ \hline \end{array}$ |  | $\begin{array}{cc} \hline D_{i} & U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \\ \hline \end{array}$ |  | $\begin{array}{cc} D_{i} & U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \\ \hline \end{array}$ |  | $\begin{array}{cc} D_{i} & U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \end{array}$ |  | $\begin{array}{cc} D_{i} & U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \\ \hline \end{array}$ |  |
| NMIJ | 21 | 14 | -3 | 31 | 21 | 14 | -8 | 29 | 22 | 15 | -11 | 27 | 16 | 13 | -13 | 24 | 7 | 13 | -13 | 21 |
| CEM | -13 | 51 | 4 | 48 | -27 | 51 | 6 | 48 | -31 | 51 | 8 | 48 | -35 | 51 | 10 | 48 | -35 | 51 | 13 | 48 |
| NMIA | -0.3 | 11.7 | 2.6 | 3.5 | -4.5 | 11.7 | 3.2 | 3.2 | -1.0 | 11.4 | 4.0 | 2.5 | 0.0 | 11.5 | 1.5 | 2.7 | 2.2 | 11.6 | 0.3 | 2.6 |
| INRIM | 6 | 16 | 7 | 10 | 4 | 18 | 6 | 10 | -2 | 17 | 25 | 13 | -6 | 16 | 11 | 14 | -6 | 14 | 10 | 14 |
| KRISS | 10 | 20 | -1 | 24 | 8 | 20 | -3 | 24 | 10 | 20 | -4 | 24 | 7 | 20 | -7 | 24 | 3 | 20 | -6 | 24 |
| LNE | 88 | 29 | -8316 | 26 | 136 | 31 | -12067 | 29 | 168 | 35 | -11028 | 33 | 179 | 37 | -7593 | 35 | 75 | 38 | -3293 | 36 |
| METAS | 2 | 28 | 4 | 68 | -4 | 35 | 7 | 108 | -2 | 35 | 10 | 128 | -5 | 33 | 10 | 129 | -7 | 30 | 12 | 123 |
| NIM | -3 | 12 | -6 | 9 | -9 | 14 | -12 | 16 | -4 | 14 | -19 | 20 | 4 | 14 | -22 | 20 | 0 | 12 | -28 | 16 |
| NIST | 10 | 44 | 3 | 100 | 11 | 43 | 6 | 100 | 15 | 44 | 7 | 100 | 15 | 44 | 7 | 120 | 6 | 45 | 4 | 110 |
| NPL | 1 | 27 | -12 | 25 | -4 | 27 | -19 | 25 | -2 | 27 | -25 | 25 | -2 | 27 | -30 | 25 | 0 | 27 | -30 | 25 |
| NPLI | -12 | 13 | -3098 | 300 | 6 | 13 | -6210 | 300 | 23 | 12 | -7753 | 300 | 30 | 12 | -8728 | 300 | 33 | 13 | -9080 | 300 |
| NRC | -9 | 31 | -23 | 29 | -21 | 31 | -41 | 29 | -22 | 31 | -51 | 29 | -24 | 31 | -57 | 29 | -23 | 31 | -56 | 29 |
| PTB | -7 | 23 | -11 | 20 | -17 | 23 | -19 | 20 | -17 | 23 | -26 | 20 | -19 | 23 | -31 | 20 | -18 | 23 | -31 | 20 |
| SP | -4 | 49 | 5 | 71 | -7 | 49 | -5 | 71 | -17 | 49 | -8 | 71 | -15 | 49 | -1 | 71 | 1 | 49 | 10 | 71 |
| UME | -13 | 50 | -14 | 59 | -22 | 50 | -20 | 59 | -19 | 50 | -23 | 59 | -14 | 50 | -22 | 59 | -11 | 50 | -22 | 59 |
| VNIIM | 3 | 21 | 6 | 28 | -1 | 21 | 11 | 28 | 1 | 21 | 15 | 28 | 0 | 21 | 18 | 28 | -2 | 21 | 20 | 28 |
| VSL | -12 | 21 | -128 | 110 | -17 | 27 | -240 | 150 | -12 | 32 | -333 | 180 | -10 | 37 | -388 | 210 | -8 | 43 | -390 | 230 |

MEASURAND : AC Voltage ratio
NOMINAL VALUES: Ten decimal ratio values : 0.01 , and 0.1 to 0.9 by step of 0.1 ; Ten elevenths ratio values : $1 / 11$ to $10 / 11$ by step of $1 / 11$ FREQUENCY: 1 kHz

Table of Degrees of equivalence

| Voltage ratio <br> Lab i | 0.4 |  |  |  | 0.3 |  |  |  | 0.2 |  |  |  | 0.1 |  |  |  | 0.01 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  |
|  |  | $\mathrm{U}_{i}$ | $l(\mathrm{nV} / \mathrm{V})$ |  | $l(\mathrm{nV} / \mathrm{V})$ |  | 1 (nV/V) | $\mathrm{U}_{\mathbf{i}}$ | $D_{i}$ $I$ I | $U_{i}$ | 1 (nV/V) |  |  | $\mathrm{U}_{i}$ | $l$ ( $\mathrm{nV} / \mathrm{V}$ ) |  | $I$ (nV/V) |  | $I$ (nV/V) |  |
| NMIJ | 1 | 12 | -9 | 19 | -7 | 12 | -7 | 16 | -7 | 12 | -4 | 13 | -7 | 12 | 3 | 9 | -76 | 79 | 65 | 160 |
| CEM | -32 | 51 | 18 | 48 | -30 | 51 | 20 | 48 | -20 | 51 | 19 | 48 | -12 | 51 | 16 | 48 | -12 | 49 | -9 | 50 |
| NMIA | 3.9 | 11.6 | 2.0 | 2.8 | 0.6 | 11.7 | 0.0 | 2.9 | 0.9 | 11.7 | 0.4 | 3.2 | -0.4 | 11.9 | 3.1 | 3.9 | 2.5 | 9.7 | 0.5 | 1.5 |
| INRIM | -1 | 13 | 4 | 15 | -6 | 14 | 15 | 12 | -3 | 14 | 10 | 11 | 7 | 14 | -10 | 8 | -78 | 80 | 150 | 51 |
| KRISS | 2 | 20 | -4 | 24 | -2 | 20 | -6 | 24 | -1 | 20 | -6 | 24 | -2 | 20 | -1 | 24 | -38 | 22 | 20 | 30 |
| LNE | -58 | 37 | 2176 | 35 | -135 | 35 | 7460 | 33 | -91 | 31 | 9880 | 29 | 11 | 29 | 7879 | 26 | 2428 | 15 | 527 | 11 |
| METAS | -5 | 29 | 15 | 129 | -9 | 27 | 14 | 128 | -6 | 24 | 12 | 108 | -5 | 19 | 11 | 68 | -78 | 65 | 68 | 85 |
| NIM | 16 | 14 | -26 | 12 | 12 | 14 | -29 | 9 | 3 | 17 | -20 | 9 | 1 | 13 | -1 | 9 | 8 | 13 | -60 | 8 |
| NIST | 12 | 45 | 12 | 110 | 6 | 46 | 12 | 110 | 5 | 45 | 12 | 100 | 3 | 44 | 14 | 100 | -57 | 500 | 71 | 500 |
| NPL | 3 | 27 | -26 | 25 | -1 | 27 | -22 | 25 | 1 | 27 | -15 | 25 | 0 | 27 | -5 | 25 | 33 | 50 | -11 | 49 |
| NPLI | 32 | 13 | -8333 | 300 | 21 | 13 | -6989 | 300 | 18 | 13 | -5315 | 300 | 10 | 13 | -2599 | 300 | -54 | 11 | 3488 | 300 |
| NRC | -21 | 31 | -48 | 29 | -21 | 31 | -40 | 29 | -15 | 31 | -27 | 29 | -9 | 31 | -10 | 29 | 2329 | 61 | -861 | 60 |
| PTB | -13 | 23 | -25 | 20 | -13 | 23 | -22 | 20 | -8 | 23 | -14 | 20 | -6 | 23 | -4 | 20 | -1 | 51 | -49 | 100 |
| SP | 10 | 49 | 11 | 71 | 2 | 49 | 17 | 71 | 1 | 49 | 6 | 71 | -3 | 49 | 9 | 71 | -18 | 49 | -38 | 71 |
| UME | -3 | 50 | -12 | 59 | -4 | 50 | -11 | 59 | 2 | 50 | -1 | 59 | 1 | 50 | 4 | 59 | 14 | 88 | -1094 | 88 |
| VNIIM | -1 | 21 | 23 | 28 | -7 | 21 | 18 | 28 | -5 | 21 | 21 | 28 | -4 | 22 | 11 | 28 | -4 | 24 | -36 | 33 |
| VSL | -2 | 37 | -343 | 210 | -2 | 32 | -259 | 180 | 2 | 27 | -165 | 150 | 2 | 21 | -79 | 110 | -86 | 43 | -2 | 260 |






















MEASURAND : AC Voltage ratio
NOMINAL VALUES : Ten decimal ratio values : 0.01 , and 0.1 to 0.9 by step of 0.1 ; Ten elevenths ratio values : 1/11 to 10/11 by step of $1 / 11$
FREQUENCY: 1 kHz

Table of Degrees of equivalence

| Voltage ratio <br> Lab i | 10/11 |  |  |  | 9/11 |  |  |  | 8/11 |  |  |  | $7 / 11$ |  |  |  | 6/11 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  |
|  | 1 (nV/V) | $\mathrm{U}_{i}$ | $l(\mathrm{nV} / \mathrm{V})$ |  | $l(\mathrm{nV} / \mathrm{V})$ |  | 1 (nV/V) |  | 1 (nV/V) |  | 1 (nV/V) |  | $l(\mathrm{nV} / \mathrm{V})$ |  | 1 (nV/V) |  | $l(\mathrm{nV} / \mathrm{V})$ |  | $\begin{gathered} D_{i} \quad U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \end{gathered}$ |  |
| NMIJ | 11 | 14 | -9 | 32 | 6 | 14 | -11 | 29 | 2 | 14 | -17 | 27 | -2 | 13 | -14 | 25 | 0 | 13 | -16 | 23 |
| CEM | -2 | 51 | 10 | 48 | -20 | 51 | 20 | 48 | -17 | 51 | 25 | 48 | -30 | 51 | 36 | 48 | -28 | 51 | 38 | 48 |
| NMIA | -0.2 | 11.7 | 2.5 | 3.5 | 1.0 | 11.7 | 1.9 | 3.1 | 0.4 | 11.6 | -1.1 | 3.3 | -2.2 | 11.6 | 1.6 | 2.7 | -1.4 | 11.6 | 0.5 | 2.9 |
| INRIM | 5 | 14 | -3 | 8 | 3 | 13 | 1 | 10 | 2 | 14 | 4 | 12 | 11 | 14 | -22 | 13 | -1 | 13 | 11 | 13 |
| KRISS | 6 | 21 | -6 | 24 | 3 | 21 | -14 | 24 | 2 | 21 | -25 | 24 | -2 | 21 | -31 | 24 | -2 | 21 | -35 | 24 |
| LNE | 109 | 33 | -9902 | 690 | 262 | 36 | -14320 | 690 | 323 | 39 | -14532 | 690 | 304 | 41 | -12227 | 690 | 193 | 42 | -8656 | 690 |
| METAS | 5 | 18 | 0 | 50 | 2 | 22 | 3 | 74 | 0 | 27 | 3 | 103 | -3 | 29 | 10 | 114 | -2 | 30 | 9 | 124 |
| NIM | 7 | 14 | 8 | 12 | 12 | 14 | 8 | 16 | 11 | 14 | 9 | 9 | 17 | 14 | 4 | 12 | 16 | 14 | -8 | 12 |
| NIST | 3 | 63 | 9 | 120 | 7 | 65 | 18 | 130 | 8 | 67 | 20 | 130 | 8 | 68 | 25 | 130 | 10 | 69 | 21 | 130 |
| NPL | 1 | 27 | -10 | 25 | 1 | 27 | -17 | 25 | 0 | 27 | -24 | 25 | -3 | 27 | -24 | 25 | -2 | 27 | -27 | 25 |
| NPLI | -27 | 15 | -3496 | 500 | -15 | 15 | -6313 | 500 | -5 | 15 | -8249 | 500 | 2 | 15 | -9553 | 500 | 11 | 15 | -10164 | 500 |
| NRC | -9 | 40 | -33 | 38 | -20 | 40 | -56 | 38 | -27 | 40 | -74 | 38 | -33 | 40 | -78 | 38 | -33 | 40 | -82 | 38 |
| PTB | -2 | 23 | -13 | 20 | -5 | 23 | -22 | 20 | -7 | 23 | -31 | 20 | -11 | 23 | -31 | 20 | -8 | 23 | -35 | 20 |
| SP | -4 | 49 | -1 | 71 | -1 | 49 | -10 | 71 | -13 | 49 | 0 | 71 | -7 | 49 | 1 | 71 | -13 | 49 | 6 | 71 |
| UME | -10 | 50 | -21 | 59 | -15 | 50 | -28 | 59 | -18 | 50 | -34 | 59 | -20 | 50 | -29 | 59 | -19 | 50 | -28 | 59 |
| VNIIM | 0 | 21 | 9 | 28 | -2 | 21 | 15 | 28 | -3 | 21 | 15 | 28 | -9 | 21 | 20 | 28 | -8 | 21 | 17 | 28 |
| VSL | 2 | 21 | -86 | 120 | -10 | 27 | -203 | 160 | -11 | 32 | -339 | 190 | -20 | 37 | -453 | 210 | -17 | 42 | -514 | 230 |

MEASURAND : AC Voltage ratio
NOMINAL VALUES: Ten decimal ratio values : 0.01 , and 0.1 to 0.9 by step of 0.1 ; Ten elevenths ratio values : $1 / 11$ to $10 / 11$ by step of $1 / 11$ FREQUENCY: 1 kHz

Table of Degrees of equivalence

| Voltage ratio <br> Lab i | 5/11 |  |  |  | 4/11 |  |  |  | 3/11 |  |  |  | 2/11 |  |  |  | 1/11 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  | In phase |  | Quadrature |  |
|  | $l$ (nV/V) |  | $l(\mathrm{nV} / \mathrm{V})$ |  | $l(\mathrm{nV} / \mathrm{V})$ |  | $l(\mathrm{nV} / \mathrm{V})$ |  | $l(\mathrm{nV} / \mathrm{V})$ |  | $l(\mathrm{nV} / \mathrm{V})$ |  | $\begin{array}{cc} D_{i} \quad U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \end{array}$ |  | $\begin{array}{cc} \hline D_{i} & U_{i} \\ I(n \mathrm{~V} / \mathrm{V}) \\ \hline \end{array}$ |  | $\begin{array}{cc} \hline D_{i} & U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \\ \hline \end{array}$ |  | $\begin{array}{cc} \hline D_{i} \quad U_{i} \\ I(\mathrm{nV} / \mathrm{V}) \\ \hline \end{array}$ |  |
| NMIJ | 3 | 13 | -16 | 21 | 2 | 12 | -8 | 18 | 3 | 12 | -5 | 15 | 1 | 12 | -2 | 12 | 0 | 12 | 4 | 9 |
| CEM | -32 | 51 | 38 | 48 | -31 | 51 | 41 | 50 | -29 | 51 | 37 | 50 | -23 | 51 | 29 | 50 | -14 | 51 | 20 | 50 |
| NMIA | -3.4 | 11.6 | 0.9 | 2.5 | -2.5 | 11.6 | 2.8 | 3.0 | -4.2 | 11.7 | 3.6 | 3.2 | -1.6 | 11.7 | 1.1 | 3.2 | -0.2 | 11.8 | 2.4 | 3.7 |
| INRIM | 5 | 16 | 2 | 13 | 3 | 16 | 7 | 13 | 6 | 16 | 6 | 13 | 0 | 13 | 7 | 11 | 11 | 15 | -13 | 13 |
| KRISS | -4 | 21 | -34 | 24 | -4 | 21 | -19 | 24 | -3 | 21 | -6 | 24 | -2 | 21 | 4 | 24 | -1 | 22 | 2 | 24 |
| LNE | -33 | 42 | -4087 | 690 | -132 | 41 | 1000 | 690 | -238 | 39 | 5338 | 690 | -170 | 36 | 7062 | 690 | -62 | 37 | 4893 | 35 |
| METAS | -3 | 31 | 9 | 137 | -5 | 33 | 14 | 146 | -5 | 31 | 13 | 138 | -6 | 27 | 9 | 113 | -4 | 21 | 9 | 71 |
| NIM | 15 | 14 | -30 | 20 | 16 | 14 | -7 | 20 | 14 | 12 | -8 | 12 | 15 | 12 | -25 | 12 | 10 | 12 | -4 | 9 |
| NIST | 8 | 69 | 19 | 130 | 7 | 69 | 17 | 130 | 6 | 67 | 14 | 130 | 5 | 65 | 6 | 120 | 5 | 63 | 6 | 120 |
| NPL | -3 | 27 | -26 | 25 | -4 | 27 | -22 | 25 | -4 | 27 | -17 | 25 | -3 | 27 | -14 | 25 | -1 | 27 | -6 | 25 |
| NPLI | 12 | 15 | -9485 | 500 | 7 | 15 | -8323 | 500 | 7 | 15 | -6918 | 500 | 6 | 15 | -4519 | 500 | 6 | 15 | -2260 | 500 |
| NRC | -32 | 40 | -77 | 38 | -29 | 40 | -65 | 38 | -25 | 40 | -51 | 38 | -17 | 40 | -37 | 38 | -9 | 40 | -16 | 38 |
| PTB | -9 | 23 | -31 | 20 | -12 | 23 | -26 | 20 | -13 | 23 | -20 | 20 | -13 | 23 | -17 | 20 | -9 | 23 | -7 | 20 |
| SP | -9 | 49 | -10 | 71 | -13 | 49 | -7 | 71 | -10 | 49 | -24 | 71 | -5 | 49 | -27 | 71 | -10 | 49 | -23 | 71 |
| UME | -18 | 50 | -22 | 59 | -18 | 50 | -13 | 59 | -15 | 50 | -5 | 59 | -12 | 50 | -1 | 59 | -5 | 50 | 6 | 59 |
| VNIIM | -11 | 21 | 19 | 28 | -14 | 21 | 16 | 28 | -13 | 21 | 14 | 28 | -12 | 21 | 4 | 28 | -5 | 22 | 2 | 28 |
| VSL | -9 | 42 | -505 | 230 | -15 | 37 | -463 | 210 | -12 | 32 | -358 | 190 | -19 | 27 | -239 | 160 | -9 | 21 | -110 | 120 |






















