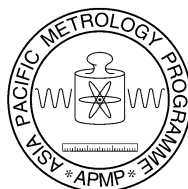


APMP reference no. APMP.EM-K6.a



**APMP International Comparison of Ac-dc Transfer  
Standards at the Lowest Attainable Level of  
Uncertainty**

**Final Report**

**Ilya Budovsky  
National Measurement Institute, Australia**

# APMP reference no. APMP.EM-K6.a

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## APMP International Comparison of Ac-dc Transfer Standards at the Lowest Attainable Level of Uncertainty

### 1. Scope

This comparison has offered the same range and frequencies as the key Comparison CCEM-K6a with the view of providing the National Metrology Institutes (NMIs) of the APMP member economies with an opportunity to link the values of their standards for ac-dc transfer difference to the international reference values. The comparison is part of the Global Mutual Recognition Arrangement (MRA) process.

### 2. Definition of the Measurand

Ac-dc transfer difference is defined as

$$\delta = \frac{U_{ac} - U_{dc}}{U_{dc}}$$

where

$U_{ac}$  is an rms ac voltage, and

$U_{dc}$  is a dc voltage which, when reversed, produces the same mean output response as the rms ac voltage.

Differences are expressed in microvolts per volt ( $\mu\text{V}/\text{V}$ ), and a positive sign signifies that more ac than dc was required for the same output response.

### 3. The Travelling Standard

The travelling standard was a Holt Model 11 Single-Junction Thermal Voltage Converter, Part Number 90081C, with the following nominal parameters:

Rated Input Voltage:	4V
Heater Resistance:	400 $\Omega$
Thermocouple Resistance:	7 $\Omega$
Output Voltage:	7 mV

The Thermal Converter was supplied with a GR type-874 adapter plate 11 Part Number 84980 and two Tee-pieces, a GR type-874 and an N-male with an N-to-GR type 874 adapter. In order to raise the confidence in the results the travelling standard had been chosen to have a relatively high magnitude of ac-dc difference (from 5  $\mu\text{V}/\text{V}$  at 1 kHz to approximately 30  $\mu\text{V}/\text{V}$  at 1 MHz). The participants were asked to measure the ac-dc difference of the travelling standard at 3 V and selected frequencies that included those of CCEM-K6a.

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## 4. Measurement Conditions

- \* The voltage was defined at the mid-point of the Tee-piece. The participants had the option of using either or both Tee-pieces or a Tee-piece of their own however, only one set of results could be reported by each participant
- \* When using the GR type 874 Tee-piece supplied with the Travelling Standard, the Thermal Converter was connected to the side of the Tee-piece marked in green.
- \* The input and output of the Travelling Standard was always earthed to protect the insulation between the heater and the thermocouple.

## 5. Test Points

The ac-dc difference of the travelling standard was measured with 3 V applied at the following frequencies:

Standard: 1 kHz, 20 kHz, 100 kHz and 1 MHz,

Optional: 50 kHz and 500 kHz.

## 6. Reports

Each participant was asked to submit a report within one month after completing the measurements. All reports have been received and contain at least the following:

- \* Detailed description of the measurement setup including a drawing that can be used, if necessary, in the final report of the Comparison;
- \* Definition of the measurand including the Tee-piece used;
- \* Detailed description of the measurement procedure;
- \* The mean value of the results, their standard deviation and the number of measurements taken to obtain the results;
- \* Complete uncertainty budget in accordance with the principles of the ISO Guide to the Expression of Uncertainty in Measurement. Individual uncertainty components, the standard uncertainty and the degrees of freedom should be included.

## 7. Participants and the Time Schedule

The list of the participants and time schedule are shown in Tables 1 and 2. Each participant was given a time slot of 6 weeks, comprising 4 weeks for measurement and 2 weeks for transportation.

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**Table 1**  
**Participants of APMP.EM-K6a**

<b>Economy</b>	<b>NMI</b>	<b>Standard, AC-DC Comparator System</b>	<b>Traceability</b>
Australia	NMIA	SJTC, fully automated dual-channel	NMIA
Malaysia	NML-SIRIM	SJTC, fully automated dual-channel	NMIA
Hong Kong	SCL	MJTC, fully-automated dual-channel	NPL
Singapore	NMC	MJTC, fully automated dual-channel	PTB
India	NPL	MJTC, semi-automated dual-channel	NPLI
Germany	PTB	MJTC, fully automated differential	PTB
Chinese Taipei	CMS	MJTC, fully automated dual-channel	PTB
New Zealand	MSL	Electronic transfer std., fully automated dual-channel	NMIA
Japan	NMIJ	SJTC, fully automated dual-channel	NMIJ
Thailand	NIMT	SJTC, fully automated dual-channel	NMIA
Korea	KRISS	MJTC, semi-automated dual-channel	PTB
Viet Nam	VMI	SJTC, fully automated dual-channel	NMIA
Indonesia	KIM-LIPI	SJTC, fully automated dual-channel	NMIA
South Africa	NMISA	MJTC, fully automated dual-channel	PTB
Philippines	ITDI	SJTC, fully automated dual-channel	NMIA

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**Table 2**  
**Comparison Schedule**

<b>Economy</b>	<b>Laboratory</b>	<b>Period of Measurement</b>	<b>Responsible Person</b>	<b>e-mail Address</b>
Australia	NMIA		Ilya Budovsky	Ilya.Budovsky@nmi.gov.au
Malaysia	NML-SIRIM	15/11/2000-31/12/2000	Abdul Rashid Bin Zainal Abidin	abd.rashid_z.abidin@sirim.my
Hong Kong	SCL	1/1/2001-15/2/2001	Y.K.Yan	ykyan@itc.gov.hk.
Singapore	NMC	15/2/2001-31/3/2001	Jing Tao	jing_tao@nmc.a-star.edu.sg
Australia	NMIA	1/4/2001-15/5/2001	Ilya Budovsky	Ilya.Budovsky@csiro.au
India	NPL	15/5/2001-30/6/2001	V.K.Rustagi A.K.Govil	rustagi@csnpl.ren.nic.in
Germany	PTB	1/7/2001-15/8/2001	Manfred Klonz	Manfred.Klonz@ptb.de
Chinese Taipei	CMS	15/8/2001-30/9/2001	Wei, Yih-cheng	YihChengWei@itri.org.tw
New Zealand	IRL	1/10/2001-15/11/2001	Murray Early	m.early@irl.cri.nz
Australia	NMIA	15/11/2001-31/12/2001	Ilya Budovsky	Ilya.Budovsky@nmi.gov.au
Japan	NMIJ	1/1/2002 -15/2/2002	Hitoshi Sasaki Hirojuki Fujiki	hitoshi-sasaki@aist.go.jp fujiki@aist.go.jp
Thailand	NIMT	15/2/2002 -31/3/2002	Chalit Kumtawee Ajchara Charoensook	nimt@nimt.or.th
Korea	KRISS	1/4/2002 -15/5/2002	Sung-Won Kwon	swkwon@kriss.re.kr
Australia	NMIA	15/5/2002-15/8/2002	Ilya Budovsky	Ilya.Budovsky@csiro.au
Viet Nam	VMI	15/8/2002-30/9/2002	Nguyen Anh Son	vmi@fpt.vn
Indonesia	KIM-LIPI	1/10/2002-30/11/2002	Bumbang Suprianto	bkmkim@cbn.net.id
South Africa	NMISA	1/12/2002-15/1/2003	Moses Temba	MLTemba@csir.co.za
Australia	NMIA	15/1/2003-28/2/2003	Ilya Budovsky	Ilya.Budovsky@csiro.au
Philippines	ITDI	1/3/2003-15/4/2002	Manuel Ruiz	mmr@agham.dost.gov.ph
Australia	NMIA	15/4/2003-31/5/2003	Ilya Budovsky	Ilya.Budovsky@nmi.gov.au

## 8. Transportation

- \* The case was transported by air freight without a carnet for Customs clearance.
- \* The case was designed so that the Thermal Converter was transported assembled together with the adapter plate and the N-type Tee together with the N-to-GR adapter. There was no need to disassemble these parts, however the participants had to ensure good contact before taking measurements.

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## 9. Contents of the pack

1. Thermoelement. Holt Model 11 Part Number 90081C, s/n 0943500001033
2. Adapter. Holt Model 11 Part Number 84980, s/n 0943500001037
3. Tee Piece, type 874TL
4. Tee Piece, type N. Pasternak PE9390
5. N-to-Type 874 Adapter. Pasternak PE9358
6. Output Connection Cable
7. Comparison Protocol

## 10. Measurement Results

It is known that the ac-dc difference of a TVC depends greatly on its input connector and the tee-adaptor used to connect it to the reference TVC. As a rule, in order to reduce this uncertainty, the test voltage is defined at the center-point of the tee adaptor. Such a definition was also adopted for the comparison described here. Two types of connector, known as Type N and GR Type 874, are commonly used in TVCs of the highest precision. The travelling standard was equipped with the latter connector. However, it was important to enable comparison of NMIs that use either type of connector in their reference TVC. For this purpose, the travelling standard was circulated with two tee adaptors, one being Type 874 and the other Type N-male with an additional N-female to Type 874 adaptor at the travelling standard end.

Prior to the start of the comparison, using methods described in [2], NMIA conducted a study of the differences that arise from the use of the travelling standard with the two circulated adaptors. These differences are presented in Table 3

**Table 3**

Correction $\delta_{874} - \delta_{N+874}$ in $\mu V/V$ at Frequencies					
1 kHz	20 kHz	50 kHz	100 kHz	500 kHz	1 MHz
0	-0.3	-0.7	-1.5	-4	-6.2

The summary of reported measurement results is given in Table 4. All results are for the Type 874 connector. The results of those participants who used Type N (NMC, MSL, NMIJ, NMISA, VMI and ITDI ) have been adjusted using the corrections in Table I. Since the uncertainties of these corrections were approximately one order of magnitude less than those reported by the participants, no further adjustments were made to the reported uncertainties below.

**Table 4**

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Laboratory	Nominal Measurement Period	Measured Ac-dc Difference $\delta_{LAB}$ and Expanded Uncertainty (95%) $U_{LAB}$ in $\mu V/V$											
		1 kHz		20 kHz		50 kHz		100 kHz		500 kHz		1 MHz	
		$\delta$	$U$	$\delta$	$U$	$\delta$	$U$	$\delta$	$U$	$\delta$	$U$	$\delta$	$U$
<b>NMIA</b>		<b>-5.0</b>	0.8	<b>-2.5</b>	1.9	<b>1.0</b>	4.0	<b>4.6</b>	5.0	<b>24.1</b>	12.0	<b>34.0</b>	18.0
<b>SIRIM</b>	15/11/2000-31/12/2000	<b>-5.5</b>	5.0	<b>-3.7</b>	7.0	<b>2.2</b>	6.0	<b>2.0</b>	8.0	<b>26.2</b>	17.0	<b>40.5</b>	27.0
<b>SCL</b>	1/1/2001-15/2/2001	<b>-10.0</b>	9.0	<b>-6.0</b>	9.0	<b>-7.0</b>	10.0	<b>-1.0</b>	15.0	<b>11.0</b>	33.0	<b>16.0</b>	78.0
<b>NMC</b>	15/2/2001-31/3/2001	<b>-5.1</b>	5.2	<b>-3.4</b>	5.2	<b>-0.4</b>	5.6	<b>1.1</b>	5.6	<b>7.0</b>	12.0	<b>16.8</b>	32.0
<b>NMIA</b>	1/4/2001-15/5/2001	<b>-5.0</b>	0.8	<b>-1.5</b>	1.9			<b>4.2</b>	5.0	<b>24.0</b>	12.0	<b>34.5</b>	18.0
<b>NPLI</b>	15/5/2001-30/6/2001	<b>-8.4</b>	4.4	<b>4.4</b>	4.6	<b>-3.5</b>	5.6	<b>-1.1</b>	6.4	<b>11.2</b>	22.8	<b>9.5</b>	26.0
<b>PTB</b>	1/7/2001-15/8/2001	<b>-5.3</b>	0.8	<b>-2.8</b>	0.8	<b>-0.6</b>	1.4	<b>1.1</b>	2.8	<b>5.4</b>	11.0	<b>8.9</b>	25.0
<b>CMS</b>	15/8/2001-30/9/2001	<b>-5.5</b>	2.0	<b>-3.0</b>	2.4	<b>-0.2</b>	2.7	<b>1.7</b>	6.7	<b>16.0</b>	16.0	<b>28.0</b>	29.0
<b>MSL</b>	1/10/2001-15/11/2001	<b>-4.4</b>	6.2	<b>-1.3</b>	8.4	<b>0.7</b>	12.7	<b>5.2</b>	16.3	<b>28.3</b>	33.0	<b>27.4</b>	53.4
<b>NMIA</b>	15/11/2001-31/12/2001	<b>-4.8</b>	0.8	<b>-2.2</b>	1.9	<b>1.1</b>	4.0	<b>4.4</b>	5.0	<b>22.1</b>	12.0	<b>29.7</b>	18.0
<b>NMIJ</b>	1/1/2002 - 15/2/2002	<b>-5.3</b>	1.1	<b>-3.1</b>	1.1	<b>0.1</b>	1.3	<b>4.2</b>	1.9	<b>22.9</b>	7.1	<b>27.7</b>	20.2
<b>NIMT</b>	15/2/2002 - 31/3/2002	<b>-4.7</b>	5.0	<b>-4.0</b>	6.0	<b>-1.2</b>	7.0	<b>3.0</b>	11.0	<b>29.9</b>	20.0	<b>49.7</b>	28.0
<b>KRISS</b>	1/4/2002 - 15/5/2002	<b>-6.6</b>	2.9	<b>-3.1</b>	2.9	<b>-0.7</b>	3.3	<b>2.1</b>	3.4	<b>12.5</b>	11.9	<b>16.1</b>	23.3
<b>NMIA</b>	15/5/2002-15/8/2002	<b>-4.9</b>	0.8	<b>-2.3</b>	1.9	<b>1.1</b>	4.0	<b>4.5</b>	5.0	<b>22.4</b>	12.0	<b>30.5</b>	18.0
<b>VMI</b>	15/8/2002-30/9/2002	<b>-4.7</b>	4.4	<b>-1.7</b>	6.5	<b>0.7</b>	14.1	<b>3.5</b>	16.3			<b>22.8</b>	65.0
<b>KIM-LIPI</b>	1/10/2002-30/11/2002	<b>-4.8</b>	5.0	<b>-2.9</b>	6.0	<b>0.0</b>	14.0	<b>3.1</b>	21.0	<b>17.5</b>	44.0	<b>20.8</b>	73.0
<b>NMISA</b>	1/12/2002-15/1/2003	<b>-3.9</b>	3.0	<b>-2.4</b>	3.0	<b>-0.1</b>	4.0	<b>1.6</b>	4.0	<b>6.1</b>	11.0	<b>7.8</b>	31.0
<b>NMIA</b>	15/1/2003-28/2/2003	<b>-5.0</b>	0.8	<b>-2.4</b>	1.9	<b>0.9</b>	4.0	<b>4.1</b>	5.0	<b>22.9</b>	12.0	<b>32.1</b>	18.0
<b>ITDI</b>	1/3/2003-15/4/2002	<b>-1.6</b>	8.8	<b>-3.0</b>	6.6	<b>1.3</b>	13.0	<b>3.5</b>	14.0	<b>120.0</b>	25.0	<b>138.8</b>	41.0
<b>NMIA</b>	1/6/2003-15/7/2003	<b>-5.1</b>	0.8	<b>-2.5</b>	1.9	<b>1.1</b>	4.0	<b>4.6</b>	5.0	<b>22.9</b>	12.0	<b>35.2</b>	18.0
<b>NMIA Mean</b>		<b>-5.0</b>	0.8	<b>-2.2</b>	1.9	<b>1.0</b>	4.0	<b>4.4</b>	5.0	<b>23.1</b>	12.0	<b>32.7</b>	18.0
<b>Ref Value</b>		<b>-5.2</b>	0.5	<b>-2.8</b>	0.6	<b>-0.1</b>	0.9	<b>3.3</b>	1.5	<b>18.8</b>	5.3	<b>25.6</b>	11.8
<b>NMIA STD</b>		<b>0.1</b>		<b>0.4</b>		<b>0.1</b>		<b>0.2</b>		<b>0.8</b>		<b>2.3</b>	

## 11. Determination of the Reference Values

The reference values for the APMP.EM-K6a have been based on the results by participants chosen with the following criteria:

1. An independent realisation of primary standards for ac-dc difference
2. The lowest values of reported uncertainties.

The following three laboratories satisfy the above criteria: NMIA [2], PTB[3, 4] and NMIJ [5].

For each frequency, the APMP.EM-K6a reference value  $\delta_{REF-APMP}$  and its standard uncertainty  $u_{REF-APMP}$  have been calculated from the results of these three laboratories as a weighted mean [6] given by:

$$\delta_{REF-APMP} / u_{REF-APMP} = \sum \delta_{LAB_i} / u_{LAB_i}^2,$$



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where

$$1/u^2_{REF-APMP} = \sum 1/u^2_{LAB,}$$

**Table 5**  
**Deviation  $D_{LAB-APMP}$  from APMP Reference Value and expanded uncertainty (95%)  $U_{LAB-APMP}$  in  $\mu V/V$**

Laboratory	Deviation from APMP Reference Value $D_{LAB-APMP}$ and Expanded Uncertainty (95%) $U_{LAB}$ in $\mu V/V$ at Frequencies											
	1 kHz		20 kHz		50 kHz		100 kHz		500 kHz		1 MHz	
Laboratory	$\delta$	$U$	$\delta$	$U$	$\delta$	$U$	$\delta$	$U$	$\delta$	$U$	$\delta$	$U$
NMIA	0.1	0.6	0.3	1.8	1.1	3.9	1.3	4.8	5.3	10.7	8.4	13.6
SIRIM	-0.3	5.0	-0.9	7.0	2.3	6.1	-1.3	8.1	7.4	17.8	14.9	29.5
SCL	-4.8	9.0	-3.2	9.0	-6.9	10.0	-4.3	15.1	-7.8	33.4	-9.6	78.9
NMC	0.1	5.2	-0.6	5.2	-0.3	5.6	-2.2	5.8	-11.8	13.1	-8.8	34.1
NMIA	0.1	0.6	1.3	1.8			0.9	4.8	5.2	10.7	8.9	13.6
NPLI	-3.2	4.4	7.2	4.6	-3.4	5.7	-4.4	6.6	-7.6	23.4	-16.1	28.6
PTB	-0.1	0.6	0.0	0.5	-0.5	1.0	-2.2	2.4	-13.4	9.6	-16.7	22.0
CMS	-0.3	2.1	-0.2	2.5	-0.1	2.9	-1.6	6.9	-2.8	16.9	2.4	31.3
MSL	0.8	6.2	1.5	8.4	0.8	12.7	1.9	16.4	9.5	33.4	1.8	54.7
NMIA	0.3	0.6	0.6	1.8	1.2	3.9	1.1	4.8	3.3	10.7	4.1	13.6
NMIJ	-0.1	1.0	-0.3	0.9	0.3	0.9	0.9	1.2	4.1	4.7	2.0	16.4
NIMT	0.5	5.0	-1.2	6.0	-1.1	7.1	-0.3	11.1	11.1	20.7	24.1	30.4
KRISS	-1.4	2.9	-0.3	3.0	-0.6	3.4	-1.2	3.7	-6.3	13.0	-9.5	26.1
NMIA	0.3	0.6	0.5	1.8	1.2	3.9	1.2	4.8	3.7	10.7	4.9	13.6
VMI	0.5	4.4	1.1	6.5	0.8	14.1	0.2	16.4			-2.8	66.1
KIM-LIPI	0.4	5.0	-0.1	6.0	0.1	14.0	-0.2	21.1	-1.3	44.3	-4.8	74.0
NMISA	1.3	3.0	0.4	3.1	0.0	4.1	-1.7	4.3	-12.7	12.2	-17.8	33.2
NMIA	0.2	0.6	0.4	1.8	1.0	3.9	0.7	4.8	4.1	10.7	6.5	13.6
ITDI	3.6	8.8	-0.2	6.6	1.4	13.0	0.2	14.1	101.2	25.6	113.2	42.7
NMIA	0.1	0.6	0.3	1.8	1.3	3.9	1.3	4.8	4.1	10.7	9.6	13.6
<b>NMIA Mean</b>	<b>0.2</b>	<b>0.6</b>	<b>0.6</b>	<b>1.8</b>	<b>1.2</b>	<b>3.9</b>	<b>1.1</b>	<b>4.8</b>	<b>4.3</b>	<b>10.7</b>	<b>7.0</b>	<b>13.6</b>

The deviation of each laboratory's result from the APMP.EM-K6a reference value,  $D_{LAB-APMP}$ , and its Expanded Uncertainty are given in Table 5. For the three reference laboratories the correlation with the reference value has been taken into account using the formula

$$u^2_{LAB-APMP} = u^2_{LAB} - u^2_{REF-APMP}, \quad (3)$$

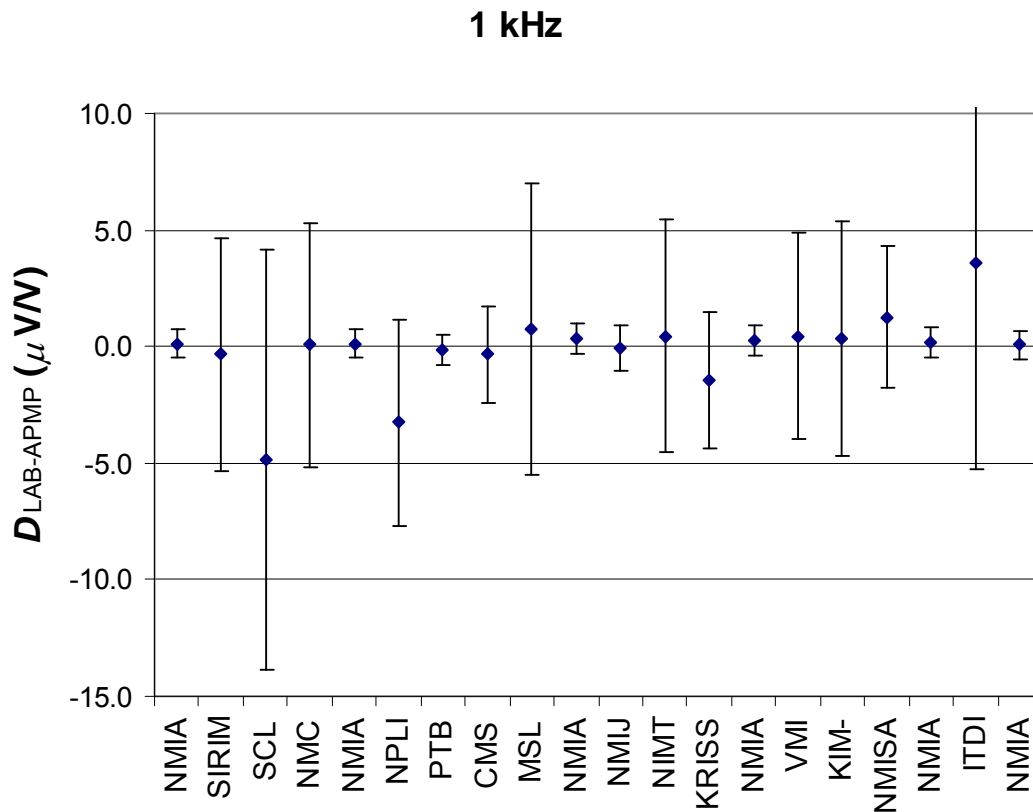
where  $u_{LAB}$  are the uncertainties reported by the laboratory. For the remaining laboratories there is no such correlation. Therefore, for these laboratories,

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$$u^2_{\text{LAB-APMP}} = u^2_{\text{LAB}} + u^2_{\text{REF-APMP}} . \quad (4)$$

Deviation  $D_{\text{LAB-APMP}}$  from APMP Reference Value and expanded uncertainties (95%)  $U_{\text{LAB-APMP}}$  are shown graphically below.

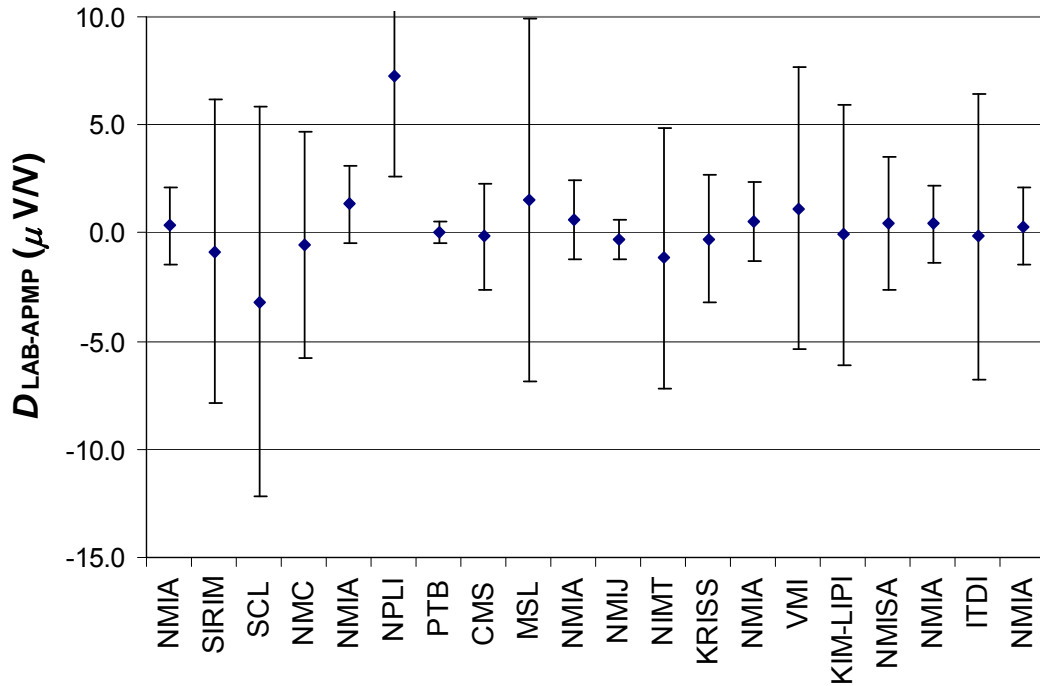
**Deviation  $D_{\text{LAB-APMP}}$  from APMP reference value and expanded uncertainty at 95% confidence level  $U_{\text{LAB-APMP}}$  in  $\mu\text{V/V}$ .**



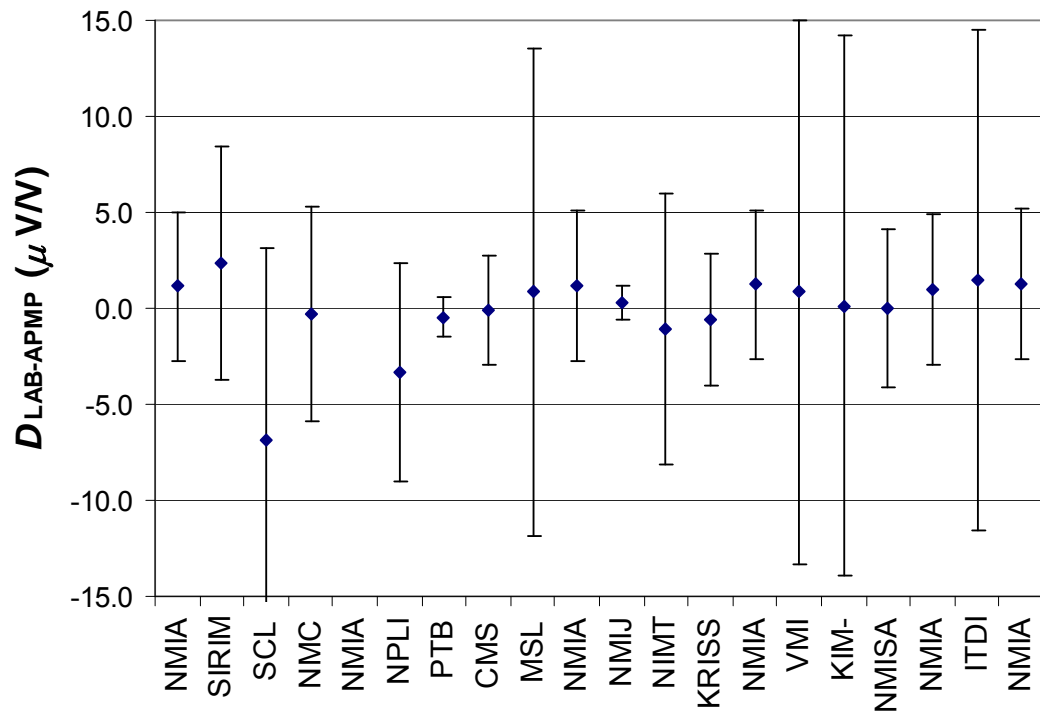
# APMP reference no. APMP.EM-K6.a

Deviation  $D_{\text{LAB-APMP}}$  from APMP reference value and expanded uncertainty at 95% confidence level  $U_{\text{LAB-APMP}}$  in  $\mu\text{V/V}$  (continued).

## 20 kHz



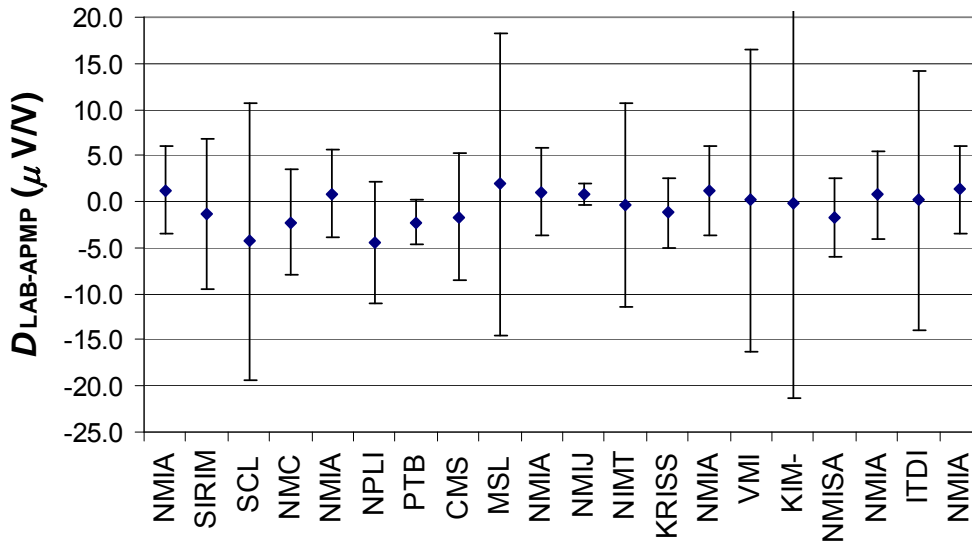
## 50 kHz



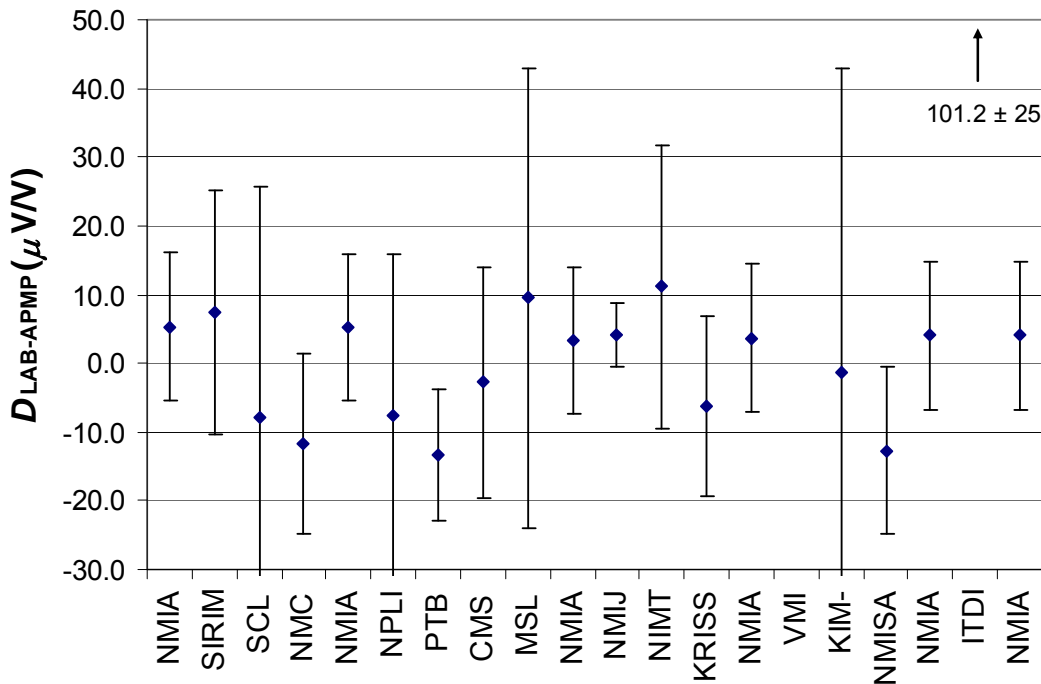
# APMP reference no. APMP.EM-K6.a

Deviation  $D_{\text{LAB-APMP}}$  from APMP reference value and expanded uncertainty at 95% confidence level  $U_{\text{LAB-APMP}}$  in  $\mu\text{V/V}$  (continued).

100 kHz



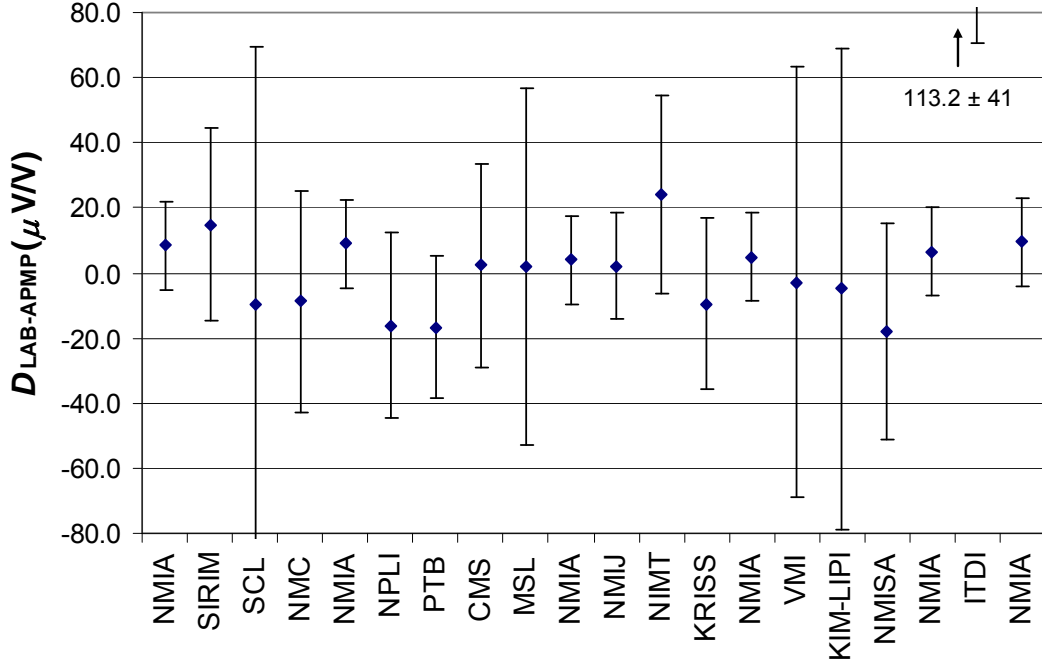
500 kHz



# APMP reference no. APMP.EM-K6.a

Deviation  $D_{\text{LAB-APMP}}$  from APMP reference value and expanded uncertainty at 95% confidence level  $U_{\text{LAB-APMP}}$  in  $\mu\text{V/V}$  (continued).

1 MHz



## 12. Linking the Results to CCEM-K6a

At the compulsory frequencies of 1 kHz, 20 kHz, 100 kHz and 1 MHz, the results of APMP.EM-K6a can be linked to CCEM-K6a through two of the three above laboratories, NMIA and PTB, that took part in both comparisons. Using their results, the difference between the APMP.EM-K6 reference value  $\delta_{\text{REF-APMP}}$  and the CCEM-K6a reference value  $\delta_{\text{REF-CCEM}}$  can be expressed as follows:

$$\delta_{\text{REF-APMP}} - \delta_{\text{REF-CCEM}} = \sum w_{\text{LAB}} (D_{\text{LAB-CCEM}} - D_{\text{LAB-APMP}}), \quad (5)$$

where  $D_{\text{LAB-CCEM}}$  and  $D_{\text{LAB-APMP}}$  are the deviations from CCEM-K6a and APMP.EM-K6a reference values of the linking laboratories, shown with corresponding expanded uncertainty in [1] and Table 5, respectively, and  $w_{\text{LAB}}$  is the weight calculated from:

$$w_{\text{LAB}} = \frac{1}{\sum \frac{1}{t_{\text{LAB-CCEM}}^2 + t_{\text{LAB-APMP}}^2 + 2r_{\text{LAB}}^2}}, \quad (6)$$

where  $t_{\text{LAB-CCEM}}$ ,  $t_{\text{LAB-APMP}}$  are transfer uncertainties caused essentially by the instability of the travelling standard and  $r_{\text{LAB}}$  is the uncertainty corresponding to imperfect reproducibility of the measurements at the laboratory in the period elapsed between the two comparisons. This uncertainty has been determined through a separate comparison held between NMIA and PTB in 2003.

# APMP reference no. APMP.EM-K6.a

**Table 6**  
**Deviation  $D_{\text{LAB-CCEM}}$  from CCEM Reference Value and expanded uncertainty**  
**(95%)  $U_{\text{LAB-CCEM}}$  in  $\mu\text{V/V}$**

Laboratory	1 kHz		20 kHz		100 kHz		1 MHz	
	$D_{\text{LAB-CCEM}}$	$U_{\text{LAB-CCEM}}$	$D_{\text{LAB-CCEM}}$	$U_{\text{LAB-CCEM}}$	$D_{\text{LAB-CCEM}}$	$U_{\text{LAB-CCEM}}$	$D_{\text{LAB-CCEM}}$	$U_{\text{LAB-CCEM}}$
NMIA	-0.2	1.5	0.1	2.2	0.2	4.6	5.2	24
PTB	0.1	0.4	0.1	1	-0.6	2	-13	24

NMIA figures in Table 6 have been adjusted by a small shift in NMIA values that occurred since participation in CCEM-K6a. The new values are the result of the study of the effect of different tee pieces mentioned above in section 2 and have been obtained by subtracting the corrections given in Table I from the values reported in [1].

The uncertainties of the link  $u_{\text{APMP-CCEM}}$  have been calculated in accordance with [7] from

$$\frac{1}{u^2_{\text{APMP-CCEM}}} = \sum \frac{1}{t^2_{\text{LAB-CCEM}} + t^2_{\text{LAB-APMP}} + 2r^2_{\text{LAB}}}. \quad (7)$$

Calculations in accordance with (5) - (7) yield the differences and expanded uncertainties given in Table 7.

**Table 7**  
**Correction  $\delta_{\text{REF-APMP}} - \delta_{\text{REF-CCEM}}$  and its expanded uncertainty (95%)**  
 **$U_{\text{APMP-CCEM}}$  in  $\mu\text{V/V}$**

1 kHz		20 kHz		100 kHz		1 MHz	
$\delta$	$U$	$\delta$	$U$	$\delta$	$U$	$\delta$	$U$
-0.1	0.3	-0.2	0.9	0.4	2.0	0.7	5.0

These differences are added to the values shown in Table 5 to obtain the values of each participant's deviation  $D_{\text{LAB-CCEM}}$  from the CCEM-K6a reference value.

Table 8 shows the deviation  $D_{\text{LAB-CCEM}}$  from the CCEM-K6a reference value and its uncertainty. For the laboratories that did not take part in CCEM-K6a, the uncertainty has been obtained from the sum of squares of uncertainties in Tables 5 and 7.

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**Table8**  
**Deviation  $D_{LAB-CCEM}$  from CCEM Reference Value and expanded uncertainty**  
**(95%)  $U_{LAB-CCEM}$  in  $\mu V/V$**

Laboratory	Deviation from CCEM-K6a Reference Value $D_{LAB-CCEM}$ and Expanded Uncertainty (95%) $U_{LAB}$ in $\mu V/V$ at Frequencies							
	1 kHz		20 kHz		100 kHz		1 MHz	
	$\delta$	$U$	$\delta$	$U$	$\delta$	$U$	$\delta$	$U$
NMIA	-0.2	1.5	0.1	2.2	0.2	4.6	5.2	24.0
SIRIM	-0.4	5.0	-1.1	7.1	-0.9	8.4	15.6	29.9
SCL	-4.9	9.0	-3.4	9.1	-3.9	15.2	-8.9	79.1
NMC	0.0	5.2	-0.8	5.3	-1.8	6.1	-8.1	34.5
NPLI	-3.3	4.4	7.0	4.7	-4.0	6.9	-15.4	29.0
PTB	0.1	0.4	0.1	1.0	-0.6	2.0	-13.0	24.0
ITRI	-0.4	2.1	-0.4	2.6	-1.2	7.2	3.1	31.7
MSL	0.7	6.2	1.3	8.5	2.3	16.5	2.5	54.9
NMIJ	-0.1	1.0	-0.5	1.3	1.3	2.3	2.8	17.1
NIMT	0.4	5.0	-1.4	6.1	0.1	11.3	24.8	30.8
KRISS	-1.5	3.0	-0.5	3.1	-0.8	4.2	-8.8	26.6
VMI	0.4	4.4	0.9	6.6	0.6	16.5	-2.1	66.3
KIM-LIPI	0.3	5.0	-0.3	6.1	0.2	21.2	-4.1	74.1
NMISA	1.2	3.1	0.2	3.2	-1.3	4.7	-17.1	33.6
ITDI	3.5	8.8	-0.4	6.7	0.6	14.2	113.9	43.0

### 13. Degree of Equivalence between Pairs of Laboratories

For two mutually independent laboratories  $i$  and  $j$  the degree of equivalence  $D_{i,j}$  and its expanded uncertainty  $U(D_{i,j})$  have been calculated as:

$$D_{i,j} = d_i - d_j, \text{ and} \quad (8)$$

$$U^2(D_{i,j}) = U^2(d_i) + U^2(d_j) - 2r_{ij}U(d_i)U(d_j), \quad (9)$$

where  $r_{ij}$  is the correlation coefficient for the results of NMI <sub>$i$</sub>  and NMI <sub>$j$</sub>  due to mutual correlation. The value of  $r_{ij}$  has been taken as zero for all pairs of laboratories, including mutually dependent laboratories. This is because, as evident from the results, the uncertainties of the laboratories that take the traceability from other NMIs are significantly larger than those of the calibration of their standards by the reference NMI. The values  $D_{i,j}$  and  $U(D_{i,j})$  are shown in Tables 9 to 14.

# APMP reference no. APMP.EM-K6.a

## 14. Conclusions

The APMP International Comparison of Ac-dc Transfer Standards at the Lowest Attainable Level of Uncertainty APMP.EM-K6a started in 2000 and concluded in 2003. The travelling standard has not been damaged and has shown excellent stability. The results submitted by the overwhelming majority of the participants lie well within the reported uncertainty. At the standard frequencies the results have been linked to those of the CCEM-K6a Key Comparison. The main results of these comparisons have been published in [8].

Since the completion of this comparisons the two reference laboratories, NMIA and PTB, have made adjustments to the values of their primary standards based on further research [9,10]. Applying the new values in the frequency range from 100 kHz to 1 MHz significantly reduces the difference to the reference value of this comparison. The uncertainties in this frequency range have also decreased. It is recommended that NMIs that are traceable to NMIA and PTB have their standards recalibrated.

**Table 9**  
**Degree of Equivalence between pairs of laboratories at 1 kHz**  
 **$D_{i,j}$  and its expanded uncertainty (95%)  $U(D_{i,j})$  in  $\mu V/V$**

	NMIA		NML-SIRIM		SCL		NMC		NPLI		PTB		CMS		MSL		NMIJ		NIMT		KRISS		VMI		KIM-LIPI		NMISA		ITDI	
	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$	$D_{i,j}$	$U^2(D_{i,j})$
NMIA			0.5	5.1	5.0	9.0	0.1	5.3	3.4	4.5	0.3	0.9	0.5	2.2	-0.6	6.3	0.3	1.2	-0.3	5.1	1.6	3.0	-0.3	4.5	-0.2	5.1	-1.1	3.1	-3.4	8.8
NML-SIRIM	-0.5	5.1			4.5	10	-0.4	7.2	2.9	6.7	-0.2	5.1	0.0	5.4	-1.1	8.0	-0.3	5.1	-0.8	7.1	1.1	5.8	-0.8	6.7	-0.7	7.1	-1.6	5.9	-3.9	10
SCL	-5.0	9.0	-4.5	10			-4.9	10	-1.6	10	-4.7	9.0	-4.5	9.2	-5.6	11	-4.8	9.1	-5.3	10	-3.4	9.5	-5.3	10.0	-5.2	10	-6.1	9.5	-8.4	13
NMC	-0.1	5.3	0.4	7.2	4.9	10			3.3	6.8	0.2	5.3	0.4	5.6	-0.7	8.1	0.2	5.3	-0.4	7.2	1.5	6.0	-0.4	6.8	-0.3	7.2	-1.2	6.0	-3.5	10
NPLI	-3.4	4.5	-2.9	6.7	1.6	10	-3.3	6.8			-3.1	4.5	-2.9	4.9	-4.0	7.6	-3.2	4.5	-3.7	6.7	-1.8	5.3	-3.7	6.3	-3.6	6.7	-4.5	5.4	-6.8	9.9
PTB	-0.3	0.9	0.2	5.1	4.7	9.0	-0.2	5.3	3.1	4.5			0.2	2.2	-0.9	6.3	0.0	1.2	-0.6	5.1	1.3	3.0	-0.6	4.5	-0.5	5.1	-1.4	3.1	-3.7	8.8
CMS	-0.5	2.2	0.0	5.4	4.5	9.2	-0.4	5.6	2.9	4.9	-0.2	2.2			-1.1	6.6	-0.3	2.3	-0.8	5.4	1.1	3.6	-0.8	4.9	-0.7	5.4	-1.6	3.7	-3.9	9.1
MSL	0.6	6.3	1.1	8.0	5.6	11	0.7	8.1	4.0	7.6	0.9	6.3	1.1	6.6			0.9	6.3	0.3	8.0	2.2	6.9	0.3	7.6	0.4	8.0	-0.5	6.9	-2.8	11
NMIJ	-0.3	1.2	0.3	5.1	4.8	9.1	-0.2	5.3	3.2	4.5	0.0	1.2	0.3	2.3	-0.9	6.3			-0.6	5.1	1.4	3.1	-0.6	4.5	-0.5	5.1	-1.4	3.2	-3.7	8.9
NIMT	0.3	5.1	0.8	7.1	5.3	10	0.4	7.2	3.7	6.7	0.6	5.1	0.8	5.4	-0.3	8.0	0.6	5.1			1.9	5.8	0.0	6.7	0.1	7.1	-0.8	5.9	-3.1	10
KRISS	-1.6	3.0	-1.1	5.8	3.4	9.5	-1.5	6.0	1.8	5.3	-1.3	3.0	-1.1	3.6	-2.2	6.9	-1.4	3.1	-1.9	5.8			-1.9	5.3	-1.8	5.8	-2.7	4.2	-5.0	9.3
VMI	0.3	4.5	0.8	6.7	5.3	10	0.4	6.8	3.7	6.3	0.6	4.5	0.8	4.9	-0.3	7.6	0.6	4.5	0.0	6.7	1.9	5.3			0.1	6.7	-0.8	5.4	-3.1	9.9
KIM-LIPI	0.2	5.1	0.7	7.1	5.2	10	0.3	7.2	3.6	6.7	0.5	5.1	0.7	5.4	-0.4	8.0	0.5	5.1	-0.1	7.1	1.8	5.8	-0.1	6.7			-0.9	5.9	-3.2	10
NMISA	1.1	3.1	1.6	5.9	6.1	9.5	1.2	6.0	4.5	5.4	1.4	3.1	1.6	3.7	0.5	6.9	1.4	3.2	0.8	5.9	2.7	4.2	0.8	5.4	0.9	5.9			-2.3	9.3
ITDI	3.4	8.8	3.9	10	8.4	13	3.5	10	6.8	9.9	3.7	8.8	3.9	9.1	2.8	11	3.7	8.9	3.1	10	5.0	9.3	3.1	9.9	3.2	10	2.3	9.3		



# APMP reference no. APMP.EM-K6.a

**Table 10**  
**Degree of Equivalence between Pairs of Laboratories at 20 kHz**  
*D<sub>ij</sub>* and its expanded uncertainty (95%) *U(D<sub>ij</sub>)* in  $\mu V/V$

	NMIA		NML-SIRIM		SCL		NMC		NPLI		PTB		CMS		MSL		NMIJ		NIMT		KRISS		VMI		KIM-LIPI		NMISA		ITDI	
	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>
NMIA			1.5	7.3	3.8	9.2	1.2	5.5	-6.6	5.0	0.6	1.9	0.8	3.1	-0.9	8.6	0.9	2.0	1.8	6.3	0.9	3.5	-0.5	6.8	0.7	6.3	0.2	3.6	0.8	6.9
NML-SIRIM	-1.5	7.3			2.3	11	-0.3	8.8	-8.1	8.4	-0.9	7.0	-0.7	7.5	-2.4	11	-0.6	7.1	0.3	9.3	-0.6	7.6	-2.0	9.6	-0.8	9.3	-1.3	7.7	-0.7	10
SCL	-3.8	9.2	-2.3	11			-2.6	10	-10.4	10	-3.2	9.0	-3.0	9.4	-4.7	12	-2.9	9.1	-2.0	11	-2.9	9.5	-4.3	11	-3.1	11	-3.6	9.5	-3.0	11
NMC	-1.2	5.5	0.3	8.8	2.6	10			-7.8	7.0	-0.6	5.3	-0.4	5.8	-2.1	9.9	-0.3	5.3	0.6	8.0	-0.3	6.0	-1.7	8.4	-0.5	8.0	-1.0	6.1	-0.4	8
NPLI	6.6	5.0	8.1	8.4	10.4	10	7.8	7.0			7.2	4.7	7.4	5.3	5.7	9.6	7.5	4.7	8.4	7.6	7.5	5.5	6.1	8.0	7.3	7.6	6.8	5.6	7.4	8.1
PTB	-0.6	1.9	0.9	7.0	3.2	9.0	0.6	5.3	-7.2	4.7			0.2	2.5	-1.5	8.4	0.3	1.0	1.2	6.1	0.3	3.0	-1.1	6.5	0.1	6.1	-0.4	3.1	0.2	6.6
CMS	-0.8	3.1	0.7	7.5	3.0	9.4	0.4	5.8	-7.4	5.3	-0.2	2.5			-1.7	8.8	0.1	2.6	1.0	6.5	0.1	3.9	-1.3	7.0	-0.1	6.5	-0.6	3.9	0.0	7.1
MSL	0.9	8.6	2.4	11	4.7	12	2.1	9.9	-5.7	9.6	1.5	8.4	1.7	8.8			1.8	8.5	2.7	10	1.8	8.9	0.4	11	1.6	10	1.1	9.0	7.7	11
NMIJ	-0.9	2.0	0.6	7.1	2.9	9.1	0.3	5.3	-7.5	4.7	-0.3	1.0	-0.1	2.6	-1.8	8.5			0.9	6.1	0.0	3.1	-1.4	6.6	-0.2	6.1	-0.7	3.2	-0.1	6.7
NIMT	-1.8	6.3	-0.3	9.3	2.0	11	-0.6	8.0	-8.4	7.6	-1.2	6.1	-1.0	6.5	-2.7	10	-0.9	6.1			-0.9	6.7	-2.3	8.9	-1.1	8.5	-1.6	6.8	-1.0	9
KRISS	-0.9	3.5	0.6	7.6	2.9	9.5	0.3	6.0	-7.5	5.5	-0.3	3.0	-0.1	3.9	-1.8	8.9	0.0	3.1	0.9	6.7			-1.4	7.2	-0.2	6.7	-0.7	4.3	-0.1	7.3
VMI	-0.5	6.8	2.0	9.6	4.3	11	1.7	8.4	-6.1	8.0	1.1	6.5	1.3	7.0	-0.4	11	1.4	6.6	2.3	8.9	1.4	7.2			1.2	8.9	0.7	7.2	1.3	9.3
KIM-LIPI	-0.7	6.3	0.8	9.3	3.1	11	0.5	8.0	-7.3	7.6	-0.1	6.1	0.1	6.5	-1.6	10	0.2	6.1	1.1	8.5	0.2	6.7	-1.2	8.9			-0.5	6.8	0.1	9
NMISA	-0.2	3.6	1.3	7.7	3.6	9.5	1.0	6.1	-6.8	5.6	0.4	3.1	0.6	3.9	-1.1	9.0	0.7	3.2	1.6	6.8	0.7	4.3	-0.7	7.2	0.5	6.8			0.6	7.3
ITDI	-0.8	6.9	0.7	10	3.0	11	0.4	8	-7.4	8.1	-0.2	6.6	0.0	7.1	-1.7	11	0.1	6.7	1.0	9	0.1	7.3	-1.3	9.3	-0.1	9	-0.6	7.3		

**Table 11**  
**Degree of Equivalence between Pairs of Laboratories at 50 kHz**  
*D<sub>ij</sub>* and its expanded uncertainty (95%) *U(D<sub>ij</sub>)* in  $\mu V/V$

	NMIA		NML-SIRIM		SCL		NMC		NPLI		PTB		CMS		MSL		NMIJ		NIMT		KRISS		VMI		KIM-LIPI		NMISA		ITDI	
	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>
NMIA			-1.2	7.2	8.0	11	1.4	6.8	4.5	6.9	1.6	4.0	1.2	4.8	0.3	13	0.9	4.0	2.2	8.1	1.7	5.2	0.3	15	1.0	15	1.1	5.7	-0.3	14
NML-SIRIM	1.2	7.2			9.2	12	2.6	8.3	5.7	8.3	2.8	6.2	2.4	6.7	1.5	14	2.1	6.1	3.4	9.3	2.9	7.0	1.5	15	2.2	15	2.3	7.3	0.9	14
SCL	-8.0	11	-9.2	12			-6.6	11	-3.5	12	-6.4	10	-6.8	10	-7.7	16	-7.1	10	-5.8	12	-6.3	11	-7.7	17	-7.0	17	-6.9	11	-8.3	16
NMC	-1.4	6.8	-2.6	8.3	6.6	11			3.1	8.0	0.2	5.7	-0.2	6.3	-1.1	14	-0.5	5.7	0.8	9.0	0.3	6.6	-1.1	15	-0.4	15	-0.3	6.9	-1.7	14
NPLI	-4.5	6.9	-5.7	8.3	3.5	12	-3.1	8.0			-2.9	5.8	-3.3	6.4	-4.2	14	-3.6	5.7	-2.3	9.1	-2.8	6.6	-4.2	15	-3.5	15	-3.4	7.0	-4.8	14
PTB	-1.6	4.0	-2.8	6.2	6.4	10	-0.2	5.7	2.9	5.8			-0.4	3.0	-1.3	13	-0.7	1.4	0.6	7.1	0.1	3.6	-1.3	14	-0.6	14	-0.5	4.2	-1.9	13
CMS	-1.2	4.8	-2.4	6.7	6.8	10	0.2	6.3	3.3	6.4	0.4	3.0			-0.9	13	-0.3	3.0	1.0	7.6	0.5	4.5	-0.9	14	-0.2	14	-0.1	5.0	-1.5	13
MSL	-0.3	13	-1.5	14	7.7	16	1.1	14	4.2	14	1.3	13	0.9	13			0.6	13	1.9	15	1.4	13.2	0.0	19	0.7	19	0.8	13	-0.6	18
NMIJ	-0.9	4.0	-2.1	6.1	7.1	10	0.5	5.7	3.6	5.7	0.7	1.4	0.3	3.0	-0.6	13			1.3	7.1	0.8	3.5	-0.6	14	0.1	14	0.2	4.2	-1.2	13
NIMT	-2.2	8.1	-3.4	9.3	5.8	12	-0.8	9.0	2.3	9.1	-0.6	7.1	-1.0	7.6	-1.9	15	-1.3	7.1			-0.5	7.8	-1.9	16	-1.2	16	-1.1	8.2	-2.5	15
KRISS	-1.7	5.2	-2.9	7.0	6.3	11	-0.3	6.6	2.8	6.6	-0.1	3.6	-0.5	4.5	-1.4	13	-0.8	3.5	0.5	7.8			-1.4	15	-0.7	14	-0.6	5.3	-2.0	13
VMI	-0.3	15	-1.5	15	7.7	17	1.1	15	4.2	15	1.3	14	0.9	14	0.0	19	0.6	14	1.9	16	1.4	15			0.7	20	0.8	15	-0.6	19
KIM-LIPI	-1.0	15	-2.2	15	7.0	17	0.4	15	3.5	15	0.6	14	0.2	14	-0.7	19	-0.1	14	1.2	16	0.7	14	-0.7	20			0.1	15	-1.3	19
NMISA	-1.1	5.7	-2.3	7.3	6.9	11	0.3	6.9	3.4	7.0	0.5	4.2	0.1	5.0	-0.8	13	-0.2	4.2	1.1	8.2	0.6	5.3	-0.8	15	-0.1	15			-1.4	14
ITDI	0.3	14	-0.9	14	8.3	16	1.7	14	4.8	14	1.9	13	1.5	13	0.6	18	1.2	13	2.5	15	2.0	13	0.6	19	1.3	19	1.4	14		

**Table 12**  
**Degree of Equivalence between Pairs of Laboratories at 100 kHz**  
*D<sub>ij</sub>* and its expanded uncertainty (95%) *U(D<sub>ij</sub>)* in  $\mu V/V$

	NMIA		NML-SIRIM		SCL		NMC		NPLI		PTB		CMS		MSL		NMIJ		NIMT		KRISS		VMI		KIM-LIPI		NMISA		ITDI	
	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>	<i>D<sub>ij</sub></i>	<i>U<sup>2</sup>(D<sub>ij</sub>)</i>
NMIA			2.4	9.4	5.4	16	3.3	7.5	5.5	8.1	3.3	5.3	2.7	8.4	-0.8	17	0.2	4.9	1.4	12	2.3	6.0	0.9	17	1.3	22	2.8	6.4	0.9	15
NML-SIRIM	-2.4	9.4			3.0	17	0.9	10	3.1	10	0.9	8.5	0.3	11	-3.2	18	-2.2	8.2	-1.0	14	-0.1	8.9	-1.5	18	-1.1	23	0.4	9.2	-1.5	16
SCL	-5.4	16	-3.0	17			-2.1	16	0.1	16	-2.1	15	-2.7	17	-6.2	22	-5.2	15	-4.0	19	-3.1	16	-4.5	22	-4.1	26	-2.6	16	-4.5	21
NMC	-3.3	7.5	-0.9	10	2.1	16			2.2	8.8	0.0	6.3	-0.6	9.0	-4.1	17	-3.1	5.9	-1.9	13	-1.0	6.9	-2.4	17	-2.0	22	-0.5	7.2	-2.4	15
NPLI	-5.5	8.1	-3.1	10	-0.1</																									

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**Table 13**  
**Degree of Equivalence between Pairs of Laboratories at 500 kHz**  
 **$D_{i,j}$  and its expanded uncertainty (95%)  $U(D_{i,j})$  in  $\mu V/V$**

	NMIA	NML-SIRIM	SCL	NMC	NPLI	PTB	CMS	MSL	NMIJ	NIMT	KRISS	VMI	KIM-LIPI	NMISA	ITDI
	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$
NMIA		-3 21	12 35	16 17	12 26	18 14	7 20	-5 35	0 12	-7 23	11 17	4 11	6 46	17 16	-97 28
NML-SIRIM	3 21		15 38	19 22	15 29	21 20	10 25	-2 38	3 18	-4 27	14 22	7 18	9 48	20 22	-94 31
SCL	-12 35	-15 38		4 36	0 41	6 35	-5 37	-17 47	-12 34	-19 39	-2 36	-8 33	-7 56	5 36	-109 42
NMC	-16 17	-19 22	-4 36		-4 27	2 16	-9 21	-21 36	-16 14	-23 25	-6 19	-12 13	-11 46	1 18	-113 29
NPLI	-12 26	-15 29	0 41	4 27		6 25	-5 29	-17 41	-12 24	-19 31	-1 27	-8 23	-6 50	5 26	-109 35
PTB	-18 14	-21 20	-6 35	-2 16	-6 25		-11 19	-23 35	-17 11	-25 23	-7 16	-13 10	-12 45	-1 16	-115 27
CMS	-7 20	-10 25	5 37	9 21	5 29	11 19		-12 37	-7 18	-14 27	4 21	-3 17	-2 47	10 21	-104 31
MSL	5 35	2 38	17 47	21 36	17 41	23 35	12 37		5 34	-2 39	16 36	10 33	11 56	22 36	-92 42
NMIJ	0 12	-3 18	12 34	16 14	12 24	17 11	7 18	-5 34		-7 21	10 14	4 5	5 45	17 13	-97 26
NIMT	7 23	4 27	19 39	23 25	19 31	25 23	14 27	2 39	7 21		17 24	11 21	12 49	24 24	-90 33
KRISS	-11 17	-14 22	2 36	6 19	1 27	7 16	-4 21	-16 36	-10 14	-17 24		-6 13	-5 46	6 18	-108 29
VMI	-4 11	-7 18	8 33	12 13	8 23	13 10	3 17	-10 33	-4 5	-11 21	6 13		1 44	13 12	-101 26
KIM-LIPI	-6 46	-9 48	7 56	11 46	6 50	12 45	2 47	-11 56	-5 45	-12 49	5 46	-1 44		11 46	-103 51
NMISA	-17 16	-20 22	-5 36	-1 18	-5 26	1 16	-10 21	-22 36	-17 13	-24 24	-6 18	-13 12	-11 46		-114 28
ITDI	97 28	94 31	109 42	113 29	109 35	115 27	104 31	92 42	97 26	90 33	108 29	101 26	103 51	114 28	

**Table 14**  
**Degree of Equivalence between Pairs of Laboratories at 1 MHz**  
 **$D_{i,j}$  and its expanded uncertainty (95%)  $U(D_{i,j})$  in  $\mu V/V$**

	NMIA	NML-SIRIM	SCL	NMC	NPLI	PTB	CMS	MSL	NMIJ	NIMT	KRISS	VMI	KIM-LIPI	NMISA	ITDI
	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$	$D_{i,j}$ $U^2(D_{i,j})$
NMIA		-8 32	17 80	16 37	23 32	24 26	5 34	5 56	5 21	-17 33	17 29	10 67	12 75	25 36	-106 45
NML-SIRIM	8 32		25 84	24 45	31 41	32 37	13 43	13 62	13 34	-9 42	24 39	18 72	20 80	33 44	-98 52
SCL	-17 80	-25 84		-1 86	7 84	7 82	-12 85	-11 96	-12 81	-34 85	0 83	-7 103	-5 108	8 86	-123 90
NMC	-16 37	-24 45	1 86		7 44	8 41	-11 46	-11 64	-11 38	-33 46	1 43	-6 74	-4 81	9 48	-122 55
NPLI	-23 32	-31 41	-7 84	-7 44		1 36	-19 42	-18 62	-18 33	-40 42	-7 39	-13 72	-11 79	2 44	-129 51
PTB	-24 26	-32 37	-7 82	-8 41	-1 36		-19 38	-19 59	-19 27	-41 38	-7 34	-14 70	-12 77	1 40	-130 48
CMS	-5 34	-13 43	12 85	11 46	19 42	19 38		1 63	0 35	-22 44	12 41	5 73	7 80	20 46	-111 53
MSL	-5 56	-13 62	11 96	11 64	18 62	19 59	-1 63		0 57	-22 63	11 61	5 86	7 92	20 64	-111 69
NMIJ	-5 21	-13 34	12 81	11 38	18 33	19 27	0 35	0 57		-22 35	12 31	5 68	7 76	20 37	-111 46
NIMT	17 33	9 42	34 85	33 46	40 42	41 38	22 44	22 63	22 35		34 40	27 73	29 80	42 45	-89 52
KRISS	-17 29	-24 39	0 83	-1 43	7 39	7 34	-12 41	-11 61	-12 31	-34 40		-7 71	-5 78	8 42	-123 50
VMI	-10 67	-18 72	7 103	6 74	13 72	14 70	-5 73	-5 86	-5 68	-27 73	7 71		2 99	15 74	-116 79
KIM-LIPI	-12 75	-20 80	5 108	4 81	11 79	12 77	-7 80	-7 92	-7 76	-29 80	5 78	-2 99		13 81	-118 85
NMISA	-25 36	-33 44	-8 86	-9 48	-2 44	-1 40	-20 46	-20 64	-20 37	-42 45	-8 42	-15 74	-13 81		-131 54
ITDI	106 45	98 52	123 90	122 55	129 51	130 48	111 53	111 69	111 46	89 52	123 50	116 79	118 85	131 54	

## References

- [1] M. Klonz, "CCEM-K6.a: Key comparison of ac-dc voltage transfer standards at the lowest attainable level of uncertainty," *Metrologia Tech. Suppl.*, 2002, vol. 39, 01002 .
- [2] I. Budovsky and B D Inglis, "High-Frequency AC-DC Differences of NMIA Single-Junction Thermal Voltage Converters at Frequencies," *IEEE Transactions on Instrum. Meas.*, Vol. 50, No1, February 2001, pp 101-105.
- [3] M. Klonz, "Ac-dc transfer difference of PTB-Multijunction thermal converter from 10 Hz to 100 kHz," *IEEE Transactions on Instrum. Meas.*, Vol. 36, , pp 320-329, 1987.
- [4] M. Klonz, "Ac-dc transfer difference of PTB-Multijunction thermal converter at 1 MHz," *CPEM'90 Digest*, Ottawa, June 1990, pp 60-61.

# APMP reference no. APMP.EM-K6.a

- [5] H Sasaki and K Takahashi, "Development of a high-precision AC-DC transfer standard using the Fast\_Reversed DC Method," Researches of the Electrotechnical Laboratory, No 989, June 1999.
- [6] C.F. Dietrich, Uncertainty, Calibration and Probability, Adam Hilger, Bristol, UK, 1991
- [7] Delahaye F. and Witt T.J., "Linking the results of key comparison CCEM-K4 with the 10 pF results of EUROMET.EM-K4," *Metrologia Tech. Suppl.*, 2002, vol. 39, 01005.
- [8] Budovsky, I.; BinZainalAbidin, A.R.; Yan, A.Y.K.; Liu, L.; Rustagi, V.K.; Govil, A.K.; Klonz, M.; Wei, Y.; Early, M.D.; Sasaki, H.; Fujiki, H.; Kumtawee, C.; Charoensook, A.; Kwon, S.-W.; Son, N.A.; Suprianto, B.; Temba, M.; Ruiz, M.; Leones, S.P.B., "APMP International Comparison of AC-DC Transfer Standards at the Lowest Attainable Level of Uncertainty," *IEEE Transactions on Instrumentation and Measurement*, Volume 54, Issue 2, April 2005, pp.795 – 798.
- [9] T. Hagen and I. Budovsky, "Single- Junction Thermal Voltage Converters With Reduced Uncertainties at Frequencies up to 1 MHz," *IEEE Transactions on Instrum. Meas.*, April 2009, to be published.
- [10] L. Scarioni, M. Klonz, and E. Keßler, "NEW GENERATION OF CRYSTAL QUARTZ THIN-FILM MULTIJUNCTION THERMAL CONVERTERS". In: Symposium of Metrology 2004, Querétaro, Mexico, October 25-27, 2004, October 2004.

## APENDIX 1. Uncertainty Budgets

### NMIA

Frequency (kHz)	1- $\sigma$ Uncertainty Components ( $\mu V/V$ )						Total	$\nu_{eff}$	Expanded Uncertainty ( $\mu V/V$ )
	Re.f TVC	Type A	Ref. Drift	Connectors	Meas Setup				
1	0.4	0.2	0.1	0.0	0.1	0.4	78	0.8	
20	0.9	0.2	0.2	0.1	0.1	0.9	60	1.9	
50	1.9	0.2	0.5	0.3	0.2	2.0	60	4.0	
100	2.3	0.2	0.5	0.8	0.3	2.5	65	5.0	
500	5.9	0.2	0.5	1.2	0.6	6.1	60	12.1	
1000	8.8	0.2	1.0	1.5	1.0	9.0	55	18.1	

### NML-SIRIM

Contribution	2V Std.	2V to 3V transfer	4V NML - 3V	n	T-piece	Drift in 2V Std.	Rounding off uncertainty	Combined uncertainty	$\nu_{eff}$	k	U 95%
Unit	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)			(ppm)
Evaluation Type	B	A	A	A			B				
DOF, $\nu$	50	9	49	59			$\infty$				
Frequency (Hz)											
1000	2	0.78	0.51	1	0.05	0.05	0.29	2.44	93.4	1.99	5
20000	2.5	1.77	0.58	1	0.05	0.05	0.29	3.29	61.7	2.00	7
50000	2.5	1.21	0.53	1	0.05	0.06	0.29	3.01	79.4	1.99	6
100000	3.5	1.08	0.62	1	0.1	0.1	0.29	3.86	69.8	1.99	8
500000	8.5	1.05	0.78	1	0.1	0.1	0.29	8.66	53.9	2.01	17
1000000	13.5	1.08	0.68	1	0.1	0.1	0.29	13.60	51.5	2.01	27

# APMP reference no. APMP.EM-K6.a

## SCL

Test Voltage (V)	Test Freq. (Hz)	Ks (ppm/nV)	Kx (ppm/nV)	Standard Uncertainty Contributions					Combined Standard Uncertainty u(Sx) (± ppm)	Expanded Uncertainty at 95 % C.L. U (± ppm)	Coverage Factor k
				Type B				Type A			
				u(Ss) (ppm)	u(Mr) (nV)	u(Nr) (nV)	u(β) (ppm)	u(random) (ppm)			
3	1 k	0.13	0.13	3.5	2.9	2.9	2.9	0.4	4.58	8.98	1.96
	20 k	0.13	0.13	3.5	2.9	2.9	2.9	0.3	4.58	8.98	1.96
	50 k	0.13	0.13	4.0	2.9	2.9	2.9	0.4	4.98	9.75	1.96
	100 k	0.13	0.13	4.5	2.9	2.9	5.8	0.3	7.35	14.40	1.96
	500 k	0.13	0.13	12.0	2.9	2.9	11.5	0.3	16.66	32.66	1.96
	1 M	0.13	0.13	27.0	2.9	2.9	28.9	0.3	39.53	77.48	1.96

$$u^2(Sx) = u^2(Ss) + Ks^2u^2(Mr) + Kx^2u^2(Nr) + u^2(\beta) + u^2(\text{random})$$

## NMC

Frequency	1 kHz	20 kHz	50 kHz	100 kHz	500 kHz	1 MHz
<b>Type A standard uncertainty (μV/V)</b>	<b>0.1</b>	<b>0.1</b>	<b>0.2</b>	<b>0.2</b>	<b>0.1</b>	<b>0.3</b>
▪ Standard deviation (μV/V)	0.3	0.3	0.5	0.5	0.2	0.8
<b>Type B standard uncertainty (μV/V)</b>	<b>2.5</b>	<b>2.5</b>	<b>2.8</b>	<b>2.8</b>	<b>5.5</b>	<b>15.2</b>
▪ Reference standard (μV/V)	1.0	1.0	1.5	1.5	5.0	15.0
▪ System Set-up (μV/V)	2.3	2.3	2.4	2.4	2.4	2.6
<b>Combined standard uncertainty (μV/V)</b>	<b>2.6</b>	<b>2.6</b>	<b>2.8</b>	<b>2.8</b>	<b>5.6</b>	<b>16</b>
Degree of freedom	8	8	8	8	8	8

## NPLI

Uncertainty budget of the ac-dc voltage transfer difference measurement in NPL, India									
Standard measurement uncertainty in ppm at different frequencies									
Influence quantity	1 kHz	20 kHz	50 kHz	100 kHz	500 kHz	1000k Hz	Degrees of freedom	Type A or B	Shape of distribution
Measurement data	0.4	0.5	0.3	0.4	0.4	0.5	14	A	Normal
Reference Standard	0.6	1.0	1.8	2.2	10.0	11.1	infinity	A	Normal
Measurement set up	0.5	0.5	0.5	0.5	3.0	4.0	Infinity	B	Rectangular
Connector & Tee	0	0	0	1.0	4.0	5.0	Infinity	B	Rectangular
Value of Exponent	2.0	2.0	2.0	2.0	2.0	2.0	Infinity	B	Rectangular
Combined standard uncertainty ( u <sub>s</sub> )	2.2	2.3	2.8	3.2	11.4	13.0			
Expanded uncertainty for 95% confidence level(U)	4.4	4.6	5.6	6.4	22.8	26.0			

# APMP reference no. APMP.EM-K6.a

PTB

The model function is:  $\delta_x = \delta_s + \delta_d + \delta_{con} + \delta_{calibrator}$

$\delta_x$	AC-DC Voltage Transfer Difference of the unknown standard
$\delta_s$	AC-DC Voltage Transfer Difference of the standard at the 3 V taken from (5)
$\delta_{con}$	AC-DC Voltage Transfer Difference due to the different T-connectors especially at high frequencies and electromagnetic influences from outside
$\delta_{calibrator}$	AC-DC Voltage Transfer Difference with different calibrators and calibration set-ups in the step-down
$\delta_d$	measured difference $\delta_d$ of the ac-dc transfer differences of the unknown $\delta_x$ and the known standard $\delta_s$

Table I shows the uncertainty budget for the PTB standard at 3 V, the PMJTC at 3 V and the calibration of the travelling standard (SJTC).

**Table I Uncertainty budget**

influence quantity	Standard measurement uncertainty $u$ in $\mu\text{V/V}$ at the frequencies					
	1 kHz	20 kHz	50 kHz	100 kHz	500 kHz	1 MHz
$u(\delta_{TH})$	0,01	0,01	0,01	0,01	0,01	0,01
$u(\delta_{L,G,C})$	0	0,2	0,5	0,9	4,5	9,3
$u(\delta_{skin})$	0	0	0	0	1,1	4,4
$u(\delta_{con})$	0	0	0,1	0,5	1,8	2,4
$u(\delta_F)$	0	0	0	0	0	0
$u(\delta_s)$	<b>0,0</b>	<b>0,2</b>	<b>0,5</b>	<b>1,0</b>	<b>5,0</b>	<b>10,6</b>
$u(\delta_A)$	0,1	0,1	0,1	0,1	0,2	0,2
$u(\delta_C)$	0,2	0,2	0,2	0,2	0,2	0,2
$u(\delta_d)$	<b>0,2</b>	<b>0,2</b>	<b>0,2</b>	<b>0,2</b>	<b>0,3</b>	<b>0,3</b>
$u(\delta_{con})$	<b>0</b>	<b>0</b>	<b>0,1</b>	<b>0,5</b>	<b>1,8</b>	<b>2,4</b>
$u(\delta_{PMJTC})$	<b>0,2</b>	<b>0,3</b>	<b>0,5</b>	<b>1,2</b>	<b>5,3</b>	<b>11,9</b>
$u(\delta_{ASJTC})$	0,2	0,2	0,2	0,2	0,2	0,2
$u(\delta_{CSJTC})$	0,2	0,2	0,2	0,2	0,2	0,2
$u(\delta_{dSJTC})$	<b>0,3</b>	<b>0,3</b>	<b>0,3</b>	<b>0,3</b>	<b>0,3</b>	<b>0,3</b>
$u(\delta_{con})$	<b>0</b>	<b>0</b>	<b>0,1</b>	<b>0,5</b>	<b>1,8</b>	<b>2,4</b>
$u(\delta_{calibrator})$	<b>0,2</b>	<b>0,2</b>	<b>0,3</b>	<b>0,4</b>	<b>0,6</b>	<b>2,4</b>
$u(\delta_{SJTC})$	<b>0,4</b>	<b>0,4</b>	<b>0,7</b>	<b>1,4</b>	<b>5,6</b>	<b>12,2</b>
$U (k=2)$	<b>0,8</b>	<b>0,8</b>	<b>1,4</b>	<b>2,8</b>	<b>11</b>	<b>25</b>

Remarks:

$$u^2(\delta_s) = u^2(\delta_{TH}) + u^2(\delta_{L,G,C}) + u^2(\delta_{skin}) + u^2(\delta_{con}) + u^2(\delta_F);$$

$$u^2(\delta_d) = u^2(\delta_A) + u^2(\delta_C);$$

$$u^2(\delta_{PMJTC}) = u^2(\delta_s) + u^2(\delta_d) + u^2(\delta_{con})$$

$$u^2(\delta_{dSJTC}) = u^2(\delta_{ASJTC}) + u^2(\delta_{CSJTC});$$

$$u^2(\delta_{SJTC}) = u^2(\delta_{PMJTC}) + u^2(\delta_{dSJTC}) + u^2(\delta_{con}) + u^2(\delta_{calibrator})$$

$$U = k u(\delta_{SJTC}); k \text{ is taken as } 2$$

# APMP reference no. APMP.EM-K6.a

CMS

Source of uncertainty	Uncertainty, $\mu\text{V}/\text{V}$ , 3 V test voltage at frequency					
	1 kHz	20 kHz	50 kHz	100 kHz	500 kHz	1 MHz
Random effect	0.3	0.3	0.3	0.7	1	1.3
Standard's uncertainty	0.5	0.5	0.7	1.5	4	8
Comparator's uncertainty	0.8	1.0	1.2	3	7	12
Combined standard uncertainty	1.0	1.2	1.4	3.4	8.1	15
Degrees of freedom	1000	2074	3842	4454	34437	141807
Coverage factor, k	1.96	1.96	1.96	1.96	1.96	1.96
Expanded uncertainty	2.0	2.4	2.7	6.7	16	29

MSL

Table of Uncertainty Components							
Description	Standard Uncertainty ( $\mu\text{V}/\text{V}$ )						Comment
	Frequency (kHz)						
	1	20	50	100	500	1000	
Reference Standard	3	4	6	7.5	14	20	NML Calibration of 792A ( $\nu = 200$ )
Stability of Reference	0.8	1.2	1.2	1.6	8.2	16.3	Comparison with other instruments ( $\nu = 5$ )
Type A, non-linear drift and meeting definition	0.1	0.2	0.2	0.2	0.2	0.3	Evaluated during measurement process ( $\nu = 100$ )
Grounding	0.5	0.5	2.0	3.0	3.0	4.0	Different grounding points ( $\nu = 5$ )
Measurement set-up	0.3	0.5	0.4	0.5	1.4	2.0	Changes due to variation in equipment ( $\nu = 13$ )
Difference in Tee definition	0	0	0	0.1	0.2	1.0	Change from GR tee + adaptor to Type N tee ( $\nu = 5$ )
<b>Combined standard uncertainty</b>	3.2	4.2	6.5	8.3	16.5	26.2	
<b>Effective degrees of freedom</b>	199	186	171	139	68	31	
<b>Expanded uncertainty</b>	6.2	8.4	12.7	16.3	33.0	53.4	

# APMP reference no. APMP.EM-K6.a

NMIJ

Uncertainty budget of the ac-dc voltage transfer difference measurement														
influence quantity	Type	u	Standard measurement uncertainty u in 10 <sup>-6</sup> at frequencies											
			1kHz	degree	20kHz	degree	50kHz	degree	100kHz	degree	500kHz	degree	1MHz	degree
reference		u(δs)	0.4		0.4		0.4		0.6		2.5		8.0	
Thomson effect	A	u(δTha)	0.2	10	0.2	10	0.2	10	0.2	10	0.2	10	0.2	10
	B	u(δThb)	0.3	Inf.	0.3	Inf.	0.3	Inf.	0.3	Inf.	0.3	Inf.	0.3	Inf.
reactive components and skin effect	B	u(δL,C,S)	0.0	Inf.	0.0	Inf.	0.02	Inf.	0.08	Inf.	1.93	Inf.	7.7	Inf.
connectors	B	u(δcon)	0.0	11	0.08	11	0.2	11	0.5	11	1.6	11	2	11
different measurement		u(δd)	0.4		0.4		0.5		0.7		2.5		6.2	
standard deviation	A	u(δa)	0.3	31	0.3	31	0.3	31	0.3	31	0.3	31	0.3	31
resolution of DVM	B	u(δr)	0.16	31	0.16	31	0.16	31	0.16	31	0.16	31	0.16	31
thermal noise	B	u(δtn)	0.09	31	0.09	31	0.09	31	0.09	31	0.09	31	0.09	31
DC offset	B	u(δoff)	0.1	31	0.1	31	0.1	31	0.1	31	0.1	31	0.1	31
stability of AC output	B	u(δsta)	0.15	31	0.15	31	0.15	31	0.15	31	0.15	31	0.15	31
index measurements	B	u(δi)	0.1	31	0.1	31	0.1	31	0.1	31	0.1	31	0.1	31
Reproducibility	B	u(δR)	0.12	6	0.12	6	0.17	6	0.23	6	0.58	6	0.87	6
connectors and T	B	u(δc,T)	0.0	11	0.08	11	0.2	11	0.5	11	1.6	11	2.00	11
AC adjustment	B	u(δad)	0.0	4	0.0	4	0.0	4	0.0	4	0.0	4	0.29	4
Grounding	B	u(δG)	0.0	11	0.0	11	0.0	11	0.07	11	1.73	11	5.77	11
Standard measurement uncertainty		u(δx) /Effective	0.6	193	0.6	206	0.6	182	0.9	60	3.5	77	10.1	100
expanded uncertainty for confidence level of 95%		U	1.1		1.1		1.3		1.9		7.1		20.2	

Remarks:  $u^2(\delta x) = u^2(\delta s) + u^2(\delta d)$

NMIT

Unit	Repeatability of meas	Calibrat of Holt 20	Drift of Standard	Calibrat of Sens	Drift in Temp drift	Drift in Hum drift	Linearity of Ac-dc	Error of Connector	Dist and Noise	EMI and RFI	Drift in Freq setting	Rounding off Uncert	Resolution of DMM	Stability of UUC	Ue																	
	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>	1*10 <sup>-6</sup>																		
Dist.	Normal	Normal	Rect	Normal	Rect	Normal	Rect	Normal	Rect	Normal	Rect	Normal	Rect	Rect																		
Divisor	1	2	√3	1	√3	√3	√3	2	√3	√3	1	√3	√3	√3																		
Ci	1	1	1	1	1	1	1	1	1	1	1	1	1	1																		
Vi	9																															
Freq (Hz)	Value	ur	Value	us	Value	du	Value	user	Value	ut	Value	uhum	Value	ulin	Value	ucon	Value	udis	Value	ueml	Value	ufreq	Value	uro	Value	ures	Value	ustb	uc	neff	k	1*10 <sup>-6</sup>
1 k	0.11	0.11	1.8	0.9	0.80	0.5	0.1	0.1	1	0.58	1	0.58	1	0.58	1	0.58	1	0.58	0.2	0.2	1	0.58	1	0.58	2.3	1.3	2.3	2E+06	2.000	5		
20k	0.13	0.13	2.5	1.3	0.35	0.2	0.1	0.1	1	0.58	1	0.58	1	0.58	1	0.58	1	0.58	0.4	0.4	1	0.58	1	0.58	4.3	2.5	3.2	3E+06	2.000	6		
50k	0.1	0.11	5.8	2.9	0.55	0.3	0.1	0.1	1	0.58	1	0.58	1	0.58	1	0.58	1	0.58	0.4	0.4	1	0.58	1	0.58	2.6	1.5	3.6	1E+07	2.000	7		
100k	0.19	0.19	8.2	4.1	0.35	0.2	0.1	0.1	1	0.58	1	0.58	1	0.58	1	0.58	1	0.58	0.7	0.7	1	0.58	1	0.58	5.0	2.9	5.3	6E+06	2.000	11		
500k	0.4	0.37	18	9	0.45	0.3	0.1	0.1	1	0.58	1	0.58	1	0.58	1	0.58	1	0.58	0.7	0.7	1	0.58	1	0.58	6.0	3.5	9.8	4E+06	2.000	20		
1M	0.3	0.33	28	14	0.34	0.2	0.1	0.1	1	0.58	1	0.58	1	0.58	1	0.58	1	0.58	0.6	0.6	1	0.58	1	0.58	3.2	1.8	14.2	3E+07	2.000	28		

KRISS

Source of Uncertainty	Symbol	Degrees of freedom	Standard uncertainty (μV/V) (k=1)					
			1kHz	20 kHz	50 kHz	100 kHz	500 kHz	1 MHz
1. Standard TVC	$u_{B1}$	∞	1.4	1.4	1.6	1.6	5.9	11.6
2. Uncertainty from N value	$u_N$	24	0.02	0.01	0	0.01	0.04	0.05
3. Repeated measurements	$u_{AP}$	96	0.41	0.4	0.4	0.5	0.64	0.79
combined standard uncertainty	$u_C$		1.5	1.5	1.6	1.7	5.9	11.6
effective degrees of freedom	$\nu_{eff}$		15391	16856	27744	12129	709795	#####
Expanded uncertainty(k=2)	$U$		2.9	2.9	3.3	3.4	11.9	23.3

# APMP reference no. APMP.EM-K6.a

VMI

Componet		Applied	Type	Distribution	v	1kHz	20kHz	50kHz	100kHz	1MHz	Note
Reference TVC (s/n: 503-2001)	$u(\delta_{Ref})$	3 V	B	Normal	30	1.2	1.6	3.4	4.6	15.5	From report          $(\Delta n_x / n_x) \cdot \delta_{iut}$ $(\Delta f / f) \cdot \delta_{iut}$
Connectors	$u(\delta_{conn})$		B	Normal	15	1	2	4	4	10	
Drift in Ref TVC /year	$u(\delta_{RefDrift})$		B	Rectangular	20	1.0	1.0	3.0	3.0	15	
ESDM	$u(\delta_A)$		A	Normal	4	0.3	0.3	0.2	0.4	0.4	
Temperature/Humidity	$u(\delta_{T,H})$		B	Normal	20	1	2	4	4	20	
Sensitivity Calculation	$u(\delta_n)$		B	Normal	25	0.1	0.1	0.1	0.1	0.1	
Frequence Setting	$u(\delta_f)$		B	Normal	20	0.1	0.1	0.1	0.1	0.1	
IUT Stability	$u(\delta_{IUT Stab})$		B	Normal	20	0.5	0.5	1	2	10	
Rounding off values	$u(\delta_{round val})$		A	Rectangular	1000	0.06	0.06	0.06	0.06	0.6	
Rounding off uncertainty	$u(\delta_{round unc})$		A	Rectangular	1000	0.06	0.06	0.06	0.06	0.6	

KIM-LIPI

ref=A55-2v

iut=A55-3v

A55-2v certificate from NML (ppm) =>Ref.:RN 43027											
1 kHz		20 kHz		50 kHz		100 kHz		500 kHz		1 MHz	
Diff	Uncert	Diff	Uncert	Diff	Uncert	Diff	Uncert	Diff	Uncert	Diff	Uncert
2.2	2.5	5.7	3.2	10.7	6.2	15.2	8.7	35.0	19.0	48.0	30.0

Build up results from 2v to 3v (ppm)											
1 kHz		20 kHz		50 kHz		100 kHz		500 kHz		1 MHz	
iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert
-4.4	0.5	-6.6	0.2	-9.1	0.4	-11.4	0.4	-18.9	0.3	-24.1	0.4
		ESDM =>									
	0.2		0.1		0.2		0.2		0.1		0.2

A55-3v corrected (ppm)											
1 kHz		20 kHz		50 kHz		100 kHz		500 kHz		1 MHz	
iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert
-2.2	2.5	-0.9	3.2	1.6	6.2	3.8	8.7	16.1	19.0	23.9	30.0

ref=A55-3v

iut=Holt-4v

Build up results from 3v to 4v (ppm)											
1 kHz		20 kHz		50 kHz		100 kHz		500 kHz		1 MHz	
iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert
-2.6	0.4	-2.0	0.4	-1.6	0.2	-0.7	0.5	1.4	0.4	-3.1	0.4
		ESDM =>									
	0.2		0.2		0.1		0.2		0.2		0.2

Holt-4v corrected											
1 kHz		20 kHz		50 kHz		100 kHz		500 kHz		1 MHz	
iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert	iutcor	iutuncert
-4.8	2.5	-2.9	3.2	0.0	6.2	3.1	8.7	17.5	19.0	20.8	30.0
		iut exp unc ==>									
	5		6		14		21		44		73







