



Final report

SIM.M.FF-S9.2016

Water flow: 10 m³/h ... 130 m³/h

Pilot laboratory #1: PTB Physikalisch-Technische Bundesanstalt
Department of Liquid Flow
Bundesallee 100
D-38116 Braunschweig
Germany

Pilot laboratory #2: CENAM Centro Nacional de Metroología
Dirección de Metrología de Flujo y Volumen
km 4.5 carretera a los Cués
El Marqués, Querétaro
Mexico, 76246

Coordinator Carl Felix Wolff - PTB
Phone: +49- (0)531 - 592 8211
Email: carl.f.wolff@ptb.de

Participants PTB - Enrico Frahm
CENAM - Roberto Arias Romero, Manuel Maldonado
CISA, Chile - Jeny Vargas Angel
IBMETRO, Bolivia - Juan José Mendoza Aguirre
INACAL, Perú - Adriel Arredondo
INTI, Argentina - Marcelo Alejandro Silvosa

Authorship **Enrico Frahm - PTB**
Phone: +49 (0)531 - 592 1333
Email: enrico.frahm@ptb.de
Roberto Arias Romero - CENAM
Phone: +52 - 442 - 211 0571
Email: mmaldona@cenam.mx, rarias@cenam.mx

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1 Summary

The objective of the Supplementary Comparison (SC) SIM.M.FF-S9 for water flow measurement was to support and prove the Calibration and Measurement Capabilities (CMC) of the participating NMIs of Chile (CISA), Peru (INACAL), Bolivia (IBMETRO) and Argentina (INTI). As pilot laboratories, the national metrology institutes of Germany (PTB) and CENAM (Mexico) supported the comparison with reference values. The comparison was organized as a single round robin, started in January 2016 at PTB and finished in August 2019, also at PTB. A combined setup of a turbine meter and Coriolis meter was used as a transfer standard. The nominal calibration conditions of the SC were defined in the flow range between 10 m³/h and 130 m³/h, 20 °C fluid temperature and 3 bar line pressure.

In order to estimate the uncertainties u_{TS} , both transfer meter were subjected to extensive characterisation measurements at pilot laboratory PTB. The following parameters were researched in detail: fluid temperature, line pressure, reproducibility, flow stability and meter sensitivity to different inflow conditions. The E_N values for turbine meter were calculated based on PTB data, only. The E_N values for Coriolis meter are partly linked to Key Comparison CCM.FF-K1.2015 and were calculated by using a common reference value of PTB and CENAM data.

The uncertainty of turbine meter u_{TS} was clearly dominated by the sensitivity to disturbed inflow conditions which leads to large values of u_{TS} with > 0.20 %. Beside one calibration, all labs passed the E_N criteria of ≤ 1.20. But, due to large values of u_{TS} , the calibrations for all labs were evaluated as inconclusive. The evaluation criteria u_{comp}/u_{base} exceeded the critical value of 2.00 for all calibrations. Finally, the turbine meter was not suitable for a confirmation of the submitted CMC values.

The calibration results of Coriolis meter were characterized by a strong dependency on zero setting. The observed effect was adjusted for the data of both reference laboratories by introducing a new method for autozero correction. Maximum uncertainty values for Coriolis u_{TS} were estimated with 0.069 % at low flowrates and 0.033 % at high flowrates. Beside two calibrations, all laboratories complied with the E_N criteria of < 1.20. In contrast to turbine meter, the evaluation criteria u_{comp}/u_{base} exceeded the critical value of 2.00 at one calibration, only. In consequence, the calibrations by using Coriolis meter were suitable for a confirmation of the submitted CMC values.

In summary, the comparison was successfully finished for a confirmation of the submitted CMC values, related to mass calibrations. For volume related CMC's this comparison was not suitable.

Acknowledgements

We would like to thank all participants for taking part within this comparison and for their support. This round robin would not be possible without all your help, discussions and organization. Our acknowledgements include all participating staff of the laboratories - scientists, technicians and administration.

A special thank goes to Carl Felix Wolff - (PTB - International Cooperation Department) who supported the comparison by his organizing and his maintaining contact with the partners.

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2 Introduction and objective

The objective of the Supplementary Comparison SIM.M.FF-S9 for water flow measurement was to support and prove the Calibration and Measurement Capabilities (CMC) of the participating National Metrology Institutes as part of the CIPM MRA (<http://kcdb.bipm.org>).

The CMC-values of participating laboratories (Table 1) were evaluated by establishing a "Supplementary Comparison Reference Value" (SCRV) and the Degree of Equivalence (E_N) between laboratories and SCR.V.

The basic subject of the calibrations was to determine the meter K -factor of the transfer flowmeters.

Depending on the operating principle of the used transfer meters, following meter- K -factors were the subject of measurements and had to be determined during calibrations:

Meter #1:

Turbine flowmeter volume-related frequency output:
 K_V (pulses/unit volume)

Meter #2:

Coriolis flowmeter:

- a) mass-related frequency output:
 K_m (pulses/unit mass)
- b) volume-related frequency output:
 K_V (pulses/unit volume)

3 Participants and measurement schedule

Participant list and measurement schedule are presented in Table 1. After three years of preparation, the comparison officially started in January 2016.

Table 1: Participant list and measurement periods of standard calibration program (day #1 until day #3 of Table 4), * pilot laboratories. Additional calibrations at pilot laboratory PTB are listed in Table 6.

NMI	Country	RMO	Contact	Calibration period
PTB*	Germany	EURAMET	enrico.frahm@ptb.de	13.01. - 15.01.2016
CISA	Chile	SIM	j.vargas@ci-sa.com	28.04. – 04.05.2016
INACAL	Peru	SIM	cochoa@inacal.gob.pe	13.03. – 16.03.2017
IBMETRO	Bolivia	SIM	fespejo@ibmetro.org	01.03. – 05.03.2018
INTI	Argentina	SIM	marsil@inti.gob.ar	06.12. – 14.12.2018
CENAM*	Mexico	SIM	rarias@cenam.mx	03.06. – 05.06.2019
PTB*	Germany	EURAMET	enrico.frahm@ptb.de	08.08. – 12.08.2019

4 Description of the transfer standard

4.1 Transfer meter setup

The transfer meter setup (Figure 1) consisted a turbine flowmeter (Figure 2) at the inflow and a Coriolis flowmeter (Figure 3) at the outflow. The technical details of the meters are listed in Table 2 and Table 3. For flow conditioning, tube bundles were installed before and after turbine meter. Beside the two transfer flowmeters, all additional items were provided by pilot laboratory (PTB):

- Pipework for meter installation (Figure 4)
- Cables for connecting transfer meters and the auxiliary devices to electronic boxes
- Electronic box (Figure 5).

In order to provide optimum reproducibility conditions, the flowmeters and the inter-connecting pipework were equipped with pin-in-hole alignment capabilities. All elements of pipework were manufactured in stainless steel.

In addition to the used flowmeters, auxiliary measurands for diagnostic purposes were included in the transfer meter setup:

- Water density (based on a signal delivered by the Coriolis flowmeter)
- Fluid temperature by temperature transmitter
- Fluid pressure by pressure transmitter
- Pressure drop across the turbine meter by differential pressure transmitter

A detailed description of the setup is given in the Technical Protocol of this SC [1].

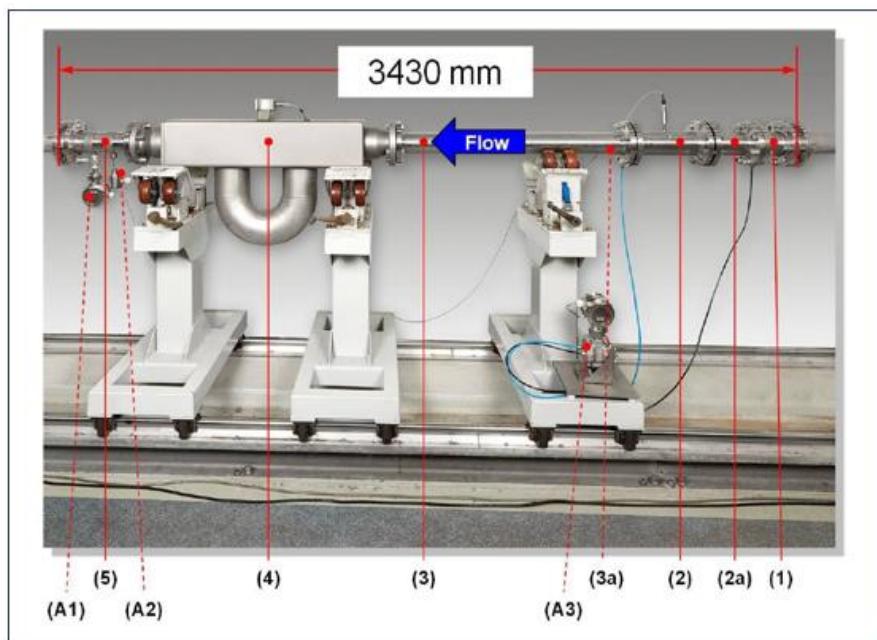


Figure 1: Transfer meter setup and pipework - Sample installation at pilot laboratory

- | | |
|--|--|
| (1) Inlet pipe section | (2) Turbine meter |
| (2a) Tube-bundle flow conditioner dedicated to the turbine | |
| (3) Connecting pipe section | (3a) Integrated tube-bundle flow conditioner |
| (4) Coriolis flowmeter | (5) Outlet pipe section |
- Auxiliary devices:*
- | |
|--|
| (A1) Pressure transmitter |
| (A2) Temperature transmitter |
| (A3) Differential pressure transmitter |

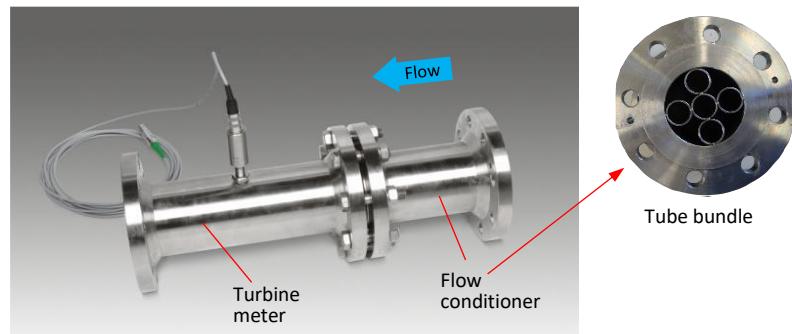


Figure 2: Transfer meter #1 - Turbine meter, DN80 mm



Figure 3: Transfer meter #2 - Coriolis flowmeter, DN80 mm

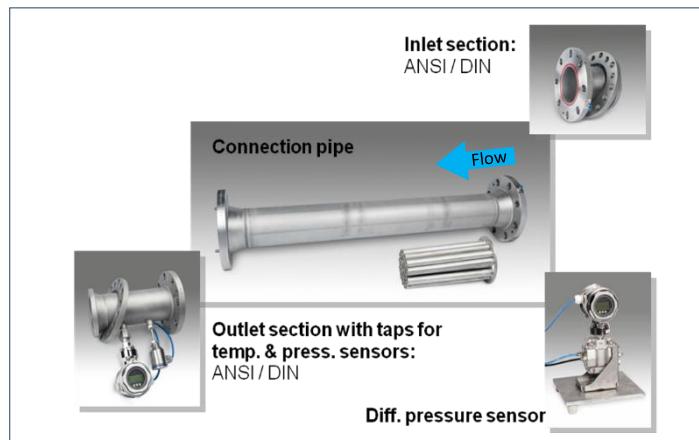


Figure 4: Transfer setup – pipework

Table 2: Transfer meter #1 - Turbine flowmeter (Figure 2)

Manufacturer:	KEM Küppers Elektromechanik GmbH	Germany
Type:	HM 080.71.FDE040-TS15-D	
Serial No.:	01130721	
Pipe size:	DN80	Nominal: 80 mm
Signal pick-up:	Type: VTE*/P-Ex Carrier-frequency pulse amplifier Serial No.: 02497623	Signal voltage: ca. 24 V
Output signal:	Frequency	(0 Hz) ... 450 Hz (at 240 m³/h)
	Nominal meter K -factor: $K_{V,nom}$	11.4850 pulses/L
Additional equipment:	Tube-bundle flow conditioner	Permanently installed at the inflow to meter

Table 3: Transfer meter #2 - Coriolis flowmeter (Figure 3)

Manufacturer:	Rota Yokogawa GmbH & Co KG	Germany
Type:	ROTAMASS	
Serial No.:	D1K601386 (flow sensor) D1K601375 (flow transmitter and indicator)	
Pipe size:	DN80	Nominal: 80 mm
Signal output #1:	Mass-flowrate related: frequency	0 kHz ... 10 kHz
	Nominal meter K-factor: $K_{m,nom}$	144.056 pulses/kg
Signal output #2:	Volume-flowrate related: frequency	0 kHz ... 10 kHz
	Nominal meter K-factor: $K_{V,nom}$	28.800 pulses/L
Signal output #3:	Fluid density: current signal	4 mA ... 20 mA

4.2 Additional data logging

For the reported SC an additional datalogging system was designed. Beside standard impulse logging of the laboratory, an electronic device was provided by the pilot laboratory (PTB) for a separate and independent data recording. Basically, electric pulses from transfer meters and additional process parameter, measured by the auxiliary devices (chapter 4.1), were logged by the electronic box (Figure 5). Also, power supply of the measurement instruments was provided by the box. The detailed use of the electronic box is described in SC Technical Protocol [1].

The electronic box was developed as a parallel working system, which does not affect the standard impulse count recording of the laboratories.

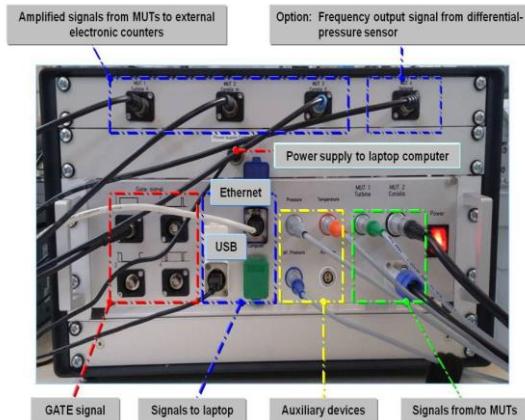


Figure 5: Front side of the electronic box - Connectivity to MUTs, external electronic counters and laptop computer

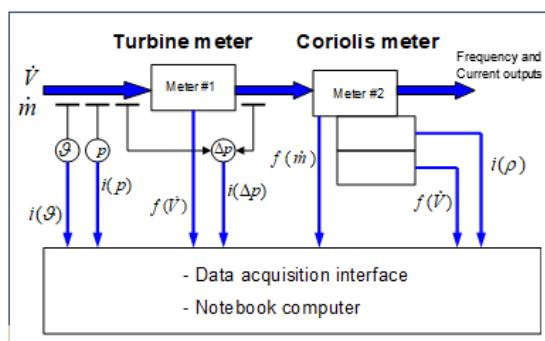


Figure 6: Electronic box - signal acquisition

5 Measurement program

5.1 Calibration program at participating laboratories

The objective of the measurement program was to verify the CMC entries of the participating laboratories. Therefore, it was necessary for all laboratories to calibrate the setup under comparable measurement conditions. All participants were asked to calibrate the transfer setup as far as possible under the following SC reference conditions.

SC reference conditions:

Fluid temperature: 20 °C

Line pressure: 3 bar (measured as positive back pressure after Coriolis meter)

Nominal flowrates: listed in Table 4

Setup: using the complete SC setup (Figure 1).

Table 4: Main tasks and flowrates of calibration days in participating laboratories as defined in SC Technical Protocol [1]

Calibration day	Main task	Preparations before calibration	Autozero setting at Coriolis meter	Repeated measurements	Nominal flowrate	Post-processing
Day #1	Lab-to-lab reproducibility	Installation of transfer meters	yes	5	10, 30, 60, 100, 130	Transfer package remains in calibration line
Day #2	Main calibration of KC1 and Day-to-day reproducibility	-	no	5	10, 30, 60, 100, 130	Transfer package remains in calibration line
Day #3	Repeatability at selected flowrates	-	no	10	30, 60, 130	Transfer package is removed from calibration line

5.2 Calibration methods and uncertainties of participating laboratories

During SC each laboratory had to calibrate the setup by using their standard calibration method, which was subjected to the CMC entry (Table 5). Each laboratory provided the pilot laboratory with a description of the calibration procedure and an overview to the used calibration rig (Chapter 11.1.) All laboratories had an independent traceability in realization of their standards.

Table 5: Participating laboratories, calibration methods and CMC-values within the range of SC flowrates

NMI/DI	Country	Calibration method and reference	CMC Water CIPM MRA Database ($k = 2$)	
			$U(\text{Mass})$	$U(\text{Volume})$
PTB	Germany	Gravimetric / flying-start-stop	0.020	0.020
CISA	Chile	Gravimetric / flying-start-stop	0.150	0.150
INACAL	Peru	Gravimetric / flying-start-stop	0.076	0.076
IBMETRO	Bolivia	Master meter / flying-start-stop	0.100	0.100
INTI	Argentina	Volumetric tank / standing-start-stop (10 m³/h until 60 m³/h)	0.070	0.060
		Master meter / standing-start-stop (100 m³/h until 130 m³/h)	0.220	0.200
CENAM	Mexico	Gravimetric / flying-start-stop	0.030	0.038

5.3 Meter characterisation at pilot laboratory (PTB)

The transfer setup was subjected to extensive characterisation measurements at pilot laboratory (Table 6). These calibrations were made under clearly defined conditions, which are basically derived from SC reference conditions (Chapter 5.1). The goal of the characterisation measurements was to analyze the impact of the following parameters to transfer meter setup: fluid temperature, line pressure and reproducibility. The results aimed in a detailed knowledge about meter uncertainties u_{TS} . Additionally, a strong dependency of turbine meter characteristics to different inflow condition was assumed (Chapter 7.6). In order to consider this type of effects, data of KC1 calibrations were used within the presented SC report. During KC1 calibration an identical turbine meter was used, but with an inner diameter of 100 mm instead of 80 mm. For a simulation of real inflow conditions, the KC1 transfer setup was calibrated with several flow disturber (Figure 7) and different inflow lengths (Figure 8).

Table 6: Characterisation measurements at pilot laboratory

Task of calibrations	Nominal flowrate	Temperature	Line pressure	Repeated measurements	Measurement periods at pilot laboratory
	m ³ /h	°C	bar		
Temperature dependency	10, 30, 60, 100, 130, 150	10, 15, 20, 25, 30	3	5	16.06.2015 - 02.07.2015
Pressure dependency	10, 30, 60, 100, 130, 150	20	2, 3, 4	5	01.09.2015 - 03.09.2015
Long term reproducibility	10, 30, 60, 100, 130	20	3	5	25.11.2015
Inflow conditions (with DN100 setup of KC1)	30, 100, 200	20	3	5	03/2019 during KC1 calibrations



Figure 7: Used flow disturber for meter characterisation during KC1 - inner pipe diameter: 100 mm

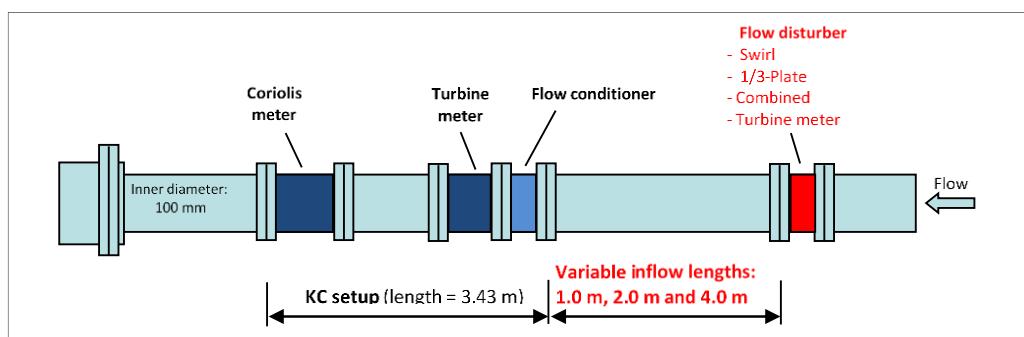


Figure 8: Calibration setup for meter characterisation during KC1 using several flow disturber and inflow lengths

6 Data calculation and evaluation criteria

6.1 Meter K-factor and temperature correction for final meter error x_i

According to the flowrates of Table 4, the meter K -factor was calculated for each calibration by using Equation (1) for turbine meter and, respectively, by Equation (2) for Coriolis meter.

$$K_V = \frac{N}{(V_{\text{ref}} \cdot 1000)} \quad (1)$$

$$K_m = \frac{N}{m_{\text{ref}}} \quad (2)$$

where	K_V	- K -factor of turbine meter (pulses/L)
	K_m	- K -factor of Coriolis meter (pulses/kg)
	N	- Counted number of pulses by the transfer meter (pulses)
	V_{ref}	- Volume, measured by the reference standard (m^3)
	m_{ref}	- Mass, measured by the reference standard (kg)

The relative measurement error e was calculated for each K -factor by:

$$e_V = \frac{K_V - K_{V,\text{nom}}}{K_{V,\text{nom}}} \cdot 100 \% \quad (3)$$

$$e_m = \frac{K_m - K_{m,\text{nom}}}{K_{m,\text{nom}}} \cdot 100 \% \quad (4)$$

where	e_V	- Relative measurement error of turbine meter – volume (%)
	e_m	- Relative measurement error of Coriolis meter - mass (%)
	$K_{V,\text{nom}}$	- Nominal K -factor of turbine meter (pulses/L)
	$K_{m,\text{nom}}$	- Nominal K -factor of Coriolis meter - mass output (pulses/kg)

6.2 Postprocessing of reported data and estimation of relative meter error x_i

Autozero correction of Coriolis data

The data of Coriolis meter were characterized by a strong drift in meter error. Especially at low flowrates, the meter showed differences of up to 1.33 % between calibration periods 2016 and 2019 (Figure 9). This observed drift was interpreted as an instability of meter autozero setting, which was confirmed by manufacturer of the meter [2]. Data of the turbine meter, which were recorded at the same time, did not show such a highly drift at low flowrates (Figure 13). Additionally, the recorded autozero value of the Coriolis meter was +59.615 kg/h during calibrations in 2016 and, respectively, -92.115 kg/h in 2019, which do underline the discussed autozero instability.

In consequence, a correction of Coriolis data was introduced as followed. The differences between flowrates of Coriolis meter and lab reference were calculated and plotted against reference flowrate itself (Figure 10). The interception term of the fitted linear function was detected as the "zero missetting" value, separately for each calibration day, but over full flow scale (Table 7). The original flowrates of Coriolis meter were corrected by this method and a new meter error was calculated (Figure 11).

This method is based on the following two assumptions: The Coriolis meter is a linear device and the non-linear characteristics of the results in Figure 9 were not caused by leakage effects of the calibration facility. Both pilot laboratories can guarantee the nonexistence of leakage during reported calibrations, which was verified by previous comparisons (e.g. CCM-K1.2015). In consequence, the **correction method was only applied to the results of pilot laboratories**.

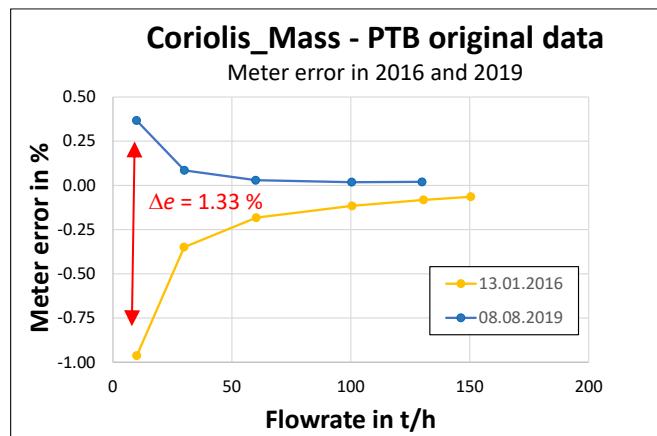


Figure 9: Meter drift of Coriolis_Mass - original PTB data of day #1 in 2016 and 2019

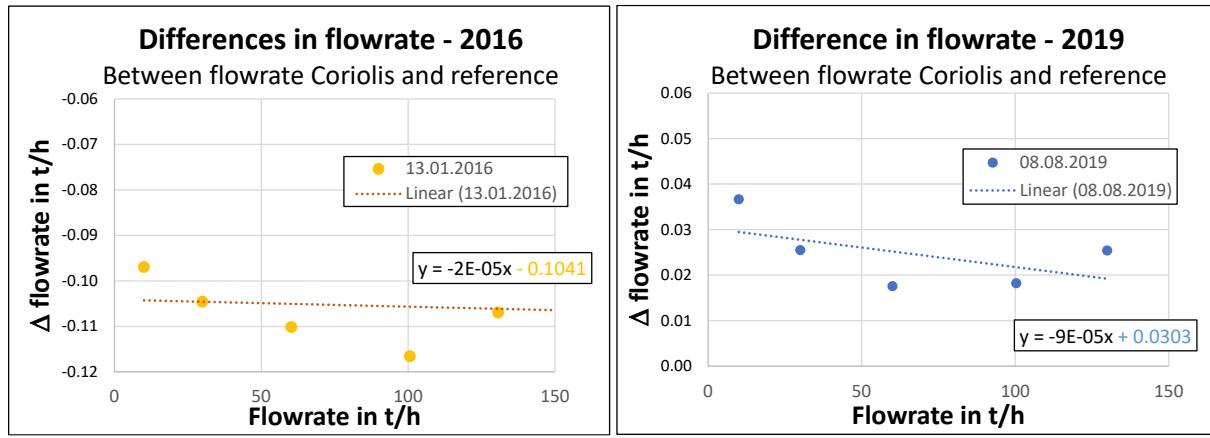


Figure 10: Example of differences in flowrate between Coriolis and reference data - original PTB data of day #1 in 2016 and 2019; interception value of fitted linear function for correction of Coriolis data

Table 7: Correction values for Coriolis_Mass data, based on autozero discussion and estimated interception, e.g. in Figure 10

Pilot laboratory and calibration period	Correction value for Coriolis_Mass flowrate		
	Day #1	Day #2	Day #3
	t/h	t/h	t/h
PTB_1 in 01/2016	-0.104	-0.084	-0.068
PTB_2 in 08/2019	0.030	0.039	0.065
CENAM in 06/2019	-0.003	-0.008	-0.015

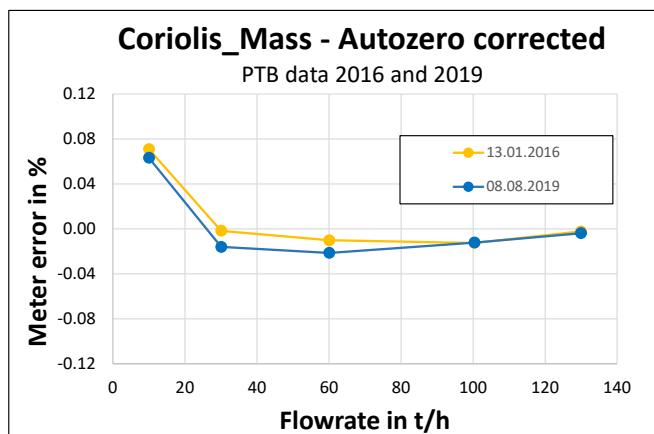


Figure 11: Example of autozero corrected final Coriolis_Mass data - PTB of day #1 in 2016 and 2019

Temperature correction

Both transfer meters showed a systematic temperature dependency in meter error (Section 7.3). All reported meter error of participated laboratories, including autozero corrected data of pilot laboratories, were corrected by applying Equation (22) until Equation (25) and Table 15, to aim a temperature corrected meter error $e_{v,cor}$ for volume and $e_{m,cor}$ for mass.

For final evaluation by E_N values, a mean meter error (x_i) was calculated separately for each laboratory, transfer meter and flowrate (Equation 5), based on calibration results of day #1 and day #2 (Table 4).

$$x_i = \frac{\sum_{k=1}^n (e_{cor,k})}{n} \quad (5)$$

where

- x_i - Temperature corrected meter error for E_N -value evaluation
- n - Number of measurements at calibrated test point
- i - Laboratory index

6.3 Uncertainty $u_{x,i}$ of reported and temperature corrected values x_i

As described in [2], [3] and [4], the uncertainty of reported values x_i include uncertainties introduced by the participant's flow reference ($u_{base,i}$), by transfer meter (u_{TS}) and by repeatability of the reported values (Equation 6). The used input parameter of $u_{base,i}$ do represent the CMC values of Table 5 which were under evaluation during this comparison. Uncertainty calculations of u_{TS} were based on Equation (18), for Turbine meter, respectively, for Coriolis meter on Equation (19). Final values of u_{TS} are given in Table 10 and Table 11. The term $\frac{s}{\sqrt{n}}$ (Equation 6) represents the repeatability of measurements made in the participating laboratory [3], based on calibration results of day #1 and day #2 (Table 4).

$$u_{x,i} = \sqrt{u_{base,i}^2 + u_{comp}^2} = \sqrt{u_{base,i}^2 + u_{TS}^2 + \frac{s^2}{n}} \quad (6)$$

where

- $u_{x,i}$ - Uncertainty of reported and temperature corrected meter error (%)
- $u_{base,i}$ - Uncertainty of laboratory reference, here it is equal to CMC_i (%)
- u_{comp} - Uncertainty of transfer meter measurements (%)
- u_{TS} - Uncertainty of transfer meter (%)
- s - Standard deviation of the mean of measurements at one flowrate point (%)

All values of u are valid for $k = 1$.

6.4 Coriolis meter - Method for E_N value calculation and linkage to KC1

6.4.1 Linkage of SIM comparison to Key Comparison KC1

The evaluation of Coriolis data is partly based on a linkage to key comparison CCM.FF-K1.2015 (KC1). The pilot laboratories CENAM and PTB took part in KC1 and supported the presented SIM comparison by the higher-ordered results of KC1 (Figure 12). The applied procedure is described in follow and was applied for Coriolis_Mass data only.

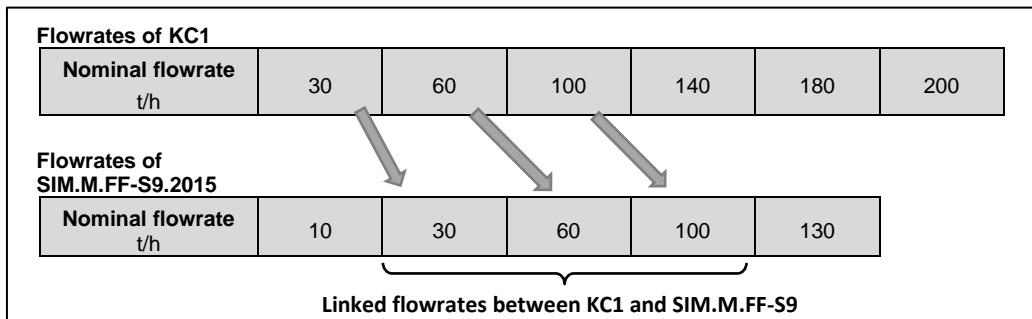


Figure 12: Linkage between comparison KC1 and SIM.M.FF-S9

SCC_i - Supplementary comparison correction value

$$SCC_i = x_{KC1,i} - KCRV \quad (7)$$

where

- SCC_i - Supplementary comparison correction for laboratory i (%)
- $KCRV$ - Key Comparison Reference value of KC1 (%)
- $x_{KC1,i}$ - Results of laboratory i during KC1 (%)

Uncertainty of SCC_i

$$u(SCC_i) = \sqrt{u_{x,KC1,i}^2 + u_{KCRV}^2} \quad (8)$$

where

- $u_{SCC,i}$ - Uncertainty of SCC for laboratory i (%)
- $u_{x,KC1,i}$ - Uncertainty of calibration results of laboratory i during KC1 (%)
- u_{KCRV} - Uncertainty of KCRV during KC1 (%)

Table 8: Input parameter and results of SCC_i for PTB, based on KC1 data

Nominal Flowrate	$KCRV$	$u(KCRV)$	$x_{KC1,i}$	$u(x_{KC1,i})$	SCC_i	$u(SCC_i)$
$k = 1$	$k = 1$	$k = 1$	$k = 1$	$k = 1$	$k = 1$	$k = 1$
t/h	%	%	%	%	%	%
30	0.041	0.010	0.045	0.024	0.004	0.022
60	0.038	0.007	0.041	0.016	0.004	0.014
100	0.033	0.006	0.032	0.014	-0.001	0.013

Table 9: Input parameter and results of SCC_i for CENAM, based on KC1 data

Nominal Flowrate	$KCRV$	$u(KCRV)$	$x_{KC1,i}$	$u(x_{KC1,i})$	SCC_i	$u(SCC_i)$
$k = 1$	$k = 1$	$k = 1$	$k = 1$	$k = 1$	$k = 1$	$k = 1$
t/h	%	%	%	%	%	%
30	0.041	0.010	0.047	0.027	0.006	0.025
60	0.038	0.007	0.049	0.019	0.012	0.018
100	0.033	0.006	0.045	0.018	0.012	0.017

6.4.2 Supplementary Comparison reference value $SCRV_{Cor}$ and its uncertainty

The Supplementary Comparison Reference Value for Coriolis_Mass data was calculated following the procedure A of [6]:

Input data and uncertainties at linked flowrates of 30 t/h, 60 t/h and 100 t/h:

- ⇒ original data of CENAM and PTB were corrected by using SCC_i (Equation 9)
- ⇒ the uncertainties of the corrected value were calculated by using (Equation 10)

Input data and uncertainties at flowrates of 10 t/h and 130 t/h:

- ⇒ the results of equation (5) were used as $x_{Cor,i}$
- ⇒ the uncertainties of equation (5) were used as $u(x_{Cor,i})$

$$x_{Cor,i} = x_i - SCC_i \quad (9)$$

where

$x_{Cor,i}$ - By SCC_i corrected results of reference laboratory i during SIM comparison (%)

$$u(x_{Cor,i}) = \sqrt{u_{x,i}^2 + u_{SCC,i}^2} \quad (10)$$

where

$u(x_{Cor,i})$ - Uncertainty of $x_{Cor,i}$ for reference laboratory i during SIM comparison (%)

The reference value $SCRV_{Cor}$ was calculated for each flowrate as a weighted mean error of both reference laboratories, including standard uncertainties $u(x_{Cor,i})$ of the measurements as the weights:

$$SCRV_{Cor} = \frac{\left(\frac{x_{Cor,i}}{u_{x,Cor,i}^2} + \frac{x_{Cor,j}}{u_{x,Cor,j}^2} \right)}{\left(\frac{1}{u_{x,Cor,i}^2} + \frac{1}{u_{x,Cor,j}^2} \right)} \quad (11)$$

where

$SCRV_{Cor}$ - Reference value of the comparison for Coriolis_Mass meter (%)

The standard uncertainty $u(SCRV_{Cor})$ is given with:

$$\frac{1}{u_{SCRV,Cor}^2} = \frac{1}{u_{x,Cor,i}^2} + \frac{1}{u_{x,Cor,j}^2} \quad (12)$$

where

$u(SCRV_{Cor})$ - Standard uncertainty of $SCRV_{Cor}$ with $k = 1$ (%)

In equations 11 and 12, i stands for PTB and j for CENAM.

6.4.3 Determination of d_i and E_N -values

The differences of participating laboratories to $SCRV_{Cor}$ were calculated with Equation (13), the extended uncertainty of the difference with Equation (14). The final E_N values for comparison evaluation were calculated by using Equation (15).

$$d_i = SCRV_{Cor} - x_i \quad (13)$$

where

d_i - Degree of equivalence (DoE) as the difference of SIM-participant i to $SCRV_{Cor}$ (%)

Uncertainty of d_i

$$U(d_i) = 2 \cdot \sqrt{u_{x,i}^2 + u_{SCRV,Cor}^2} \quad (14)$$

where

$U(d_i)$ - Uncertainty of d_i of participant i during SIM comparison with $k = 2$ (%)

$E_{N,i}$ - value of participant

$$E_{N,i} = d_i / U(d_i) \quad (15)$$

where

$E_{N,i}$ - Normalized Degree of Equivalence as the difference of SIM-participant i to $SCRV_{Cor}$ (%)

6.5 Turbine meter - Method for E_N value calculation

6.5.1 Supplementary Comparison reference value $SCRV_{Turb}$ and it's uncertainty

The Supplementary Comparison Reference Value $SCRV_{Turb}$ for turbine meter is based on PTB data as the reference laboratory, only. Over full flow scale, the calibration results x_i (Equation 5) of PTB were used as $SCRV_{Turb}$ as well as the uncertainty $u(x_i)$ of PTB-data (Equation 6) were used as $u(SCRV_{Turb})$.

6.5.2 Determination of d_i and E_N -values

The differences of participants to $SCRV_{Turb}$ were calculated with Equation (13), the expanded uncertainty of the difference with Equation (17). The final E_N values for comparison evaluation were calculated by using Equation (15).

$$d_i = SCRV_{Turb} - x_i \quad (16)$$

where d_i - difference of SIM-participant i to $SCRV_{Turb}$ %

$$U(d_i) = 2 \cdot \sqrt{u_{x,i}^2 + u_{SCRV,Turb}^2} \quad (17)$$

where $U(d_i)$ - Uncertainty of d_i of participant i during SIM comparison with $k = 2$ (%)

6.6 Evaluation criteria of comparison data

For final data evaluation and decision table the following criteria were used - based on [3], [4] and [5]:

- The participant **passed the comparison if** $E_{N,i} \leq 1.0$ and $u_{comp}/u_{base} \leq 2$
The results of participating laboratory i agreed within 95 % confidence level uncertainty expectations with the $SCRV$ ($k = 2$).
- The participant passed the comparison at "**warning level**" if $1.0 < E_{N,i} \leq 1.2$ and $u_{comp}/u_{base,i} \leq 2$
- The comparison can not confirm the participant's uncertainty if $E_{N,i} \leq 1.2$ and $u_{comp}/u_{base,i} > 2$
The results were **inconclusive**, because the calibrations did not show sufficient low uncertainties to discern lab to $SCRV$ below certain level. The transfer meter and/or the calibrations were not suitable for a confirmation of the declared CMC values.
- The participant **failed the comparison if** $E_{N,i} > 1.2$
The results did indicate that the agreement was outside of uncertainty expectations.

7 Laboratory conditions, transfer meter characteristics and meter uncertainties

In accordance to the WGFF recommendation for comparison calculations [4], the standard uncertainty u_{TS} of the transfer meter is the root-sum-of-square (RSS) of several transfer meter characteristics. For this comparison the considered meter characteristics and input uncertainties of turbine meter are given in Equation (18), for Coriolis meter in Equation (19). The final values of u_{TS} were calculated separately for each flowrate (Table 10 and Table 11).

Note: The uncertainties of u_{TS} are specified and valid for the presented comparison under the given measurement conditions. The values of u_{TS} may change if the setup or calibration conditions do deviate to this comparison.

$$\text{Turbine meter: } u_{TS} = \sqrt{u_{\text{drift}}^2 + u_{\text{reprod}}^2 + u_{\text{temp}}^2 + u_{\text{pres}}^2 + u_{\text{flow}}^2 + u_{\text{inflow}}^2} \quad (18)$$

$$\text{Coriolis}_\text{Mass}: \quad u_{TS} = \sqrt{u_{\text{drift}}^2 + u_{\text{reprod}}^2 + u_{\text{temp}}^2 + u_{\text{pres}}^2 + u_{\text{flow}}^2} \quad (19)$$

where

- | | |
|---------------------|--|
| u_{drift} | - Uncertainty due to drift of transfer meter (%) |
| u_{reprod} | - Uncertainty due to reproducibility characteristics of transfer meter (%) |
| u_{temp} | - Uncertainty caused by temperature characteristics of transfer meter (%) |
| u_{pres} | - Uncertainty caused by pressure characteristics of transfer meter (%) |
| u_{flow} | - Uncertainty due to sensitivity of transfer meter to instable flow conditions (%) |
| u_{inflow} | - Uncertainty due to sensitivity of turbine meter to different inflow conditions (%) |

All values of u are expressed as $k = 1$.

Table 10: Final values of meter uncertainties u_{TS} for turbine meter (with $k = 1$)

Nominal flowrate	Meter uncertainty u_{TS} for turbine meter	Input uncertainties for u_{TS}					
		u_{drift}	u_{reprod}	u_{temp}	u_{pres}	u_{flow}	u_{inflow}
m^3/h	%	%	%	%	%	%	%
10	0.207	0.034	0.010	0.014	0.017	0.006	0.203
30	0.207	0.034	0.007	0.009	0.017	0.006	0.203
60	0.211	0.057	0.003	0.002	0.017	0.006	0.203
100	0.215	0.071	0.004	0.001	0.017	0.006	0.203
130	0.219	0.080	0.005	0.000	0.017	0.006	0.203

Table 11: Final values of meter uncertainties u_{TS} for Coriolis_Mass (with $k = 1$)

Nominal flowrate	Meter uncertainty u_{TS} for Coriolis_Mass meter	Input uncertainties for u_{TS}				
		u_{drift}	u_{reprod}	u_{temp}	u_{pres}	u_{flow}
t/h	%	%	%	%	%	%
30	0.069	0.040	0.024	0.043	0.029	0.006
60	0.056	0.010	0.010	0.045	0.029	0.006
100	0.035	0.008	0.010	0.013	0.029	0.006
140	0.032	0.006	0.009	0.004	0.029	0.006
180	0.033	0.010	0.010	0.006	0.029	0.006

7.1 Drift of transfer meter - uncertainty u_{drift}

The uncertainty due to meter drift u_{drift} was quantified by performing repeated calibrations at pilot laboratory #1 (Table 1 and Table 6), using the reference standard as described in Figure 1 under reference conditions of 3 bar and 20 °C fluid temperature. For each calibration period a mean value was calculated (Figure 13 and Figure 14). The final values of u_{drift} (Table 12) were calculated by using Equation (20), separately for each flowmeter and flowrate.

$$u_{\text{drift}} = \frac{\text{Max} (x_i) - \text{Min} (x_i)}{2 \cdot \sqrt{3}} \quad (20)$$

where

- u_{drift} - Uncertainty ($k = 1$) due to long term stability of transfer meter (%)
- x_i - Averaged and corrected meter error (%)

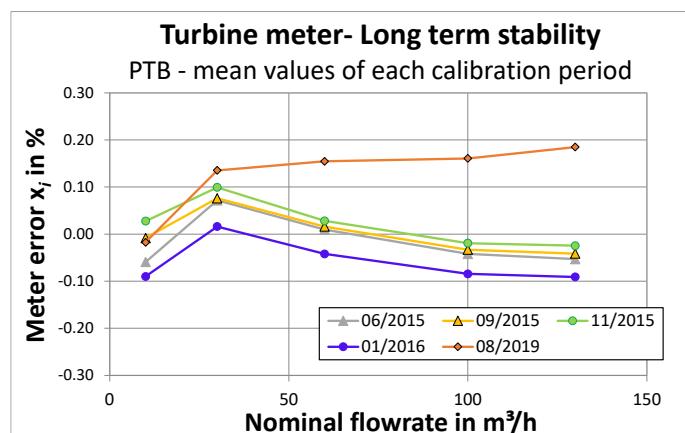


Figure 13: Long term stability of turbine meter - Mean values of corrected meter error x_i for each calibration period, measured at PTB laboratory under reference conditions of 3 bar line pressure and 20 °C fluid temperature

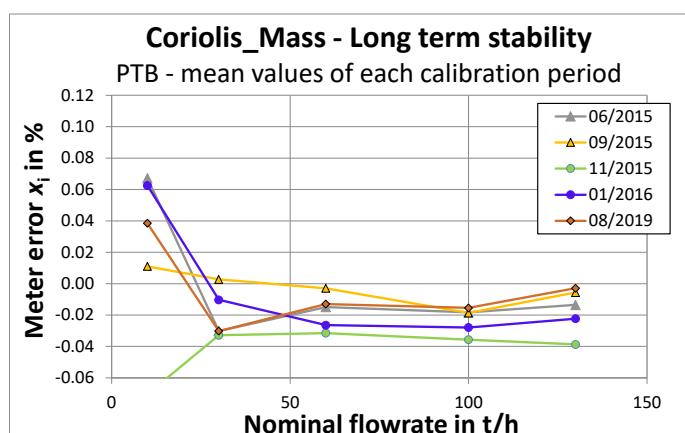


Figure 14: Long term stability of Coriolis_Mass - Mean values of corrected meter error x_i for each calibration period, measured at PTB laboratory under reference conditions of 3 bar line pressure and 20 °C fluid temperature

Table 12: Uncertainties u_{drift} caused by drift of meter error – turbine meter and Coriolis_Mass

	Nominal Flowrate				
	10 m³/h	30 m³/h	60 m³/h	100 m³/h	130 m³/h
u_{drift} Turbine meter in %	0.034	0.034	0.057	0.071	0.080
u_{drift} Coriolis_Mass in %	0.040	0.010	0.008	0.006	0.010

7.2 Quantification of reproducibility - uncertainty u_{reprod}

The uncertainty due to reproducibility characteristics u_{reprod} of the transfer meter were estimated at pilot laboratory, based on maximum values of long- and short-term reproducibility. For each period, a span of meter error $[\text{Max}(x_i) - \text{Min}(x_i)]$ was calculated (Figure 15). Because of non-normal distributed data, the uncertainty u_{reprod} was calculated separately for each flow rate by using maximum values of observed span (Equation 21). It was assumed that the final values of u_{reprod} (Table 13) did include the following sources of uncertainty: short term drift between calibration day #1 until day #3, residual uncertainty after correction of autozero (at Coriolis meter) and reassembly of the transfer setup.

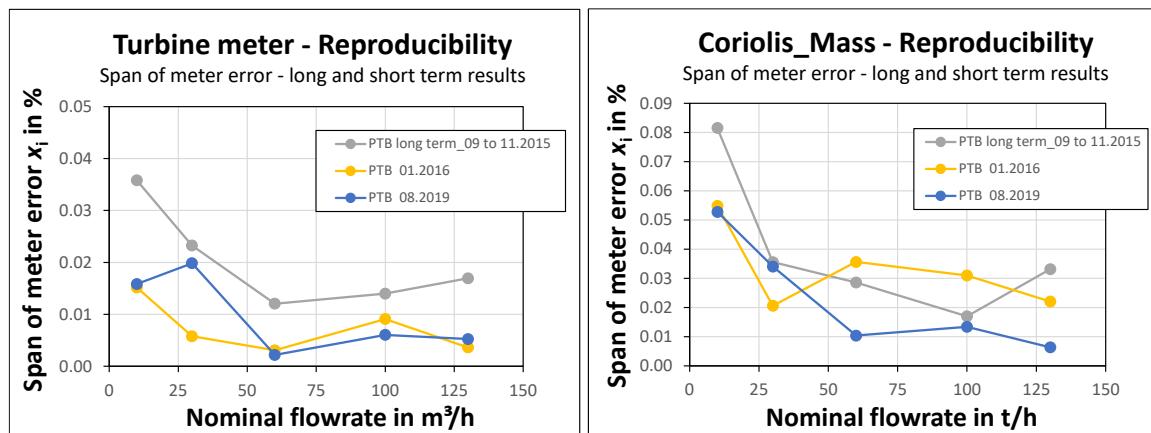


Figure 15: Results of reproducibility calibrations at pilot laboratory – Span of corrected meter error x_i (max - min) during each calibration period - measured at PTB laboratory under reference conditions of 3 bar line pressure and 20 °C fluid temperature

$$u_{\text{reprod}} = \frac{\text{Max} [\text{Max}(x_i) - \text{Min}(x_i)]}{2 \cdot \sqrt{3}} \quad (21)$$

where

u_{reprod} - Uncertainty ($k = 1$) due to reproducibility characteristics of transfer meter (%)

Table 13: Uncertainties u_{reprod} due to reproducibility characteristics of the transfer meters

$k = 1$	Nominal Flowrate				
	10 m³/h	30 m³/h	60 m³/h	100 m³/h	130 m³/h
u_{reprod} Turbine meter in %	0.010	0.007	0.003	0.004	0.005
u_{reprod} Coriolis_Mass in %	0.024	0.010	0.010	0.009	0.010

7.3 Temperature dependency - uncertainty U_{temp}

Laboratory conditions

During calibrations in participating laboratories, the span of fluid temperature ranged between 16.80 °C and 31.13 °C. The maximum variation of fluid temperature within one participating lab, expressed as $\max(T_{\text{fluid}}) - \min(T_{\text{fluid}})$, was reported with 5.99 °C (Table 14, Figure 16).

Table 14: Fluid temperatures T_{fluid} (°C) in participating laboratories during calibrations

NMI	PTB 1	CISA	INACAL	IBMETRO	INTI	CENAM	PTB 2
Max	20.01	25.39	31.13	21.10	24.00	28.12	20.22
Min	19.85	23.16	25.15	16.80	21.40	27.19	19.94
Max - Min	0.16	2.23	5.99	4.30	2.60	0.93	0.28
Mean	19.92	24.29	28.02	18.73	22.77	27.65	20.06

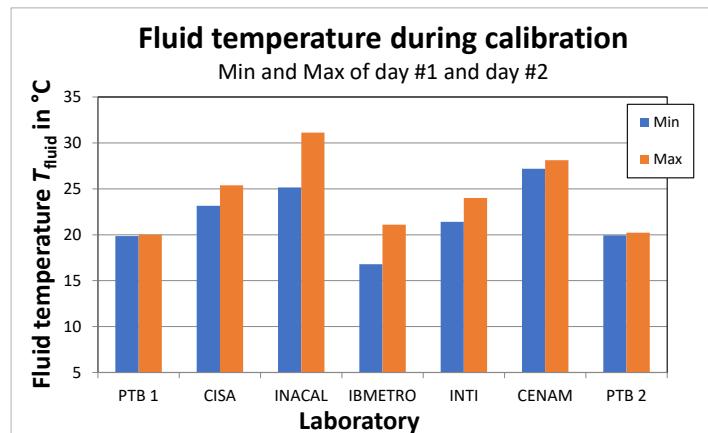


Figure 16: Fluid temperature T_{fluid} during calibrations in participating laboratories - Maximum and minimum of calibration on day #1 and day #2

Meter characteristics

The temperature characterisation measurements were realised in pilot laboratory (PTB) in 2015. The goal of characterisation measurements was to analyze meter error characteristics if the fluid temperature deviates from nominal temperature. All reported data were corrected by the following procedure, because both meters showed a distinctive dependency of meter error due to changes in fluid temperature (Figure 17).

The correction is based on the relationship between a) deviation ΔT_{Fluid} (Equation 22) of current fluid temperature T_{Fluid} to nominal temperature T_{nom} and b) deviation Δe_{nom} (Equation 23) of meter error at current temperature conditions e to meter error e_{nom} , calibrated at nominal temperature. The relationship between ΔT and Δe_{nom} was analyzed separately for each transfer meter by fitting a second-degree polynomial function using least squares fits (Figure 18 and Figure 19).

The resulting model parameter of Table 15 were used to calculate a correction value of meter error Δe_{cor} (Equation 24) and the final meter error e at current temperature conditions (Equation 25).

$$\Delta T_{\text{fluid}} = T_{\text{fluid}} - T_{\text{nom}} \quad (22)$$

where

ΔT_{fluid}	- Difference of current fluid temperature to nominal temperature of 20 °C (°C)
T_{fluid}	- Current fluid temperature (°C)
T_{nom}	- Nominal fluid temperature of 20 °C

$$\Delta e_{\text{nom}} = e - e_{\text{nom}} \quad (23)$$

where

Δe_{nom}	- Difference of meter error (%)
e	- Meter error at current temperature conditions (%)
e_{nom}	- Meter error at nominal temperature of 20 °C (%)

$$\Delta e_{\text{cor}} = a + b \cdot \Delta T_{\text{fluid}} + c \cdot \Delta T_{\text{fluid}}^2 \quad (24)$$

where

Δe_{cor}	- Correction value of meter error (%)
a, b, c	- Parameter of fitted polynomial model (Table 15) (-)

$$e_{\text{cor}} = e - \Delta e_{\text{cor}} \quad (25)$$

where

e_{cor}	- Temperature corrected meter error (%)
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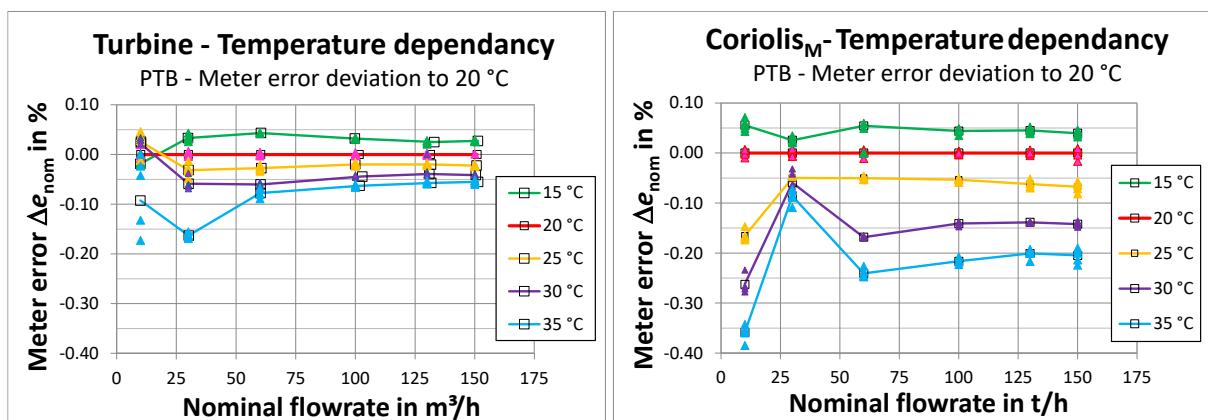


Figure 17: Temperature dependencies of turbine meter and Coriolis_Mass - Differences of meter error Δe_{nom} , expressed as results of Equation (23). All calibrations were made at pilot laboratory (PTB) in 2015.

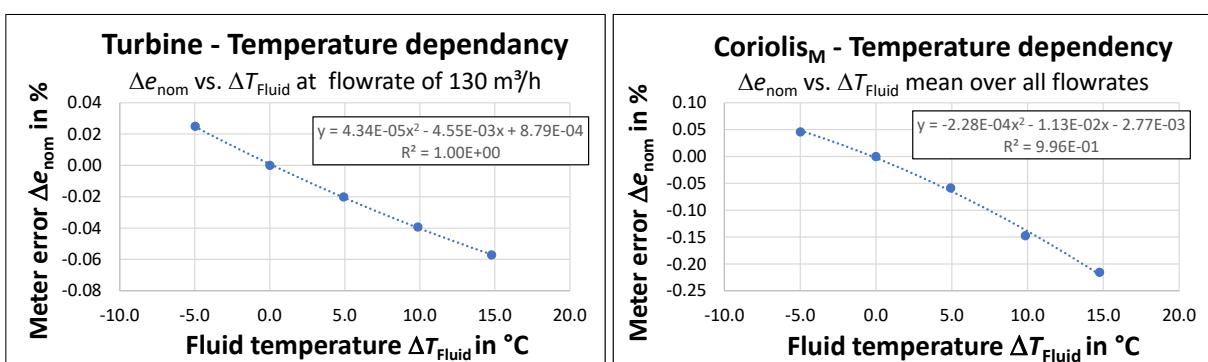


Figure 18: Temperature dependency of Turbine meter - Example relationship between ΔT_{fluid} and Δe_{nom} at flowrate of 100 m³/h (results of Equation 22 and Equation 23) in order to estimate model parameters of Equation (24).

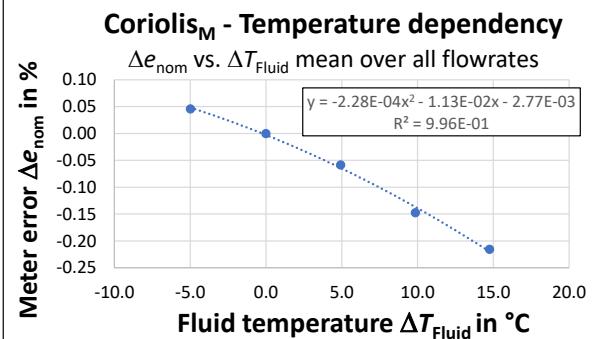


Figure 19: Temperature dependency of Coriolis meter - relationship between ΔT_{fluid} and Δe_{nom} , this mean function is based on flowrates between 60 t/h and 150 t/h (Equation 22 and Equation 23) in order to estimate model parameters of Equation (24).

Table 15: Model Parameter for temperature dependent correction of meter error e by using Equation (13) until Equation (25) for turbine meter and Coriolis_Mass meter

Nominal flowrate in m³/h	Turbine meter – model parameter			Coriolis_Mass – model parameter		
	a	b	c	a	b	c
10	2.11E-02	6.01E-03	-8.75E-04	-2.77E-03	-1.13E-02	-2.28E-04
30	1.10E-02	-5.13E-03	-4.11E-04			
60	2.20E-03	-7.41E-03	1.33E-04			
100	2.74E-03	-5.38E-03	6.38E-05			
130	8.79E-04	-4.55E-03	4.34E-05			

Meter uncertainty u_{temp}

The presented method was successfully applied during model evaluation by using the temperature characterisation measurements at pilot laboratory (PTB) in 2015 (Figure 21). Especially for Coriolis_Mass, a meter uncertainty reduction (u_{temp}) of up to 94 % was gained if the meter error e was corrected by the described method. This clear improvement of u_{temp} over full flow scale can be explained by the distinctive temperature dependency of both meters.

The calculation of u_{TS} itself is based on the following procedure and assumptions. The temperature range of reported laboratory data T_{fluid} does not exceed the investigated range of 20°C +/- 15 °C during characterisation measurements at pilot laboratory (Figure 16). The sensitivities of original meter error e and corrected meter error e_{cor} can also be expressed as specific model residuals e_{residual} to mean values over all temperatures (Equation 26 and Figure 20). Maximum and minimum values of e_{residual} were used to calculate u_{temp} (Table 16) with an assumption of a rectangular probability distribution (Equation 27). For calculation of E_N values, all reported meter errors (e_V and e_m) of participating laboratories were corrected by the described method (Equation 22 until Equation 25).

$$e_{\text{residual}} = e - e_{\text{mean}} \quad (26)$$

where e_{residual} - Model residuals (%)
 e_{mean} - Mean values of meter error at one flow rate over all temperatures (%)

$$u_{\text{temp}} = \frac{\max(e_{\text{residual}}) - \min(e_{\text{residual}})}{2\sqrt{3}} \quad (27)$$

where u_{temp} - Meter uncertainty caused by temperature effects (%)

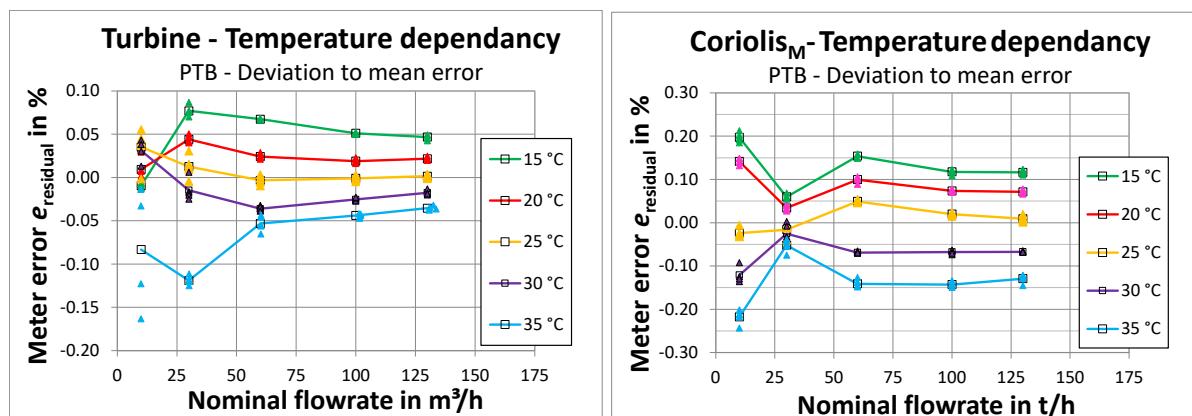


Figure 20: Temperature dependencies of Turbine meter and Coriolis_Mass - Residuals to mean values of Equation (26) for original meter error e

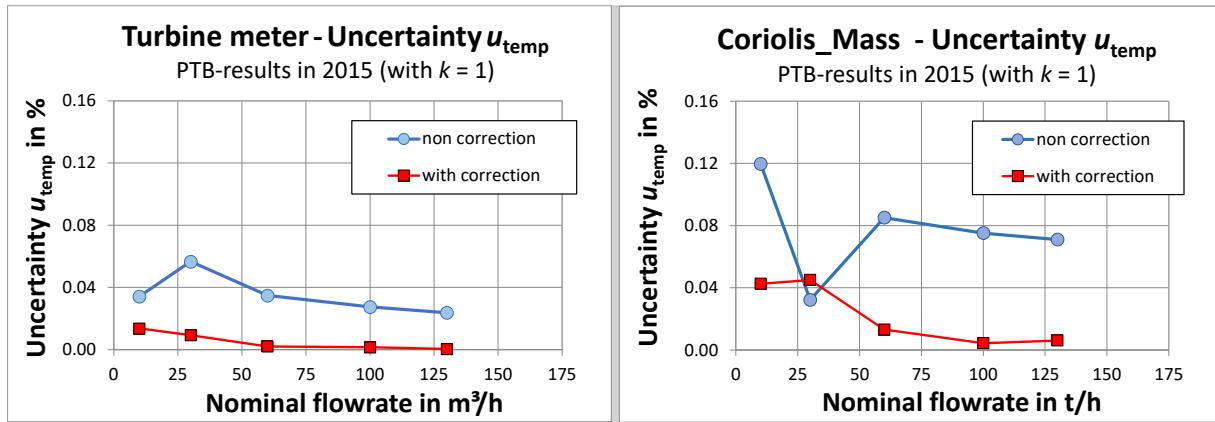


Figure 21: Meter uncertainties u_{temp} for turbine meter and Coriolis_Mass - based on non-corrected meter error e and on corrected meter error e_{cor} in 2015 - using Equation (22) until Equation (27).

Table 16: Final uncertainties of meter temperature sensitivity u_{temp}

u_{temp} ($k = 1$)	Nominal Flowrate				
	$10 \text{ m}^3/\text{h}$	$30 \text{ m}^3/\text{h}$	$60 \text{ m}^3/\text{h}$	$100 \text{ m}^3/\text{h}$	$130 \text{ m}^3/\text{h}$
Turbine meter in %	0.014	0.009	0.002	0.001	0.000
Coriolis_Mass in %	0.043	0.045	0.013	0.004	0.006

7.4 Pressure dependency - uncertainty u_{pres}

Laboratory conditions

The span of line pressure in participating laboratories p_{fluid} ranged between 0.27 bar and 3.00 bar (positive pressure after calibration setup) Figure 22.

Table 17: Line pressure p_{fluid} (bar) in participating laboratories during calibrations on day#1 and day#2; *) values for INTI representing general facility specifications

NMI	PTB 1	CISA	INACAL	IBMETRO	INTI*)	CENAM	PTB 2
Max	3.02	3.00	2.15	2.11	3.5	2.93	3.00
Min	2.97	2.45	2.00	0.27	2.2	2.51	2.98
Max - Min	0.06	0.55	0.15	1.85		0.41	0.03
Mean	3.00	2.84	2.06	1.59		2.77	2.99

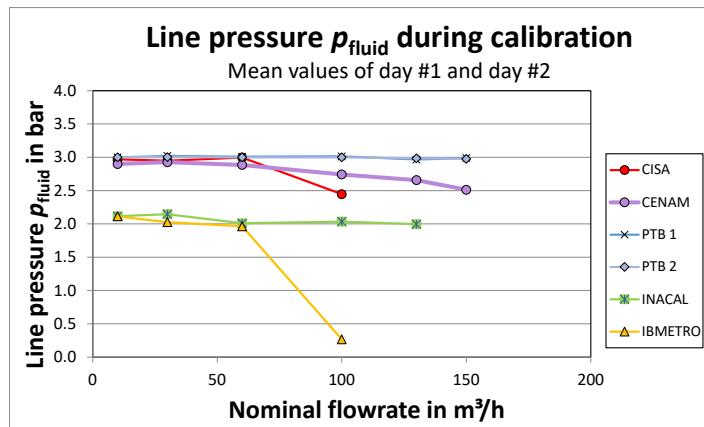


Figure 22: Line pressure during calibrations in participating laboratories – Mean values at each flowrate of calibration day #1 and day #2

Meter characteristics

Pressure dependencies of transfer meters were analyzed at pilot laboratory (PTB) during characterisation measurements in 2015 (Table 6). Due to technical restrictions, calibrations were only possible at line pressure between 2 bar and 4 bar (Figure 23).

The deviations of meter error to mean values, expressed as residuals are presented in Figure 24. For pressure differences of +/- 1 bar, the sensitivity of meter error does not exceed +/- 0.03 % for turbine meter and +/- 0.05 % for Coriolis_Mass.

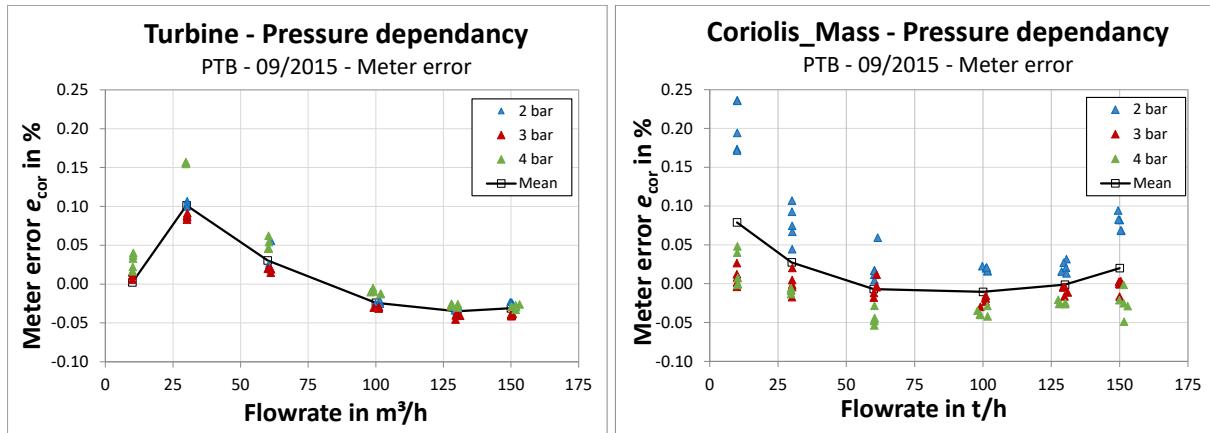


Figure 23: Pressure dependencies of turbine and Coriolis meter - Calibration results and mean values of characterization measurements at pilot laboratory PTB in 2015

Meter uncertainty u_{pres}

For uncertainty calculation of u_{pres} it was assumed that the following conservative estimation of meter sensitivities did include the pressure range between 0.27 bar and 3.02 bar of reported data (Figure 22). The pressure sensitivities were treated as uncertainty contribution for turbine meter by $u_{\text{pres}} = 0.030 \% / \sqrt{3}$ and for Coriolis by $u_{\text{pres}} = 0.050 \% / \sqrt{3}$, based on a rectangular probability distribution.

The results for turbine meter ($u_{\text{pres}} = 0.017 \%$) and Coriolis ($u_{\text{pres}} = 0.029 \%$), were used as constant values, valid for full investigated flow scale. For final calculation of E_N values, no pressure corrections were made to the data submitted by participating laboratories.

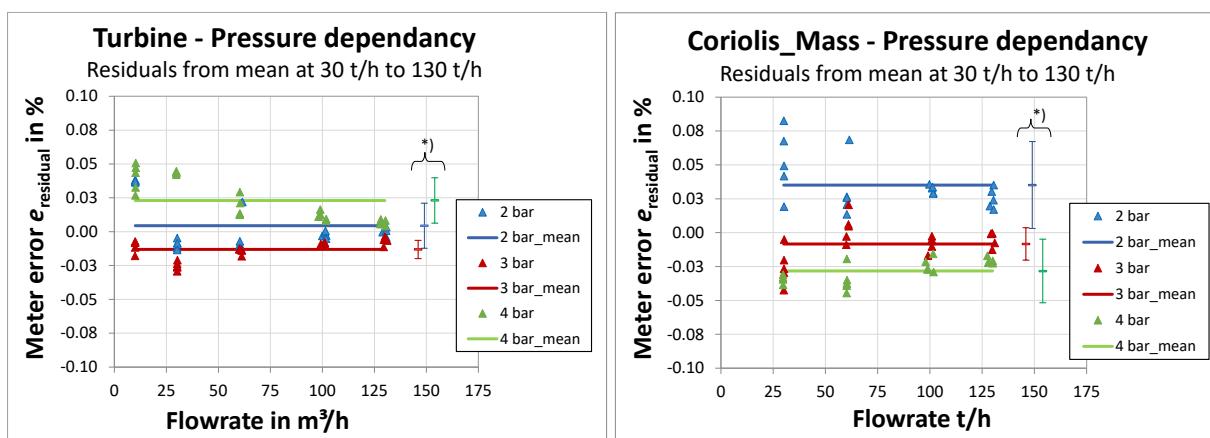


Figure 24: Pressure dependencies of turbine meter and Coriolis_Mass - Residuals to mean values of temperature corrected meter error e_{cor} . *) represents the standard deviation of e_{cor} for each pressure rate. For Coriolis meter the values at 10 t/h were not considered because of the still present autozero effect (Figure 23)

7.5 Dependency on flow stability - uncertainty u_{flow}

Laboratory conditions

For data analysis of flow stability, the deviations of reference flow between pilot laboratory (PTB) and participating laboratories were analyzed. The mean values of observed differences did not exceed +/- 3 % of flowrate at pilot laboratory (Figure 25).

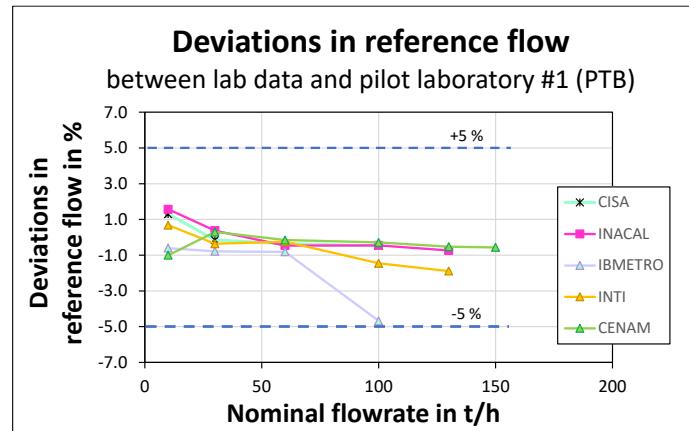


Figure 25: Flow stability \dot{m} (t/h), expressed as deviations in reference flow between pilot laboratory (PTB) calibrated in 01/2016 and reported values of participating laboratories

Meter characteristics

For analyzing meter error sensitivity to changes in flowrate, calibration results at reference laboratory (PTB) were evaluated. Between single calibration points, the meter error of a standard calibration ($T_{\text{fluid}} = 20^\circ\text{C}$, $p_{\text{fluid}} = 3$ bar) was linear interpolated. Within this model, the sensitivities of meter error were estimated by varying flowrates to maximum values of +/- 5.0 % with a resolution of 0.5 %. (Figure 26). Based on the previously discussed maximum limits in flowrate stability of +/- 5 % (Figure 25), both meter showed a maximum sensitivity in meter error of +/- 0.010 % (Figure 26).

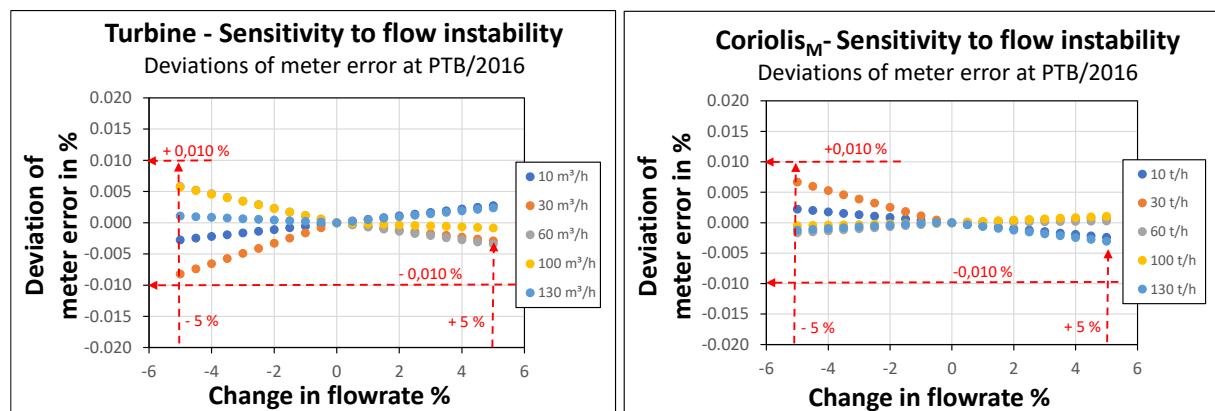


Figure 26: Sensitivity of transfer meters to flow instability - based on PTB data set in 01/2016

Meter uncertainty u_{flow}

The estimated maximum values of flow meter sensitivity were used for calculation of u_{flow} . For both meter, the flow stability sensitivities were treated as a rectangular uncertainty contribution, with $u_{\text{flow}} = 0.010 \% / \sqrt{3}$. It was assumed, that the results of $u_{\text{flow}} = 0.006 \%$ were valid for full investigated flow scale. For final calculation of E_N values, no flow stability corrections were made to the data submitted by participating laboratories.

7.6 Dependency of inflow conditions to Turbine meter

Laboratory conditions

The span of undisturbed inflow length in participating laboratories ranged between 0.1 m and 4.6 m. Typical fittings like valves, tube bundle or elbows were installed at the inflow of calibration line (Table 18).

Table 18: Reported inflow lengths of undisturbed flow and pipe installation at the inflow of calibration line in participating laboratories

NMI	PTB (pilot lab)	CISA	INACAL	IBMETRO	INTI
Undisturbed inflow length	8.5 m	4.6 m	0.1 m	3.5 m	> 2.0 m
Pipe installation before inflow	tube bundle, line reducer	line reducer	elbow, tube bundle	line reducer, valve	line reducer, valve

Turbine meter characteristics

The used turbine meter was identical to the type of flow meter, which was used during KC1, but with an inner diameter of 80 mm instead of 100 mm. During KC1, the turbine meter showed a distinctive sensitivity to disturbed inflow conditions. Within the ranges of reported SC inflow lengths (Table 18), the turbine meter of KC1 showed maximum sensitivities of meter error (Figure 27) in positive direction with +0.351 % (disturber type: 30 % closed orifice plate, inflow length: 1 m), in negative direction -0.092 % (disturber type: 2nd turbine meter, inflow length: 4 m).

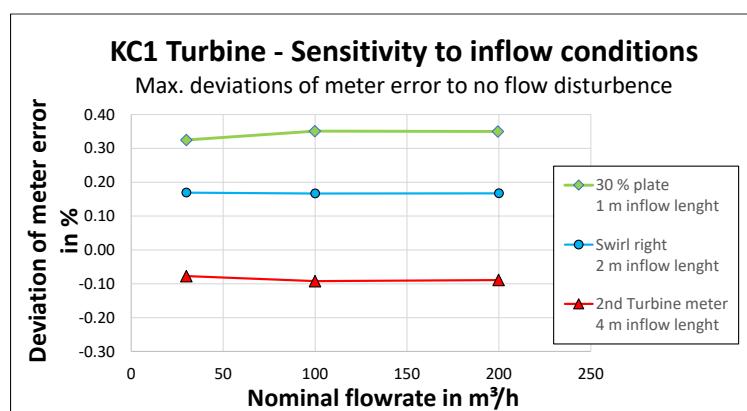


Figure 27: Maximum observed sensitivity of turbine meter to different flow disturber and inflow lengths - based on PTB calibrations in 03/2019 during KC1 comparison with a DN100 mm turbine meter

Meter uncertainty

This research was necessary, because of significant differences in turbine meter calibrations between participating laboratories. Whereas, for flowrates higher than 10 m³/h, the maximum span of Coriolis meter error reached 0.222 % between laboratories (Figure 42, without INTI). At the same time the results of turbine meter differ up to 1.048 % (Figure 29). Such differences could not be explained by a standard estimation of transfer meter uncertainties. Behind this background and according to KC1 procedure, an additional uncertainty parameter (u_{inflow}) was introduced for turbine meter to consider the influence of different inflow conditions to calibration characteristics of turbine meter.

With reference to the minimum reported inflow length of 0.10 m at participating laboratories (Table 18), the maximum observed meter error deviation at 1 m inflow length (Figure 27) was used for the estimation of turbine meter sensitivity u_{inflow} . The inflow sensitivity was treated as a rectangular uncertainty contribution with $u_{\text{inflow}} = 0.351 \% / \sqrt{3} = 0.203 \%$. It was assumed, that the results of $u_{\text{inflow}} = 0.096 \%$ are valid for full investigated flow scale. For final calculation of E_N values, no corrections for different inflow conditions were made to the submitted data of turbine meter.

8 Results and final data evaluation

8.1 Ambient air temperature

Laboratory conditions

The span of air temperature in participating laboratories ranged between 18.24 °C and 32.31 °C. The maximum variation of air temperature within a participating lab, expressed as $\max(T_{\text{air}}) - \min(T_{\text{air}})$ was reported with 5.40 °C (Table 19, Figure 28).

Table 19: Air temperatures T_{air} (°C) in participating laboratories during calibrations on day#1 and day#2;
*) values for INTI representing general facility specifications

NMI	PTB 1	CISA	INACAL	IBMETRO	INTI	CENAM	PTB 2
Max	21.99	26.16	26.30	19.20		28.48	22.70
Min	21.73	21.19	22.70	16.90		25.40	21.90
Max - Min	0.26	4.97	3.60	2.30		3.07	0.80
Mean	21.88	24.76	24.74	17.95	25 °C ± 3 °C	26.65	22.46

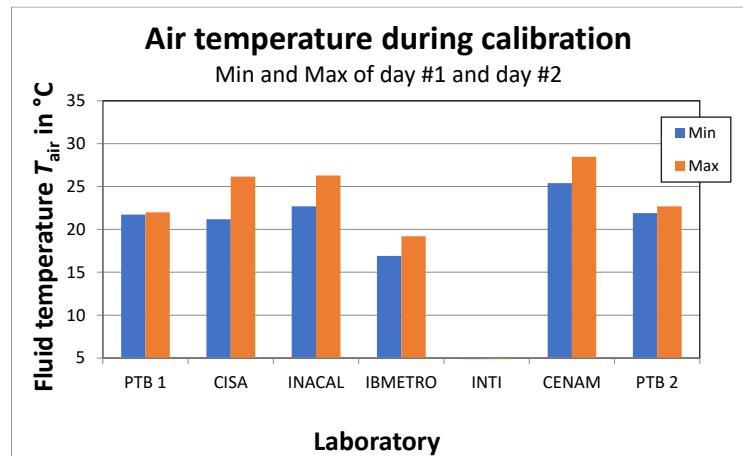


Figure 28: Air temperature T_{air} during calibrations in participating laboratories - maximum and minimum of calibration day #1 and day #2

8.2 Turbine transfer meter

8.2.1 Summarized results

Laboratory results

Table 20: Relative measurement error x_i (%) of turbine meter at participated laboratories - temperature corrected mean values of day #1 and day #2, comparison reference value $SCRV_{Turb}$ and $U(SCRV_{Turb})$

Flowrate	CISA	INACAL	IBMETRO	INTI	PTB_2 = $SCRV_{Turb}$	$U(SCRV_{Turb})$ $k = 2$
m^3/h	%	%	%	%	%	%
10	-0.700	0.222	-2.255	-0.153	-0.025	0.414
30	-0.140	0.386	-0.541	0.564	0.135	0.414
60	-0.220	0.420	-0.187	0.433	0.154	0.423
100	-0.230	0.450	-0.221	0.476	0.161	0.433
130		0.488		0.327	0.185	0.438

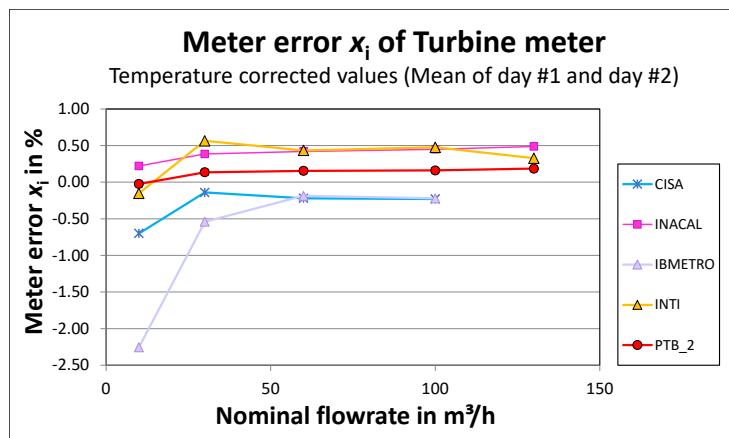


Figure 29: Relative measurement error x_i of turbine meter at participating laboratories - temperature corrected mean values of day #1 and day #2. The values of PTB_2 were used as the comparison reference value $SCRV_{Turb}$.

The degree of equivalence value E_N is a measure of result agreement of each participating laboratory to the $SCRV_{Turb}$. Expressed as the normalized differences of “lab to $SCRV_{Turb}$ ”, the final E_N values of turbine meter are summarized in Table 21 and Figure 30. Beside one calibration, all labs passed the E_N criteria of ≤ 1.20 .

Table 21: Summary of E_N -values for turbine meter of each participating laboratory. ^{a)} represents data at warning level, ^{b)} represents data with E_N values > 1.20

Flowrate	CISA	INACAL	IBMETRO	INTI
m^3/h	-	-	-	-
10	1.11 ^{a)}	0.41	3.69 ^{b)}	0.20
30	0.46	0.42	1.01 ^{a)}	0.72
60	0.61	0.43	0.54	0.46
100	0.62	0.47	0.62	0.49
130		0.48		0.22

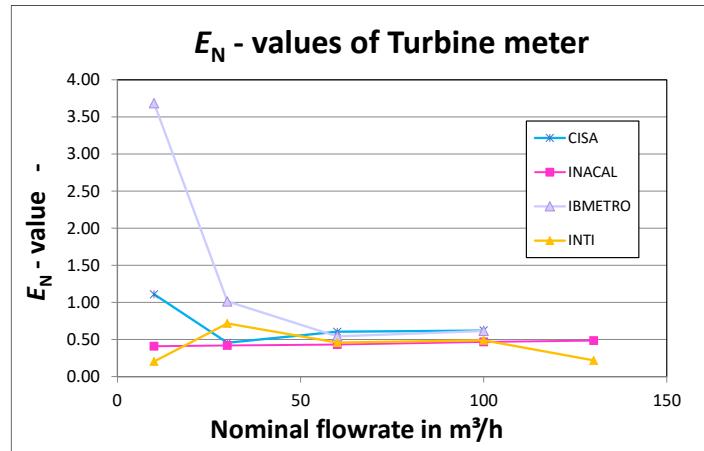


Figure 30: Summarized E_N -values of participating laboratories for turbine meter

Conclusive tests of comparison results $u_{\text{comp}}/u_{\text{base},i}$

Based on [3], for a conclusive proof of participant results and an agreement with the $SCRV_{\text{Turb}}$, the comparison uncertainty ratio $u_{\text{comp}}/u_{\text{base},i}$ should be < 2 .

Results from all participating laboratories couldn't comply with this limit (Table 22). For the purpose of the presented SC the uncertainty u_{comp} of turbine meter was too high. A calibration of turbine meter gave for all laboratories inconclusive results. Finally, the meter was not suitable for a confirmation of the declared CMC values.

Table 22: Summarized results of conclusive proof $u_{\text{comp}}/u_{\text{base},i}$ of each participating laboratory for turbine meter
- c) represents inconclusive data

Flowrate m^3/h	CISA	INACAL	IBMETRO	INTI
-	-	-	-	-
10	2.80 c)	5.67 c)	4.29 c)	7.83 c)
30	2.77 c)	5.55 c)	5.13 c)	7.16 c)
60	2.84 c)	5.72 c)	4.55 c)	7.26 c)
100	2.87 c)	5.74 c)	4.31 c)	7.18 c)
130		5.80 c)		7.29 c)

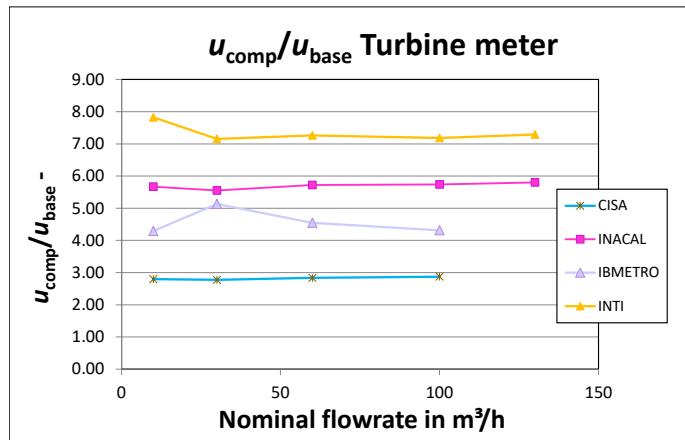


Figure 31: Summarized results of conclusive proof $u_{\text{comp}}/u_{\text{base},i}$ of each participating laboratory for turbine meter

8.2.2 Final CMC-decision tables for participating laboratories

CISA - laboratory (Chile)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 23), because of inconclusive data - at all calibrated flowrates the ratio of $u_{\text{comp}}/u_{\text{base}}$ was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

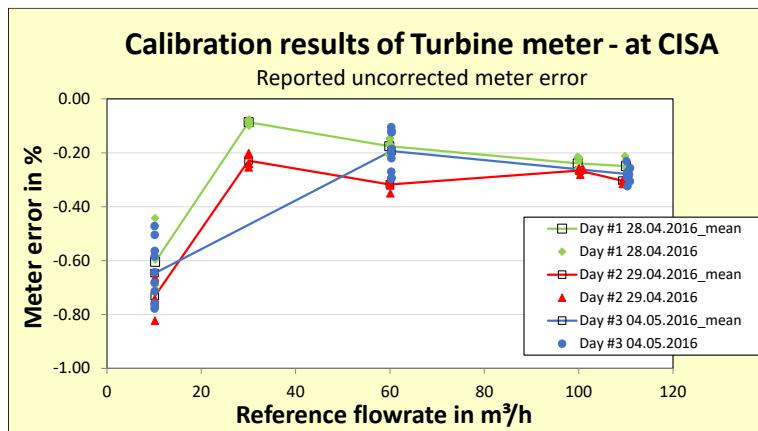


Figure 32: Calibration results of CISA laboratory for turbine meter – reported uncorrected meter error e_v

Table 23: Comparison decision table for CISA (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - ^{a)} represents E_N -values at warning level, ^{c)} represents inconclusive data

CISA / Chile							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	$u_{\text{comp}}/u_{\text{base},i}$	CMC decision status
	x_i	$U_{\text{base},i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
m^3/h	%	%	%	-	-	-	
10	-0.700	0.150	0.445	-0.675	1.11 ^{a)}	2.80 ^{c)}	inconclusive
30	-0.140	0.150	0.442	-0.276	0.46	2.77 ^{c)}	inconclusive
60	-0.220	0.150	0.451	-0.374	0.61	2.84 ^{c)}	inconclusive
100	-0.230	0.150	0.457	-0.390	0.62	2.87 ^{c)}	inconclusive
130							

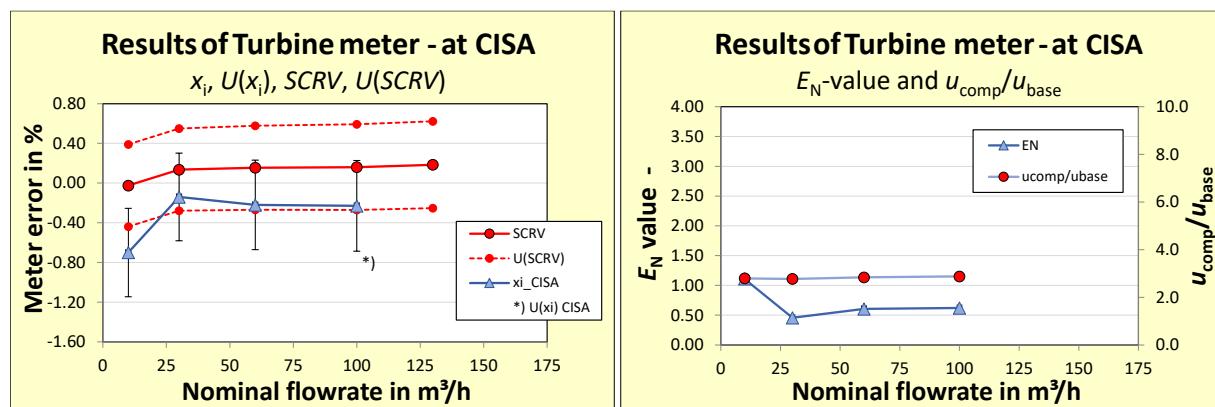


Figure 33: Comparison results of CISA laboratory for turbine meter

INACAL - laboratory (Peru)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 24), because of inconclusive data - at all calibrated flowrates the ratio of $u_{\text{comp}}/u_{\text{base}}$ was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

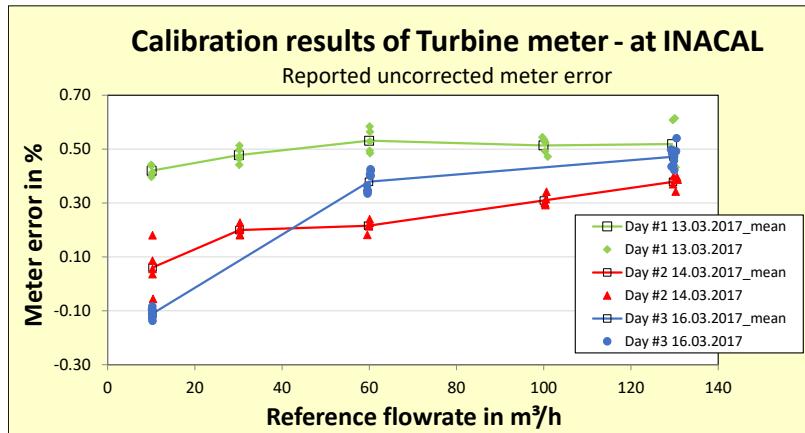


Figure 34: Calibration results of INACAL laboratory for turbine meter - reported uncorrected meter error e_v

Table 24: Comparison decision table for INACAL (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) – ^{b)} represents E_N -values > 1.20 , ^{c)} represents inconclusive data

INACAL / Peru							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	$u_{\text{comp}}/u_{\text{base}}$	CMC decision status
	x_i	$U_{\text{base},i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
m^3/h	%	%	%	-	-	-	
10	0.222	0.076	0.438	0.247	0.41	5.67 ^{c)}	inconclusive
30	0.386	0.076	0.429	0.251	0.42	5.55 ^{c)}	inconclusive
60	0.420	0.076	0.442	0.265	0.43	5.72 ^{c)}	inconclusive
100	0.450	0.076	0.443	0.289	0.47	5.74 ^{c)}	inconclusive
130	0.488	0.076	0.447	0.304	0.48	5.80 ^{c)}	inconclusive

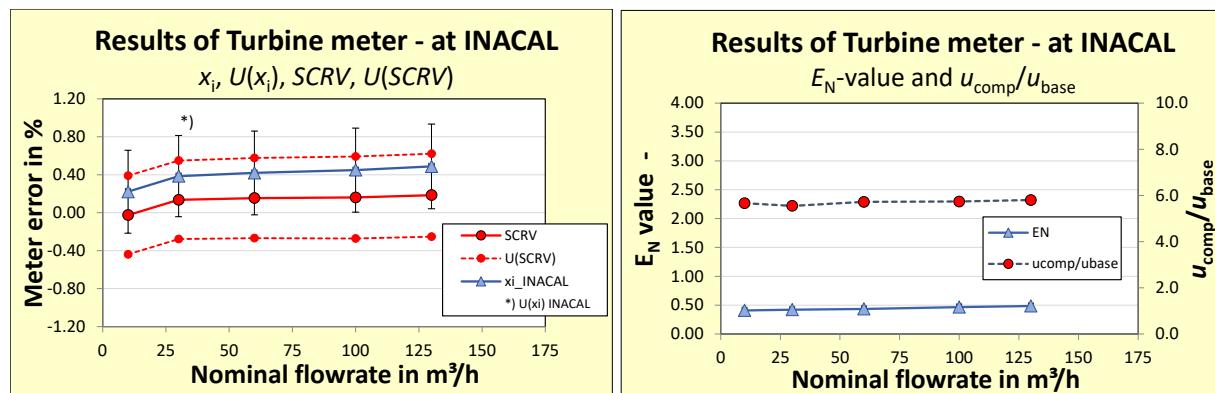


Figure 35: Comparison results of INACAL laboratory for turbine meter

IBMETRO - laboratory (Bolivia)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 25), because of inconclusive data - at all calibrated flowrates the ratio of $u_{\text{comp}}/u_{\text{base}}$ was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

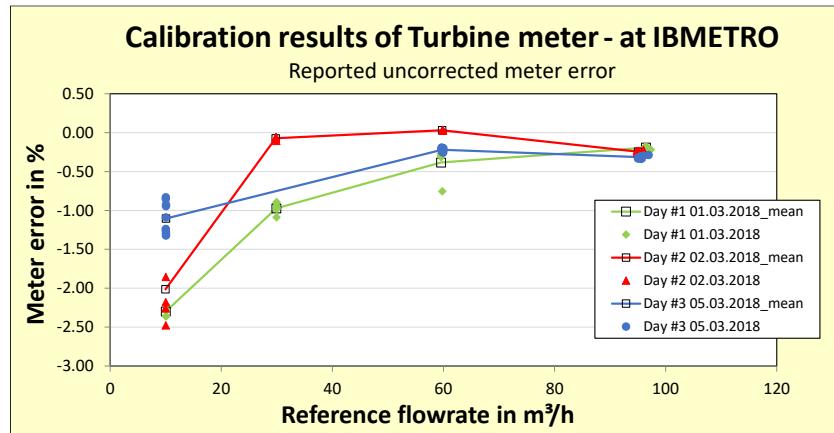


Figure 36: Calibration results of IBMETRO for turbine meter - reported uncorrected meter error e_v

Table 25: Comparison decision table for IBMETRO (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - ^{a)} represents E_N -values at warning level, ^{b)} represents E_N -values > 1.20 , ^{c)} represents inconclusive data

Nominal flowrate	IBMETRO / Bolivia						
	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	$u_{\text{comp}}/u_{\text{base}}$	CMC decision status
	x_i	$U_{\text{base},i} (k = 2)$	$U(x_i) (k = 2)$	d_i	$E_{N,i}$		
m^3/h	%	%	%	-	-	-	
10	-2.255	0.100	0.441	-2.230	3.69 ^{b)}	4.29 ^{c)}	inconclusive
30	-0.541	0.100	0.523	-0.676	1.01 ^{a)}	5.13 ^{c)}	inconclusive
60	-0.187	0.100	0.466	-0.341	0.54	4.55 ^{c)}	inconclusive
100	-0.221	0.100	0.443	-0.382	0.62	4.31 ^{c)}	inconclusive
130							

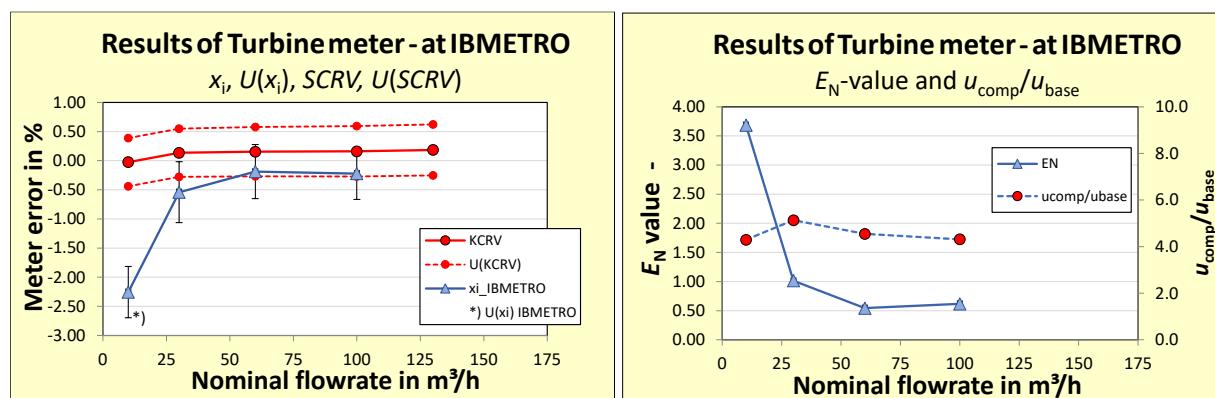


Figure 37: Comparison results of IBMETRO laboratory for turbine meter

INTI - laboratory (Argentina)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 26), because of inconclusive data - at all calibrated flowrates the ratio of $u_{\text{comp}}/u_{\text{base}}$ was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

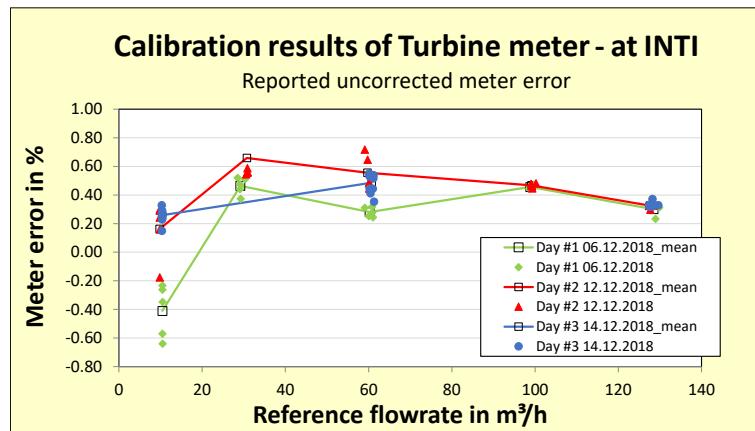


Figure 38: Calibration results of INTI for turbine meter - reported uncorrected meter error e_v

Table 26: Comparison decision table for INTI (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - ^{c)} represents inconclusive data

INTI / Argentina							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	$u_{\text{comp}}/u_{\text{base}}$	CMC decision status
	x_i	$U_{\text{base},i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
m^3/h	%	%	%	-	-	-	
10	-0.153	0.060	0.473	-0.128	0.20	7.83 ^{c)}	inconclusive
30	0.564	0.060	0.433	0.429	0.72	7.16 ^{c)}	inconclusive
60	0.433	0.060	0.440	0.279	0.46	7.26 ^{c)}	inconclusive
100	0.476	0.200	0.475	0.315	0.49	7.18 ^{c)}	inconclusive
130	0.327	0.200	0.481	0.142	0.22	7.29 ^{c)}	inconclusive

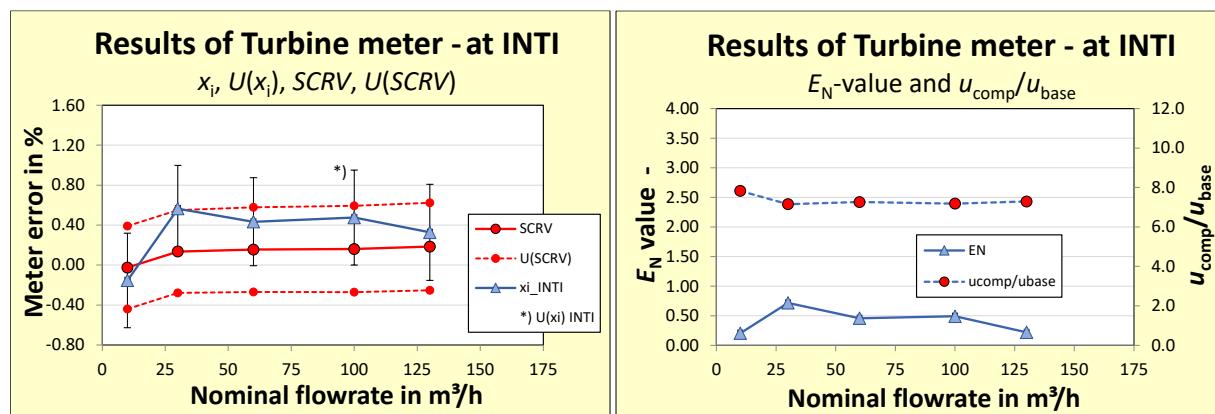


Figure 39: Comparison results of INTI laboratory for turbine meter

8.3 Coriolis_Mass transfer meter

8.3.1 Results of $SCRV_{Cor}$ calculation and E_N values for CENAM and PTB

The comparison reference value for Coriolis meter ($SCRV_{Cor}$) was partially linked to Key Comparison CCM.FF-K1.2015 (KC1) - see Chapter 6.4.1. The data of both pilot laboratories (PTB and CENAM) were used for the calculation of $SCRV_{Cor}$. - see Chapter 6.4.2. The input data are given in Table 27, the calculated values of $SCRV_{Cor}$ and its uncertainties are presented in Table 28 and Figure 40, the final E_N values are summarized in Table 29 and Figure 41.

Table 27: Input data for calculation of $SCRV_{Cor}$

Nominal flowrate	SIM comparison data				KC1 comparison data (based on Table 8 and Table 9)			
	Autozero corrected measurement error		Measurement uncertainty of x_i		Supplementary comparison correction value		Uncertainty of SCC_i	
	CENAM	PTB	CENAM	PTB	CENAM	PTB	CENAM	PTB
	x_i	x_i	$u(x_i)$ ($k = 1$)	$u(x_i)$ ($k = 1$)	SCC_i	SCC_i	$u(SCC_i)$ ($k = 1$)	$u(SCC_i)$ ($k = 1$)
t/h	%	%	%	%	%	%	%	%
10	-0.049	0.062	0.071	0.070				
30	-0.025	-0.030	0.058	0.057	0.006	0.004	0.025	0.022
60	-0.015	-0.013	0.038	0.036	0.012	0.004	0.018	0.014
100	-0.027	-0.009	0.035	0.033	0.012	-0.001	0.017	0.013
130	-0.027	-0.003	0.036	0.035				

Table 28: Calculation of $SCRV_{Cor}$

Nominal flowrate	SIM comparison data					
	SCC_i corrected measurement error		Measurement uncertainty of $x_{Cor,i}$		SCRV	$U(SCRV)$
	CENAM	PTB	CENAM	PTB		
	$x_{Cor,i}$	$x_{Cor,i}$	$u(x_{Cor,i})$ ($k = 1$)	$u(x_{Cor,i})$ ($k = 1$)		($k = 2$)
t/h	%	%	%	%	%	%
10	-0.049	0.062	0.070	0.071	0.007	0.100
30	-0.032	-0.034	0.061	0.063	-0.033	0.088
60	-0.026	-0.017	0.039	0.042	-0.021	0.057
100	-0.039	-0.008	0.035	0.039	-0.022	0.053
130	-0.027	-0.003	0.035	0.036	-0.014	0.050

Table 29: E_N -values for comparison between CENAM and PTB

Nominal flowrate	SIM comparison data					
	d_i		$U(d_i)$		E_N	
	CENAM	PTB	CENAM	PTB	CENAM	PTB
			($k = 2$)	($k = 2$)		
t/h	%	%	%	%	-	-
10	-0.056	0.055	0.101	0.099	-0.56	0.56
30	0.001	-0.001	0.090	0.085	0.01	-0.01
60	-0.005	0.004	0.062	0.053	-0.08	0.08
100	-0.017	0.014	0.058	0.048	-0.29	0.29
130	-0.013	0.011	0.053	0.048	-0.24	0.24

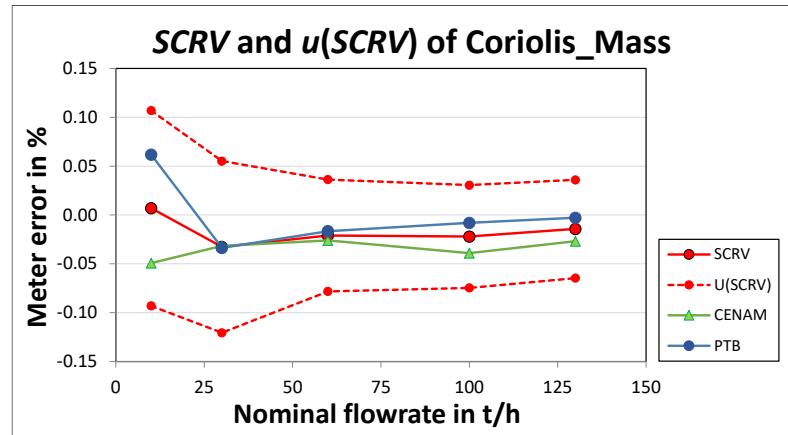


Figure 40: Results of corrected meter error for Coriolis_Mass and $SCRV_{cor}$ of the comparison between CENAM and PTB, including $U(SCRV_{cor})$

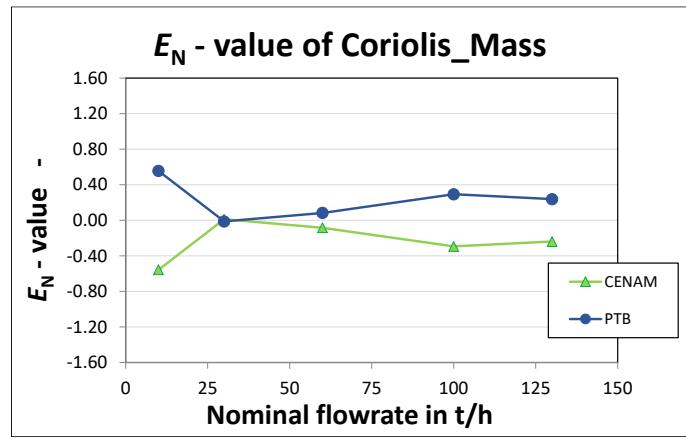


Figure 41: E_N values of basic comparison between CENAM and PTB

8.3.2 Comparison results of participating laboratories

Laboratory results

Table 30: Relative measurement error x_i (%) of Coriolis_Mass at participating laboratories – temperature corrected mean values of day #1 and day #2, comparison reference value $SCRV_{Cor}$ and $U(SCRV_{Cor})$

Flowrate	CISA	INACAL	IBMETRO	INTI	$SCRV_{Cor}$	$U(SCRV_{Cor})$ $k = 2$
t/h	%	%	%	%	%	%
10	-0.194	-0.348	-0.154	-0.137	0.007	0.100
30	-0.101	-0.120	-0.143	-0.073	-0.033	0.088
60	-0.075	0.040	-0.160	-0.004	-0.021	0.057
100	-0.064	0.059	-0.157	0.439	-0.022	0.053
130		0.072		0.338	-0.014	0.050

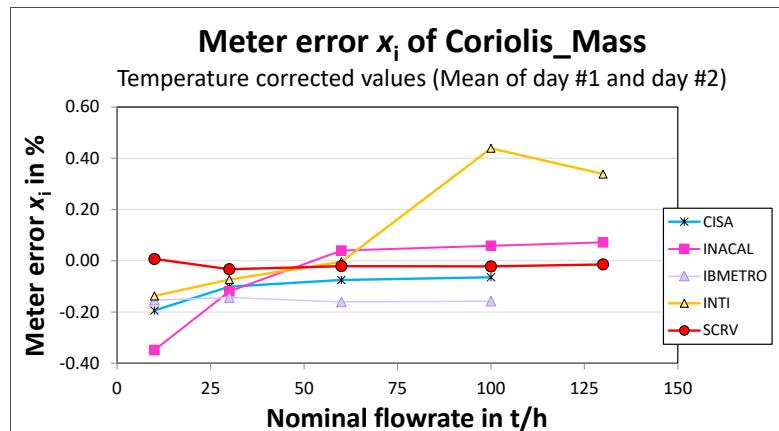


Figure 42: Relative measurement error x_i of Coriolis_Mass at participating laboratories - temperature corrected mean values of day #1 and day #2

The E_N values of participating laboratories are summarized in Table 31 and Figure 43. Beside two calibrations, all laboratories complied with the E_N criteria of < 1.2. Only at the flowrates of 100 t/h and 130 t/h this critical value.

Table 31: Summary of E_N -values of participating laboratories for Coriolis_Mass transfer meter - ^{a)} represents E_N – values at warning level between 1.00 and 1.20, ^{b)} represents E_N -values > 1.20

Flowrate	CISA	INACAL	IBMETRO	INTI
t/h	-	-	-	-
10	0.82	0.91	0.81	0.77
30	0.33	0.47	0.63	0.25
60	0.31	0.47	1.03 ^{a)}	0.11
100	0.24	0.65	1.04 ^{a)}	1.96 ^{b)}
130		0.72		1.50 ^{b)}

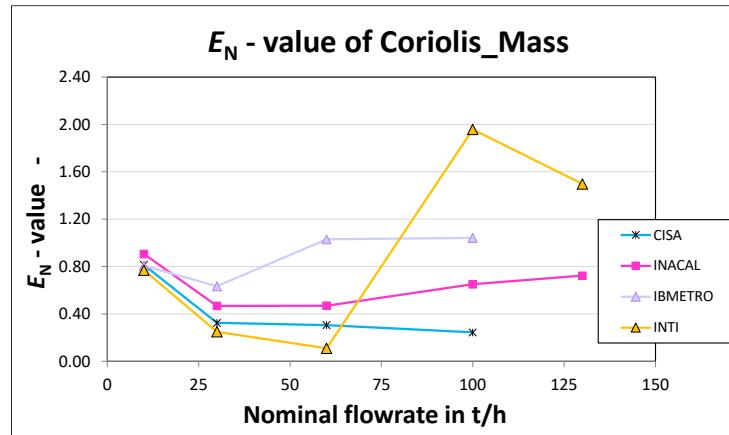


Figure 43: Summarized E_N -values of participating laboratories for Coriolis_Mass transfer meter

Conclusive tests of comparison results $u_{\text{comp}}/u_{\text{base}}$

Based on [3], for a conclusive proof of participant results and an agreement with the $SCRV_{\text{Cor}}$, the comparison uncertainty ratio $u_{\text{comp}}/u_{\text{base}}$ should be < 2 . The results for participating laboratories are summarized in Table 32 and Figure 44.

Beside one calibration, all results complied with this limit. For the final purpose of this SC the uncertainties u_{comp} of Coriolis_Mass were sufficiently low enough. Finally, the meter was suitable for a confirmation of the declared CMC values.

Table 32: Summarized results of conclusive proof $u_{\text{comp}}/u_{\text{base}}$ of participating laboratories for Coriolis_Mass transfer meter - ^{c)} represents inconclusive data

Flowrate	CISA	INACAL	IBMETRO	INTI
t/h	-	-	-	-
10	1.12	4.88 ^{c)}	1.41	2.00
30	0.79	1.91	1.13	1.66
60	0.50	1.16	0.71	1.76
100	0.44	1.09	0.64	0.93
130	-	1.02	-	0.95

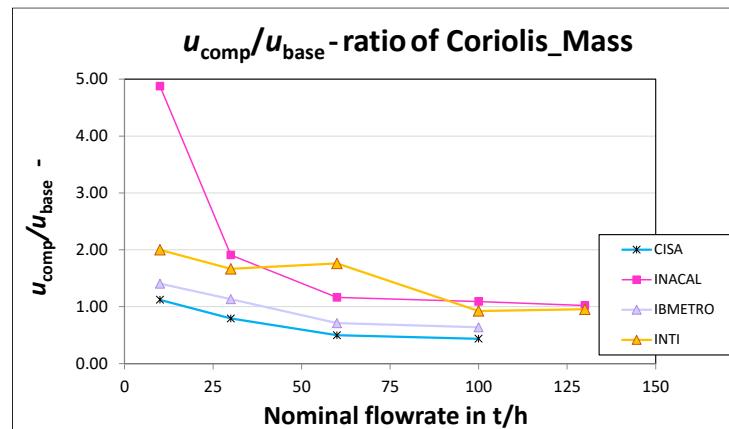


Figure 44: Summarized results of conclusive proof $u_{\text{comp}}/u_{\text{base}}$ of participated laboratories for Coriolis_Mass transfer meter

8.3.3 Final CMC-decision tables for participating laboratories

CISA - laboratory (Chile)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 33).

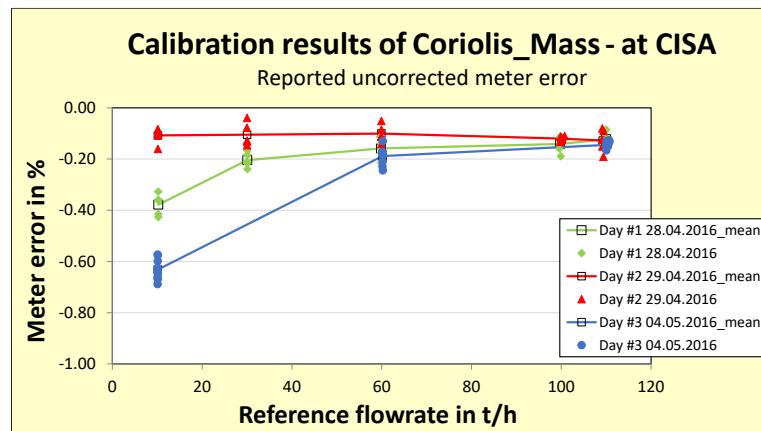


Figure 45: Calibration results of CISA for Coriolis_Mass transfer meter – reported uncorrected meter error e_m

Table 33: Comparison decision table for CISA (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2)

	CISA / Chile							
	Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)		d_i	$E_{N,i}$		
t/h	%	%	%		-	-	-	
10	-0.194	0.150	0.225		-0.201	0.82	1.12	acceptable
30	-0.101	0.150	0.192		-0.069	0.33	0.79	acceptable
60	-0.075	0.150	0.168		-0.054	0.31	0.50	acceptable
100	-0.064	0.150	0.164		-0.042	0.24	0.44	acceptable

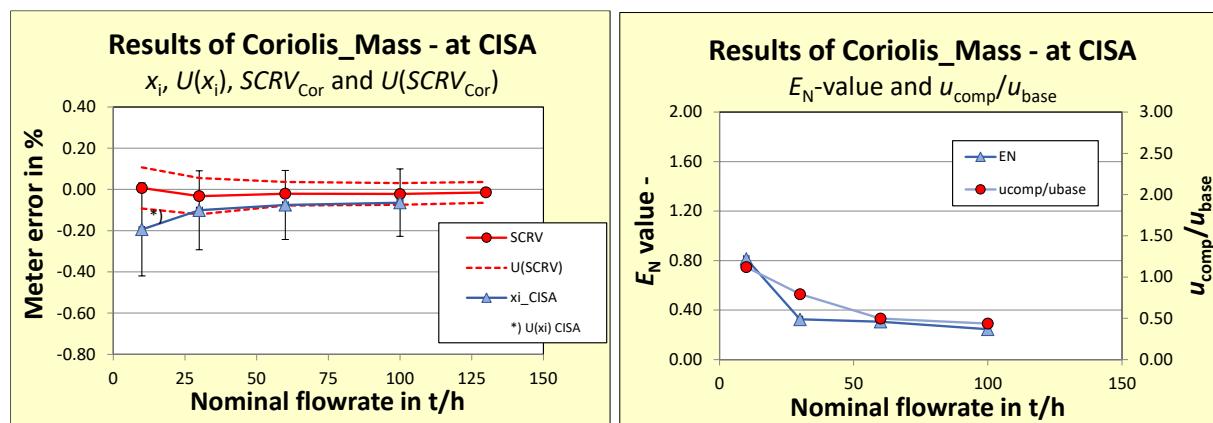


Figure 46: Comparison results of CISA laboratory for Coriolis_Mass transfer meter

INACAL - laboratory (Peru)

Beside the flowrate of 10 t/h, for mass calibration this comparison supported the declared base uncertainties of the participant (Table 34). The calibrations with Coriolis meter were not suitable for a confirmation of the declared CMC at the flowrate of 10 t/h, because the ratio of $u_{\text{comp}}/u_{\text{base}}$ was > 2 .

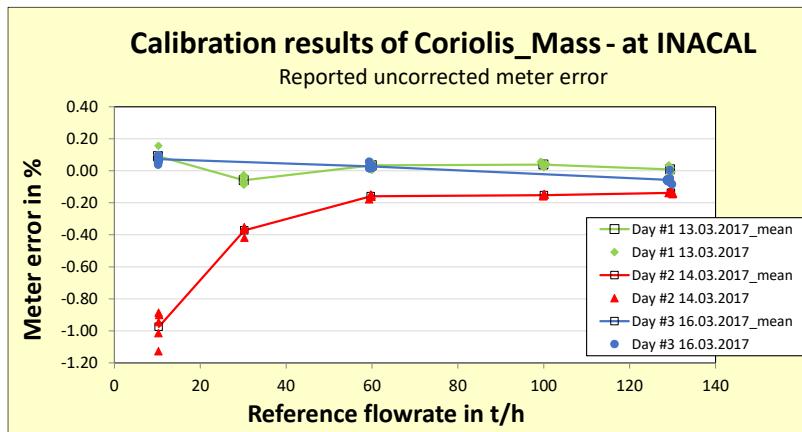


Figure 47: Calibration results of INACAL for Coriolis_Mass transfer meter – reported uncorrected meter error e_m

Table 34: Comparison decision table for INACAL laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - ^{c)} represents inconclusive data

INACAL / Peru							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	$u_{\text{comp}}/u_{\text{base}}$	CMC decision status
	x_i	$U_{\text{base},i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
t/h	%	%	%	-	-	-	
10	-0.348	0.076	0.378	-0.355	0.91	4.88 ^{c)}	inconclusive
30	-0.120	0.076	0.164	-0.087	0.47	1.91	acceptable
60	0.040	0.076	0.117	0.061	0.47	1.16	acceptable
100	0.059	0.076	0.113	0.081	0.65	1.09	acceptable
130	0.072	0.076	0.109	0.087	0.72	1.02	acceptable

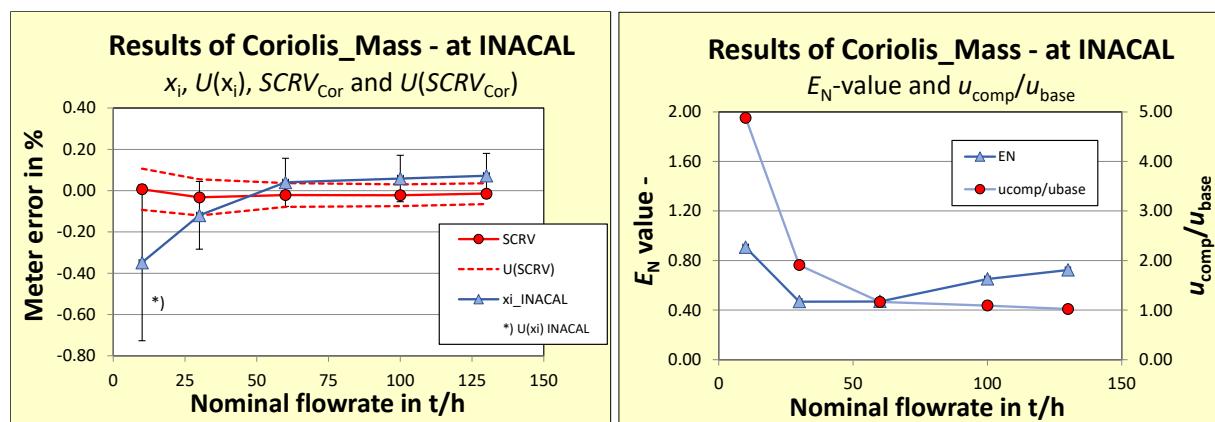


Figure 48: Comparison results of INACAL laboratory for Coriolis_Mass transfer meter

IBMETRO - laboratory (Bolivia)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 35).

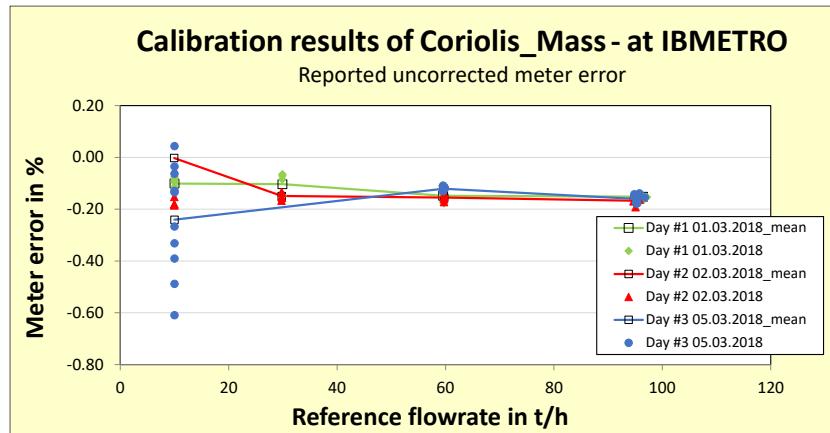


Figure 49: Calibration results of IBMETRO for Coriolis_Mass transfer meter - reported uncorrected meter error e_m

Table 35: Comparison decision table for IBMETRO laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2) -^{a)} represents E_N - values at warning level between 1.00 and 1.20

	IBMETRO / Bolivia							
	Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i} (k = 2)$	$U(x_i) (k = 2)$		d_i	$E_{N,i}$		
t/h	%	%	%		-	-	-	
10	-0.154	0.100	0.172		-0.161	0.81	1.40	acceptable
30	-0.143	0.100	0.151		-0.111	0.63	1.12	acceptable
60	-0.160	0.100	0.123		-0.139	1.03 ^{a)}	0.70	warning level
100	-0.157	0.100	0.119		-0.135	1.04 ^{a)}	0.64	warning level

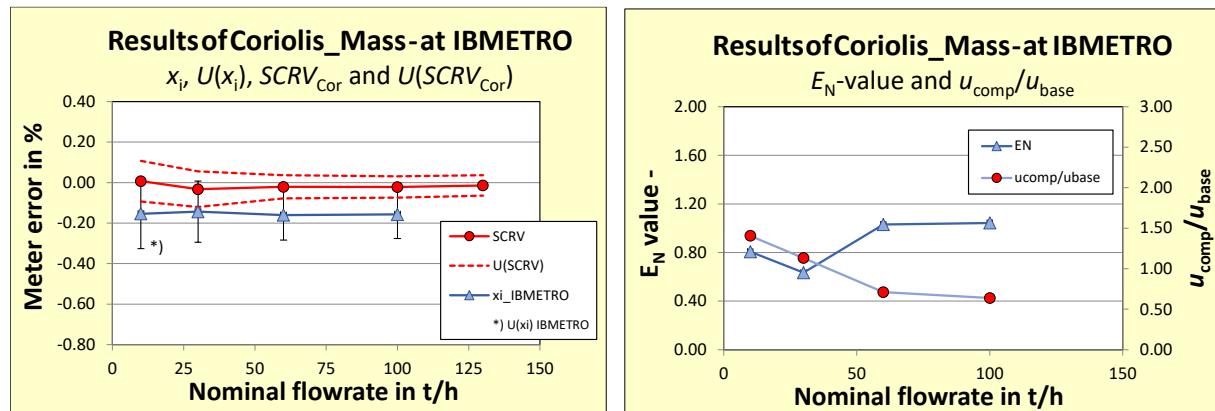


Figure 50: Comparison results of IBMETRO laboratory for Coriolis_Mass transfer meter

INTI - laboratory (Argentina)

For mass calibration between flowrates of 10 t/h and 60 t/h this comparison supported the declared base uncertainties of the participant (Table 36). The laboratory uncertainties for mass calibration at 100 t/h and 130 t/h must be declined, because the E_N value at both flowrates were > 1.20 .

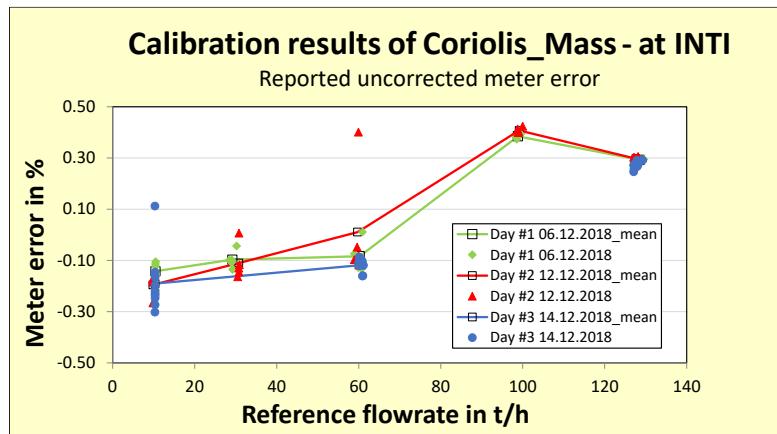


Figure 51: Calibration results of INTI for Coriolis_Mass transfer meter – reported uncorrected meter error e_m

Table 36: Comparison decision table for INTI laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2) - b) represents E_N -values > 1.20

INTI / Argentina							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
t/h	%	%	%	-	-	-	
10	-0.137	0.070	0.158	-0.144	0.77	2.00	acceptable
30	-0.073	0.070	0.136	-0.040	0.25	1.66	acceptable
60	-0.004	0.070	0.142	0.017	0.11	1.76	acceptable
100	0.439	0.220	0.229	0.461	1.96 b)	0.93	not accepted
130	0.338	0.220	0.230	0.353	1.50 b)	0.95	not accepted

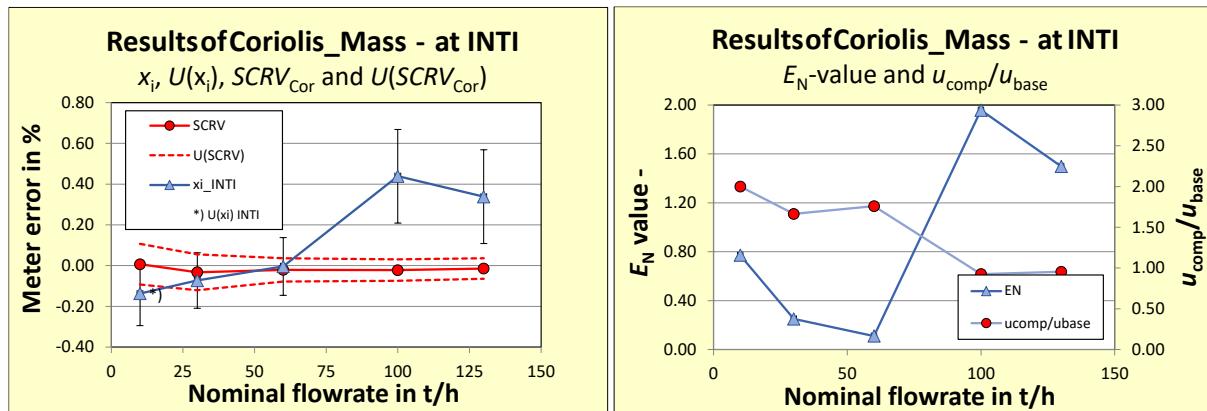


Figure 52: Comparison results of INTI laboratory for Coriolis_Mass transfer meter

9 Nomenclature and unit symbols

Terms and abbreviations

BIPM	Bureau International des Poids et Mesures
CCM	Consultative Committee for Mass and Related Quantities
CCM.FF-K1.2015	Official identifier of Key Comparison CCM-K1.2015
CENAM	Centro Nacional de Metrología - Mexico
CIPM	International Committee for Weights and Measures
CISA	Calibraciones Industriales S.A. - Chile
CMC	Calibration and Measurement Capabilities
DN	Inner pipe diameter (mm)
DoE	Degree of Equivalence
EURAMET	The European Association of National Metrology Institutes
GUM	Guide to the Expression of Uncertainty in Measurement
IBMETRO	Instituto Boliviano de Metrología - Bolivia
INACAL	Instituto Nacional de Calidad - Peru
KC1	Key comparison CCM.FF-K1.2015
KCRV	Key comparison reference value
MRA	(CIPM) Mutual Recognition Arrangement
NMI	National Metrology Institute
PTB	Physikalisch-Technische Bundesanstalt - Germany
RMO	Regional Metrology Organisation
SC	Supplementary Comparison
SIM	Sistema Interamericano de Metrología
TP	Technical Protocol
WGFF	(CCM) Working Group on Fluid Flow

Symbols and units

d_i	Degree of equivalence (DoE) as the difference of SIM-participant i to $SCRV_{Cor}$ (%)
Δe_{nom}	Difference of meter error (%)
e	Meter error at current temperature conditions (%)
e_{cor}	Temperature corrected meter error (%)
Δe_{cor}	Correction value of meter error (%)
e_{mean}	Mean values of meter error at one flow rate over all temperatures (%)
$E_{N,i}$	Normalized Degree of Equivalence as the difference of SIM-participant i to $SCRV$ (%)
e_{nom}	Meter error at nominal temperature of 20 °C (%)
e_m	Relative measurement error of Coriolis meter – mass (%)
$e_{m,cor}$	Temperature corrected measurement error of Coriolis meter (%)
$e_{residual}$	Model residuals (%)
e_v	Relative measurement error of turbine meter – volume (%)
$e_{v,cor}$	Temperature corrected measurement error of turbine meter (%)
i	Laboratory index

k	Coverage factor (-)
$KCRV$	Key Comparison Reference value of KC1 (%)
K_m	meter K -factor - mass-related output (Coriolis meter) (pulses/kg)
$K_{m,nom}$	Nominal K -factor of Coriolis meter - mass output (pulses/kg)
K_v	meter K -factor - volume-related output (turbine meter) (pulses/L)
ΔK_v	Difference in meter K -factor of turbine meter (%)
$K_{v,nom}$	Nominal K -factor of turbine meter (pulses/L)
m_{ref}	Mass, measured by the reference standard (kg)
n	Number of measurements at calibrated test point (-)
N	Counted number of pulses by the transfer meter (pulses)
p_{fluid}	Line pressure (bar)
s	Standard deviation of the mean of measurements at one flowrate point (%)
SCC_i	Supplementary comparison correction for laboratory i (%)
$SCRV$	Supplementary Comparison Reference value (%)
$SCRV_{Cor}$	Reference value of the comparison for Coriolis_Mass meter (%)
$SCRV_{Turb}$	Reference value of the comparison for turbine meter (%)
T_{air}	Air temperature (°C)
T_{fluid}	Fluid temperature (°C)
ΔT_{fluid}	Difference of current fluid temperature to nominal temperature of 20 °C (°C)
T_{nom}	Nominal fluid temperature of 20°C
$U_{base,i}$	Standard uncertainty of laboratory reference (%)
U_{comp}	Standard uncertainty of transfer meter measurements (%)
U_{TS}	Standard uncertainty of transfer meter (%)
$U_{d,i}$	Extended uncertainty of d_i of participant i during SIM comparison (%)
U_{drift}	Standard uncertainty due to drift of transfer meter (%)
U_{reprod}	Standard uncertainty due to reproducibility characteristics of transfer meter (%)
U_{SCC_i}	Uncertainty of SCC for laboratory i (%)
U_{temp}	Standard uncertainty caused by temperature characteristics of transfer meter (%)
U_{pres}	Standard uncertainty caused by pressure characteristics of transfer meter (%)
U_{flow}	Standard uncertainty due to sensitivity of transfer meter to instable flow conditions (%)
U_{inflow}	Standard uncertainty due to sensitivity of turbine meter to different inflow conditions (%)
U_{KCRV}	Standard uncertainty of Key comparison reference value during KC1 (%)
$U_{SCRV,Cor}$	Standard uncertainty of $SCRV_{Cor}$ (%)
$U_{x,i}$	Standard uncertainty of reported and temperature corrected meter error (%)
$U_{x,Cor,i}$	Uncertainty of $x_{Cor,i}$ for reference laboratory i during SIM comparison (%)
$U_{x,KC1,i}$	Uncertainty of calibration results of laboratory i during KC1 (%)
V_{ref}	Volume, measured by the reference standard (m^3)
X_i	Temperature corrected meter error for E_N -value evaluation
$X_{KC1,i}$	Results of laboratory i during KC1 (%)
$X_{Cor,i}$	By SCC_i corrected results of reference laboratory i during SIM comparison (%)

10 References

- [1] *Technical Protocol for Key Comparison CCM.FF-K1.2015.* Draft 5/3. Unpublished. 23.01.2017
- [2] Personal communications
- [3] GUM – *Guide to the Expression of Uncertainty in Measurement*, JCGM 100:2008.
- [4] BIPM: *WGFF Guidelines for CMC Uncertainty and Calibration Report Uncertainty*. 21.10.2013,
<http://www.bipm.org/utils/en/pdf/ccm-wgff-guidelines.pdf>
- [5] WRIGHT, J. et al. (2016): *Transfer standard uncertainty can cause inconclusive inter-laboratory comparisons*. In: Metrologia 53 (2016) 1243 - 1258
- [6] Cox M. G.: *Evaluation of key comparison data*, Metrologia 39 (2002) 589 - 595

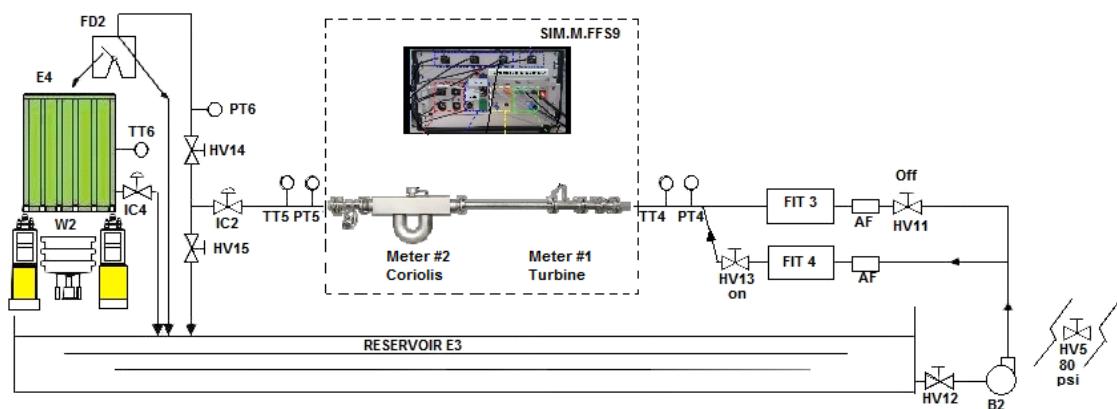
11 Appendices

11.1 Information about participating laboratories

NMI/DI	Country	RMO	Contact	Address
PTB	Germany	EURAMET	Enrico Frahm enrico.frahm@ptb.de	PTB - Physikalisch-Technische Bundesanstalt Department 1.5 Liquid Flow Bundesallee 100 38116 Braunschweig, Germany
CENAM	Mexico	SIM/ Noramet	Roberto Arias Romero rarias@cenam.mx	CENAM - Centro Nacional de Metroología km 4.5 carretera a los Cués, El Marqués, Querétaro México, 76246
CISA	Chile	SIM	Jeny Vargas Angel j.vargas@ci-sa.com	Calibraciones Industriales S.A. Nacional Flujo Líquido Barros Arana 73 Iquique República de Chile
INACAL	Peru	SIM	Adriel Arredondo aarredondo@inacal.gob.pe	Instituto Nacional de Calidad Laboratorio de Flujo de Líquidos Calle De La Prosa 150, San Borja, Lima 41 Perú
IBMETRO	Bolivia	SIM	Juan José Mendoza Aguirre jjmendoza@ibmetro.gob.bo	Instituto Boliviano de Metrología Av. Camacho Nro. 1488 La Paz Bolivia
INTI	Argentina	SIM	Marcelo Alejandro Silvosa msilvosa@inti.gob.ar	INSTITUTO NACIONAL DE TECNOLOGÍA INDUSTRIAL Dirección Técnica de Eficiencia Energética Subgerencia de Áreas de Conocimiento Parque Tecnológico Miquelete Av. General Paz 5445 B1650WAB San Martín Buenos Aires Argentina

Characteristic information of primary standard used during SC	Working procedure																
CISA – Chile <table border="1" data-bbox="203 354 732 781"> <tr> <td>Range of flowrate</td> <td>8 to 300 t/h</td> </tr> <tr> <td>Fluid temperature</td> <td>17 °C to 28 °C</td> </tr> <tr> <td>Line pressure</td> <td>3 bar</td> </tr> <tr> <td>Uncertainty ($k = 2$)</td> <td>0.15 % (Reading)</td> </tr> <tr> <td>Reference</td> <td>Weighing System Max. Cap: 3000 kg</td> </tr> <tr> <td>Operating method</td> <td>Diverter-operated flying start and finish</td> </tr> <tr> <td>Calibration line diameter</td> <td>80 mm (used during SC) Note: Max Diameter 250 mm</td> </tr> <tr> <td>Test fluid</td> <td>Cold water</td> </tr> </table>	Range of flowrate	8 to 300 t/h	Fluid temperature	17 °C to 28 °C	Line pressure	3 bar	Uncertainty ($k = 2$)	0.15 % (Reading)	Reference	Weighing System Max. Cap: 3000 kg	Operating method	Diverter-operated flying start and finish	Calibration line diameter	80 mm (used during SC) Note: Max Diameter 250 mm	Test fluid	Cold water	<p>Gravimetric calibration – static weighing – method.</p> <p>The used method for flowmeter calibration (Coriolis and Turbine) is Gravimetric Method.</p> <p>The gravimetric method comprises weighing the collected water, and time registration. The initial mass (m_0) is automatically registered before the diverter turns the flow towards the weighing tank, starting the measurement of time. After collecting an appropriate amount of liquid, the diverter is activated in the opposed direction, turning aside the water towards the reserve tank; automatically, the measurement of the time stops. Thus, the time of filling (t) of the weighing tank is determined. When the movement of the water in the weighing tank has stopped, the final mass (m_1) is registered. Then, the weighing tank is drained.</p>
Range of flowrate	8 to 300 t/h																
Fluid temperature	17 °C to 28 °C																
Line pressure	3 bar																
Uncertainty ($k = 2$)	0.15 % (Reading)																
Reference	Weighing System Max. Cap: 3000 kg																
Operating method	Diverter-operated flying start and finish																
Calibration line diameter	80 mm (used during SC) Note: Max Diameter 250 mm																
Test fluid	Cold water																



Characteristic information of primary standard used during SC	Working procedure																
INACAL – Peru <table border="1" data-bbox="203 354 774 781"> <tr> <td>Range of flowrate</td> <td>0.26 m³/h – 130 m³/h</td> </tr> <tr> <td>Fluid temperature</td> <td>15 °C – 30 °C</td> </tr> <tr> <td>Line pressure</td> <td>up to 3 bar</td> </tr> <tr> <td>Uncertainty (k = 2)</td> <td>0.26 m³/h – 10 m³/h : 0.11 % 10 m³/h – 130 m³/h : 0.08 % mass, volume</td> </tr> <tr> <td>Reference</td> <td>Weighing method</td> </tr> <tr> <td>Operating method</td> <td>Flying start and stop</td> </tr> <tr> <td>Calibration line diameter</td> <td>DN06 – DN100</td> </tr> <tr> <td>Test fluid</td> <td>Water</td> </tr> </table>	Range of flowrate	0.26 m ³ /h – 130 m ³ /h	Fluid temperature	15 °C – 30 °C	Line pressure	up to 3 bar	Uncertainty (k = 2)	0.26 m ³ /h – 10 m ³ /h : 0.11 % 10 m ³ /h – 130 m ³ /h : 0.08 % mass, volume	Reference	Weighing method	Operating method	Flying start and stop	Calibration line diameter	DN06 – DN100	Test fluid	Water	The static weighing system for flow determination represents the National Liquid Flow Standard of Peru. The static weighing system has two independent flow measurement lines; each one consists of a diverter, a set of nozzles for every flow interval and a weighing system, with maximum load capacities of 500 kg and 2000 kg, respectively. The test flow is established by means of frequency converters. Piping lengths upstream of 15D and downstream of 10D are available. The temperature of the test water is not controlled.
Range of flowrate	0.26 m ³ /h – 130 m ³ /h																
Fluid temperature	15 °C – 30 °C																
Line pressure	up to 3 bar																
Uncertainty (k = 2)	0.26 m ³ /h – 10 m ³ /h : 0.11 % 10 m ³ /h – 130 m ³ /h : 0.08 % mass, volume																
Reference	Weighing method																
Operating method	Flying start and stop																
Calibration line diameter	DN06 – DN100																
Test fluid	Water																



Fig. 1: Diverter and nozzle



Fig. 2: Water flow entry

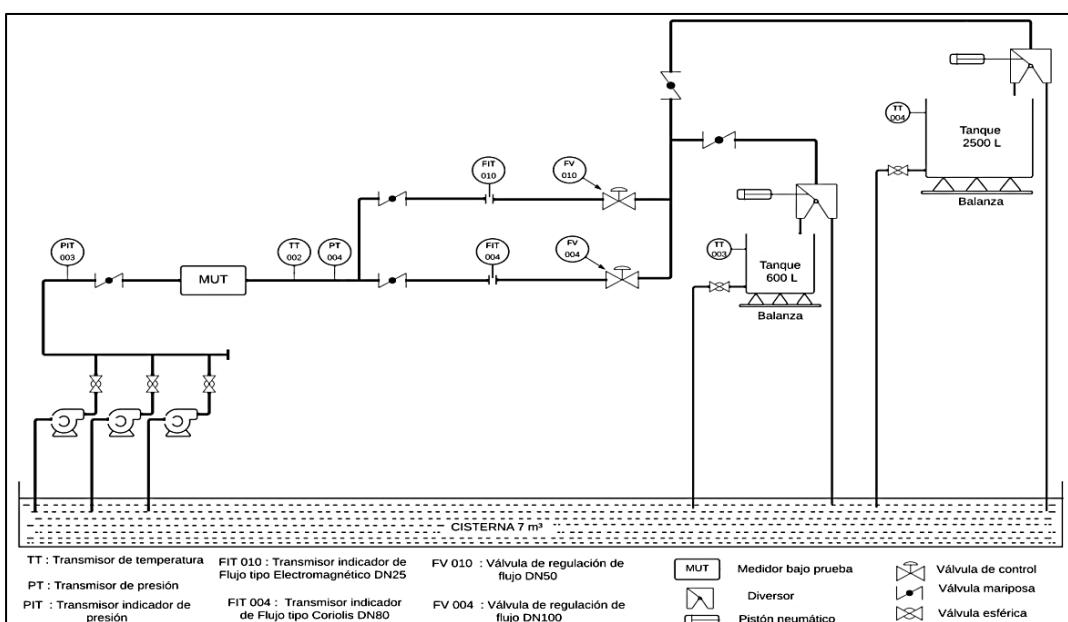
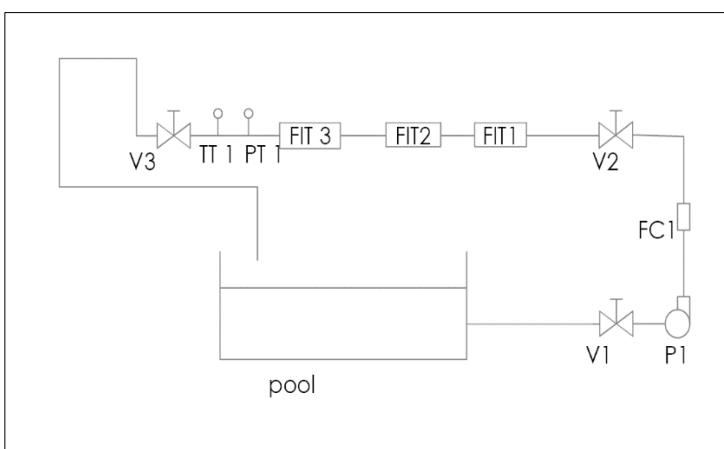


Fig. 3: Instrumentation diagram and the main components of the Static Weighing System

Characteristic information of primary standard used during SC	Working procedure																
IBMETRO – Bolivia <table border="1" data-bbox="203 354 778 720"> <tr> <td>Range of flowrate</td> <td>3 m³/h – 100 m³/h</td> </tr> <tr> <td>Fluid temperature</td> <td>16 °C – 28 °C</td> </tr> <tr> <td>Line pressure</td> <td>up to 3 bar</td> </tr> <tr> <td>Uncertainty (k = 2)</td> <td>0.10 %</td> </tr> <tr> <td>Reference</td> <td>master meter (Electromagnetic Flow meter)</td> </tr> <tr> <td>Operating method</td> <td>flying start stop</td> </tr> <tr> <td>Calibration line diameter</td> <td>50 mm ... 125 mm</td> </tr> <tr> <td>Test fluid</td> <td>water</td> </tr> </table>	Range of flowrate	3 m ³ /h – 100 m ³ /h	Fluid temperature	16 °C – 28 °C	Line pressure	up to 3 bar	Uncertainty (k = 2)	0.10 %	Reference	master meter (Electromagnetic Flow meter)	Operating method	flying start stop	Calibration line diameter	50 mm ... 125 mm	Test fluid	water	The calibration points of the flow meter under test (MUT) are established according to the comparison standards. Start the data acquisition program in the computer to determine the number of pulses to capture. The pulses were collected from MUT and the Electromagnetic Flow meter (reference meter). For each measurement, record the number of pulses from the reference meter and MUT. Also, fluid temperature, line pressure and measurement time were recorded. The ambient conditions at the beginning and at the end of each test flow were recorded.
Range of flowrate	3 m ³ /h – 100 m ³ /h																
Fluid temperature	16 °C – 28 °C																
Line pressure	up to 3 bar																
Uncertainty (k = 2)	0.10 %																
Reference	master meter (Electromagnetic Flow meter)																
Operating method	flying start stop																
Calibration line diameter	50 mm ... 125 mm																
Test fluid	water																



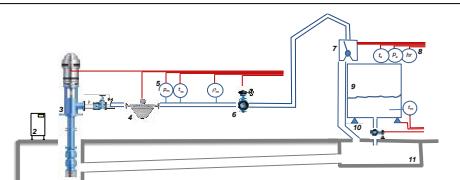
Calibration line



TAG	DESCRIPTION
V1	Valve
P1	Pump
FC1	Flow stabilizer
V2	Valve
FIT 1	Meter under Test Turbine
FIT 2	Meter under Test Coriolis
FIT 3	Flow meter Krohne
PT 1	Pressure Sensor
TT 1	Temperature Sensor
V3	Valve
pool	Recipe

Schematic diagram of the flow line

Characteristic information of primary standard used during SC	Working procedure
INTI - Argentina	
Range of flowrate	0.12 m ³ /h – 130 m ³ /h
Fluid temperature	15 °C – 30 °C
Line pressure	up to 3 bar
Uncertainty (k = 2)	Volumetric tank mass: 0.07 % volume: 0.06 % Master meter mass: 0.22 % volume: 0.20 %
Reference	Volumetric tank Master meter (turbine meter)
Operating method	standing-start-stop
Calibration line diameter	25 mm, 50 mm, 100 mm, 150 mm
Test fluid	water
	
Installed MUT during comparison calibration	
	Reference turbine meter
	
Calibration test rig	

Characteristic information of primary standard used during KC	Working procedure
CENAM – Mexico	
Range of flow rate	(100... 12 000) kg/min
Fluid temperature	Ambient (not controlled) (15...27) °C
Line pressure	up to 10 bar
Uncertainty	$U(q_m)/\% = 0.030$ $U(q_v)/\% = 0.038$ $k = 2$
Reference	Gravimetric
Operating method	Flying-start-stop
Calibration line diameter	100 mm 200 mm
Test fluid	Water
	The Mexican Primary Measurement System for Water Flow is of the Static Weighing Design. The gravimetric reference consists of two independent diverter and weighing systems; which maximum load capacities are 1500 kg and 10 000 kg, respectively. Flow is controlled by means of frequency converter and throttling valves. More than 100D upstream pipe length is available for calibrations. No fluid temperature control available.
	
<p>Fig. 1: Schematic diagram of CENAM water flow facility</p>	
<p>Fig. 2: A view of the load cell at the 10 000 kg tank</p>	

Characteristic information of primary standard used during KC	Working procedure																
PTB – Germany <table border="1" data-bbox="203 361 695 826"> <tr> <td>Range of flowrate</td> <td>0.3 m³/h ... 2,100 m³/h</td> </tr> <tr> <td>Fluid temperature</td> <td>10 °C ... 35 °C</td> </tr> <tr> <td>Line pressure</td> <td>2 bar ... 6 bar</td> </tr> <tr> <td>Uncertainty ($k = 2$)</td> <td>0.02 volume, mass</td> </tr> <tr> <td>Reference</td> <td>gravimetric</td> </tr> <tr> <td>Operating method</td> <td>Direct pumping , constant head tank flying-/ standing- start-stop</td> </tr> <tr> <td>Calibration line diameter</td> <td>25 mm ... 400 mm</td> </tr> <tr> <td>Test fluid</td> <td>water</td> </tr> </table>	Range of flowrate	0.3 m ³ /h ... 2,100 m ³ /h	Fluid temperature	10 °C ... 35 °C	Line pressure	2 bar ... 6 bar	Uncertainty ($k = 2$)	0.02 volume, mass	Reference	gravimetric	Operating method	Direct pumping , constant head tank flying-/ standing- start-stop	Calibration line diameter	25 mm ... 400 mm	Test fluid	water	<p>The PTB hydrodynamic test field (HDP) represents the national primary standard of Germany for the realization of the measurands volumetric and mass flow rate as well as the total volume and mass of flowing liquids (water). The gravimetric reference consists of three independent diverter and balance systems with max. loads of 30 t, 3 t and 300 kg. For generating and stabilizing flow rates, the supply system consists of a 400 m³ storage tank, of a frequency controlled pumping system, a constant head tank (30 m³, at a height of 30 m) and two calibration lines. For each diameter an upstream straight pipeline with a length of 50D and downstream of 20D is available. The fluid temperature is adjusted and controlled by two separate heat exchanger systems.</p>
Range of flowrate	0.3 m ³ /h ... 2,100 m ³ /h																
Fluid temperature	10 °C ... 35 °C																
Line pressure	2 bar ... 6 bar																
Uncertainty ($k = 2$)	0.02 volume, mass																
Reference	gravimetric																
Operating method	Direct pumping , constant head tank flying-/ standing- start-stop																
Calibration line diameter	25 mm ... 400 mm																
Test fluid	water																

An overhead photograph showing a complex industrial setup. On the left, a large white storage tank is connected to a network of pipes. A blue control cabinet with a screen sits on a table in the center. To the right, there's a large metal structure and various smaller components. The floor is concrete with some equipment and cables visible.

Upstream view to calibration lines

A photograph of a large industrial machine. It features a central vertical column with a horizontal platform or walkway around it. Various pipes, valves, and sensors are attached to the structure. A yellow circular device, possibly a sensor or part of a balance system, is mounted on one of the vertical supports.

3 t balance and diverter system

A schematic diagram of the hydrodynamic test field. It shows a flow path starting from a 'Storage tank' on the left, which feeds into a 'Pumps' section. The flow then enters a 'Balance foundation' where a 'Meter under test' is positioned. Above the foundation is a 'Weighing systems with diverters'. The flow continues through a 'Constant head tank' at the top right. A 'Pipe prover' is shown at the bottom right. Labels include: Weighing systems with diverters, Constant head tank, Storage tank, Balance foundation, Pumps, Pipe prover, and Meter under test.

Principle drawing of the Hydrodynamic Test Field

11.2 Detailed data report of participating laboratories

CISA laboratory – Day#1

Data report CISA : Day#1												*Original data set	Temperature correction of meter error													
Date	Nominal flow rate	Measurement time	Turbine meter												Coriolis Mass											
			V_{nom}	t	m_{ref}	m_{ref}	V_{ref}	m_{ref}	ρ_{fluid}	T_{fluid}	T_{air}	p_{air}	N	K_V	e_V	N	K_m	θ_m	Pulse count	K-factor	Meter error	$(T_{fluid} - T_{nom})$	ΔT_{fluid}	ϵ_{corr}	ϵ_{corr}	ϵ_{corr}
28.04.2016	10	352.513	[m³/h]	[s]	10.221	10.234	1003.726	1.005	998.759	2.93	23.16	24.83	1.01	11491	11.4341	0.443	144069	143.5342	0.362	28837	28.6943	-0.367	3.160	-0.474	-0.321	
28.04.2016	10	353.039	[m³/h]	[s]	10.232	10.245	1003.424	1.005	998.447	2.96	23.20	25.24	1.01	11457	11.4036	-0.709	144077	143.5844	0.327	28841	28.7066	-0.324	3.000	-0.740	-0.386	
28.04.2016	10	352.740	[m³/h]	[s]	10.244	10.257	1003.727	1.005	998.711	2.98	23.32	24.74	1.01	11475	11.4177	-0.586	144073	143.5380	0.360	28842	28.6979	-0.355	3.320	-0.618	-0.317	
28.04.2016	10	353.506	[m³/h]	[s]	10.225	10.241	1004.324	1.006	998.516	2.99	23.94	25.79	1.01	11483	11.4166	-0.596	144078	143.4577	0.415	28851	28.6841	-0.402	3.940	-0.627	-0.364	
28.04.2016	10	353.124	[m³/h]	[s]	10.240	10.254	1004.424	1.006	998.606	2.93	23.66	25.69	1.01	11472	11.4055	-0.692	144076	143.4414	0.427	28845	28.6779	-0.424	3.650	-0.723	-0.379	
28.04.2016	30	240.100	[m³/h]	[s]	30.047	30.088	2003.957	2.007	998.634	2.90	23.57	25.87	1.01	23266	11.4246	-0.991	288149	143.7900	-0.385	57434	28.6211	-0.621	3.570	-0.78	-0.338	
28.04.2016	30	240.935	[m³/h]	[s]	30.270	30.402	2004.861	2.007	998.598	2.95	23.70	25.61	1.01	23038	11.4761	-0.078	288169	143.7496	-0.213	57446	28.6169	-0.352	3.700	-0.664	-0.365	
28.04.2016	30	240.020	[m³/h]	[s]	30.114	30.126	2003.563	2.008	998.567	2.97	23.78	25.46	1.01	23039	11.4751	-0.086	288184	143.7426	-0.218	57446	28.6123	-0.352	3.780	-0.672	-0.369	
28.04.2016	30	239.771	[m³/h]	[s]	30.082	30.126	2003.563	2.007	998.529	3.01	23.90	25.25	1.01	23022	11.4736	-0.099	288144	143.8158	-0.167	57430	28.6218	-0.199	3.900	-0.884	-0.316	
28.04.2016	30	239.912	[m³/h]	[s]	30.087	30.132	2005.063	2.008	998.599	2.97	23.99	25.32	1.01	23045	11.4762	-0.077	288150	143.7112	-0.239	57438	28.6035	-0.182	3.950	-0.661	-0.383	
28.04.2016	60	120.809	[m³/h]	[s]	30.006	29.984	2002.666	2.006	998.433	3.01	24.19	24.74	1.01	22989	11.4612	-0.207	288172	143.8942	-0.112	57090	28.6423	-1.172	4.190	-0.181	-0.058	
28.04.2016	60	120.365	[m³/h]	[s]	60.017	2003.766	2.007	998.389	3.04	24.32	24.88	1.01	23003	11.4614	-0.206	288218	143.8382	-0.151	57095	28.6479	-1.222	4.220	-0.178	-0.065		
28.04.2016	60	120.506	[m³/h]	[s]	60.125	2004.660	2.008	998.461	3.12	24.40	24.82	1.01	23018	11.4657	-0.168	288128	143.8028	-0.176	57098	28.6415	-1.245	4.400	-0.140	-0.119		
28.04.2016	60	120.391	[m³/h]	[s]	60.070	2003.366	2.007	998.320	3.04	24.52	24.79	1.01	23014	11.4684	-0.145	288194	143.8549	-0.140	57095	28.6516	-1.210	4.520	-0.116	-0.081		
28.04.2016	60	120.518	[m³/h]	[s]	60.081	59.981	2004.970	2.008	998.274	3.02	24.65	24.51	1.01	23032	11.4676	-0.151	288207	143.7463	0.215	57102	28.6311	-1.281	4.450	-0.122	-0.055	
28.04.2016	100	108.639	[m³/h]	[s]	109.597	98.776	3005.586	3.011	998.202	2.43	24.85	24.68	1.01	34507	11.4603	-0.215	43283	143.8265	-0.159	86769	28.8173	0.060	4.850	-0.193	-0.096	
28.04.2016	100	108.317	[m³/h]	[s]	109.102	3006.282	3.012	998.140	2.46	25.02	24.85	1.01	34516	11.4599	-0.218	43253	143.7833	-0.189	86743	28.8002	0.001	5.020	-0.196	-0.058		
28.04.2016	100	108.397	[m³/h]	[s]	109.933	3005.084	3.011	998.095	2.45	25.14	24.79	1.01	34500	11.4587	-0.229	432347	143.8719	-0.128	86753	28.8138	0.048	5.140	-0.206	-0.061		
28.04.2016	100	108.368	[m³/h]	[s]	109.806	100.000	3004.389	3.010	998.061	2.47	25.23	24.47	1.01	34477	11.4533	-0.276	432306	143.8915	-0.114	86771	28.8254	0.088	5.230	-0.252	-0.046	
28.04.2016	100	108.428	[m³/h]	[s]	109.741	99.941	3004.095	3.010	998.000	2.47	25.39	24.09	1.01	34482	11.4554	-0.258	432326	143.8809	-0.115	86773	28.8271	0.096	5.390	-0.234	-0.044	
28.04.2016	110	98.468	[m³/h]	[s]	109.874	110.109	3005.300	3.012	997.871	2.28	25.72	23.70	1.01	34501	11.4556	-0.256	432332	143.8865	-0.138	86765	28.8092	0.032				
28.04.2016	110	98.097	[m³/h]	[s]	110.286	110.225	3005.201	3.012	997.885	2.31	25.81	23.66	1.01	34500	11.4556	-0.256	432402	143.8846	-0.119	86784	28.8154	0.053				
28.04.2016	110	98.245	[m³/h]	[s]	110.065	110.399	3003.702	3.010	997.786	2.29	25.93	23.63	1.01	34483	11.4547	-0.263	432329	143.9321	-0.086	86779	28.8267	0.093				
28.04.2016	110	98.058	[m³/h]	[s]	110.312	110.460	3004.704	3.011	997.753	2.26	26.01	23.43	1.01	34497	11.4552	-0.259	432293	143.8721	-0.128	86765	28.8115	0.040				
28.04.2016	110	98.762	[m³/h]	[s]	109.536	109.787	3005.007	3.012	997.720	2.23	26.09	23.27	1.01	34518	11.4506	-0.212	432272	143.8506	-0.143	86739	28.7950	-0.003				

CISA laboratory – Day#2

Data report CISA: Day#2												*Original data set														
Turbine meter												Coriolis Mass														
Laboratory reference												Ambient conditions														
Fluid												Pulses/liter														
Date	Nominal flowrate	Standard mass flowrate	Standard volume flowrate	Mass	Volume	Water density	Water temp.	Air pressure	Air temp.	Line temp.	Pulse count	K-factor	Meter error	Pulse count	K-factor	Meter error	Pulse count	K-factor	Meter error	Pulse count	K-factor	Meter error	Turbine meter	Coriolis Mass		
	V_{nom}	m_{ref}	V_{ref}	m_{ref}	V_{ref}	ρ_{fluid}	T_{fluid}	p_{Ar}	T_{air}	θ_m	K_V	e_V	N	K_m	θ_m	N	K_V	e_V	N	K_m	θ_m	T_{nom}	$K_{V,nom}$	$K_{m,nom}$		
	[m³/h]	[kg/h]	[l/h]	[kg]	[m³]	[kg/m³]	[°C]	[bar]	[°C]	[°C]	[Pulses]	[Pulses/Liter]	[%]	[Pulses]	[kg]	[%]	[Pulses]	[kg]	[%]	[Pulses]	[kg]	[%]	[°C]	7nom	20	°C
29.04.2016	10	355.677	10.131	10.147	1000.924	1.003	998.989	2.97	24.32	24.34	1.01	11437	-11.4080	-0.670	143.9320	-0.086	28845	28.7719	-0.097	4.320	-0.701	-0.030				
29.04.2016	10	355.301	10.145	10.145	1001.228	1.003	998.942	2.96	23.86	23.51	1.01	11428	-11.3973	-0.763	143.9077	-0.108	28843	28.7655	-0.115	3.860	-0.795	-0.038				
29.04.2016	10	355.699	10.132	10.148	1001.126	1.003	998.986	2.99	24.03	23.91	1.01	11430	-11.3999	-0.741	143.9110	-0.101	28843	28.7669	-0.115	4.030	-0.772	-0.048				
29.04.2016	10	354.861	10.154	10.170	1000.925	1.002	998.959	2.98	24.11	24.07	1.01	11437	-11.4088	-0.663	143.9339	-0.084	28844	28.7730	-0.094	4.110	-0.694	-0.031				
29.04.2016	10	355.366	10.147	10.163	1001.726	1.003	998.933	2.99	24.19	24.09	1.01	11428	-11.3904	-0.823	143.9272	-0.165	28844	28.7492	-0.176	4.150	-0.854	-0.107				
29.04.2016	30	240.313	29.989	30.056	2001.872	2.005	998.933	2.90	24.19	24.01	1.01	22972	-11.4573	-0.241	143.9433	-0.078	57447	28.6517	-0.515	4.190	-0.224	-0.024				
29.04.2016	30	239.957	30.023	30.071	2001.170	2.004	998.902	2.94	24.28	24.11	1.01	22965	-11.4575	-0.240	143.9933	-0.040	57447	28.6698	-0.483	4.280	-0.221	0.015				
29.04.2016	30	240.082	30.031	30.081	2002.770	2.006	998.934	2.97	24.48	21.19	1.01	22892	-11.4610	-0.209	143.8707	-0.129	57437	28.6310	-0.587	4.480	-0.189	-0.070				
29.04.2016	30	240.320	30.009	30.060	2003.266	2.007	998.906	2.94	24.56	24.70	1.01	22998	-11.4558	-0.254	143.8456	-0.146	57448	28.6286	-0.595	4.560	-0.233	-0.087				
29.04.2016	30	240.359	30.001	30.053	2003.064	2.007	998.960	2.94	24.69	24.91	1.01	22959	-11.4619	-0.201	143.8651	-0.132	57457	28.6346	-0.574	4.690	-0.179	-0.071				
29.04.2016	60	120.353	59.918	60.013	2003.157	2.006	998.933	2.99	24.19	25.16	1.01	22972	-11.4499	-0.305	143.8938	-0.114	57094	28.4573	-1.190	4.190	-0.279	-0.050				
29.04.2016	60	120.201	59.946	60.032	2001.551	2.004	998.967	2.97	23.78	25.93	1.01	22968	-11.4487	-0.316	143.9818	-0.051	50706	28.4750	-1.138	3.780	-0.292	-0.003				
29.04.2016	60	120.230	59.959	60.046	2002.449	2.005	998.942	2.91	23.86	26.16	1.01	22964	-11.4512	-0.294	143.9923	-0.086	50781	28.4640	-1.167	3.860	-0.270	-0.036				
29.04.2016	60	120.274	59.943	60.033	2002.651	2.006	998.999	2.94	23.99	25.88	1.01	22961	-11.4481	-0.321	143.8968	-0.111	50707	28.4579	-1.188	3.990	-0.296	-0.059				
29.04.2016	60	120.250	59.976	60.067	2003.354	2.006	998.973	2.97	24.07	25.60	1.01	22963	-11.4448	-0.350	143.8818	-0.141	50706	28.4467	-1.227	4.070	-0.324	-0.088				
29.04.2016	100	108.347	99.848	100.020	3005.073	3.010	998.988	2.42	24.61	24.96	1.01	30482	-11.4550	-0.262	143.2323	-0.133	8670	28.8251	0.087	4.610	-0.241	-0.073				
29.04.2016	100	107.287	100.805	101.005	3004.177	3.010	998.016	2.46	25.35	24.55	1.01	30481	-11.4549	-0.262	143.2289	-0.111	86758	28.8218	0.076	5.350	-0.238	-0.041				
29.04.2016	100	107.985	100.173	100.357	3004.779	3.010	998.169	2.48	24.94	24.39	1.01	30476	-11.4527	-0.281	143.2320	-0.124	86755	28.8196	0.069	4.940	-0.259	-0.060				
29.04.2016	100	108.190	99.983	100.171	3004.481	3.010	998.125	2.46	25.06	24.23	1.01	30479	-11.4543	-0.267	143.2295	-0.120	86733	28.8138	0.048	5.060	-0.244	-0.054				
29.04.2016	100	108.290	99.878	100.072	3004.381	3.010	998.061	2.37	25.23	24.31	1.01	30483	-11.4553	-0.258	143.2334	-0.112	86762	28.8225	0.078	5.230	-0.235	-0.044				
29.04.2016	110	99.945	109.641	109.641	306.777	3.013	997.987	2.30	25.68	24.41	1.01	30458	-11.4508	-0.298	143.2333	-0.192	86769	28.7968	-0.011							
29.04.2016	110	99.045	109.423	109.423	3003.877	3.010	997.902	2.32	25.89	24.49	1.01	30471	-11.4503	-0.302	143.2375	-0.081	86781	28.8262	0.091							
29.04.2016	110	99.156	109.866	109.331	3004.581	3.011	997.753	2.33	26.01	24.21	1.01	30476	-11.4487	-0.316	143.2286	-0.125	86816	28.8296	0.103							
29.04.2016	110	99.119	109.155	109.407	3005.380	3.012	997.699	2.24	26.14	24.18	1.01	30492	-11.4503	-0.302	143.2287	-0.152	86771	28.8055	0.019							
29.04.2016	110	98.800	109.450	109.708	3003.782	3.011	997.948	2.28	26.26	24.12	1.01	30476	-11.4505	-0.300	143.2320	-0.091	86780	28.8223	0.077							

CISA laboratory – Day#3

Data report CISA; Day#3												*Original data set										
Date	Nominal flowrate [m³/h]	Measur- ement time [s]	Laboratory reference						Turbine meter						Coriolis_Mass		Coriolis_Vol		Temperature correction of meter error			
			Standard mass flowrate [kg/s]	Standard volume flowrate [l/h]	m^* [kg]	V^* [l/h]	m_{ref}	V_{ref}	Water density [kg/m³]	Line pressure [bar]	Air temp. [°C]	Air pressure [bar]	Pulse count	K-factor	Meter error [%]	Pulse count	K-factor	Meter error [%]	T_{fluid} [°C]	T_{nom} [°C]	ΔT_{fluid} [°C]	T _{nom} [°C]
04.05.2016	10	357.301	10.134	10.142	1.005.850	1.007	999.230	3.00	21.42	20.71	1.01	11.4271	-0.504	144067	143.2292	-0.574	28.6383	-0.562	14.20	-0.532	-0.535	
04.05.2016	10	357.852	10.119	10.127	1.005.849	1.007	999.178	3.04	21.63	20.88	1.01	11.4079	-0.714	144065	143.2277	-0.575	28.6378	-0.563	14.30	-0.742	-0.533	
04.05.2016	10	359.076	10.089	10.098	1.006.350	1.007	999.158	3.02	21.71	20.99	1.01	11.4089	-0.682	144065	143.1560	-0.625	28.6210	-0.622	17.10	-0.711	-0.602	
04.05.2016	10	358.458	10.105	10.114	1.006.149	1.007	999.115	3.03	21.15	21.88	1.01	11.4198	-0.585	144075	143.1945	-0.598	28.6294	-0.592	1.880	-0.614	-0.573	
04.05.2016	10	358.241	10.114	10.123	1.006.449	1.007	999.083	3.04	22.00	21.27	1.01	11.4202	-0.565	144065	143.1419	-0.635	28.6170	-0.635	2.00	-0.594	-0.608	
04.05.2016	10	359.369	10.083	10.093	1.006.549	1.007	999.062	3.00	22.08	21.38	1.01	11.4167	-0.644	144072	143.1346	-0.640	28.6166	-0.637	2.080	-0.673	-0.612	
04.05.2016	10	358.912	10.098	10.108	1.006.748	1.008	999.028	3.06	22.21	21.55	1.01	11.4308	-0.472	144068	143.1023	-0.662	28.6089	-0.663	2.210	-0.502	-0.633	
04.05.2016	10	358.533	10.110	10.122	1.006.840	1.008	998.798	3.05	23.03	23.45	1.01	11.4389	-0.766	144071	143.0932	-0.669	28.6035	-0.607	3.030	-0.797	-0.630	
04.05.2016	10	359.414	10.087	10.097	1.007.048	1.008	998.960	3.05	22.46	21.84	1.01	11.4390	-0.759	144072	143.0637	-0.688	28.6034	-0.683	2.460	-0.790	-0.657	
04.05.2016	10	358.526	10.108	10.120	1.006.637	1.008	998.783	3.04	23.08	24.24	1.01	11.4285	-0.778	144070	143.1202	-0.650	28.6110	-0.556	3.080	-0.809	-0.610	
04.05.2016	60	119.885	60.195	60.262	2.004.574	2.007	998.879	2.97	22.75	24.77	1.01	22.986	-0.270	28.6238	28.5073	-0.185	28.3915	-0.253	-0.253	-0.149		
04.05.2016	60	119.681	60.255	60.345	2.003.167	2.006	998.516	2.98	23.94	25.53	1.01	22.998	-0.167	28.6193	28.4501	-0.130	28.4501	-0.212	3.940	-0.161	-0.079	
04.05.2016	60	119.978	60.175	60.249	2.005.477	2.008	998.783	2.92	23.08	24.49	1.01	23.993	-0.297	28.6240	28.4764	-0.229	28.6249	-0.277	3.080	-0.277	-0.189	
04.05.2016	60	119.800	60.271	60.346	2.005.674	2.008	998.446	2.91	23.20	24.85	1.01	22.96	-0.453	28.6222	28.4703	-0.245	28.6261	-0.273	3.200	-0.298	-0.203	
04.05.2016	60	119.860	60.201	60.293	2.004.367	2.007	998.486	2.90	24.03	25.55	1.01	23.904	-0.597	28.6220	28.4395	-0.220	28.6239	-0.195	4.030	-0.195	-0.122	
04.05.2016	60	119.840	60.208	60.288	2.004.266	2.007	998.684	2.88	23.41	25.74	1.01	23.003	-0.4621	28.6228	28.4333	-0.200	28.6228	-0.173	5.0763	-0.173	-0.129	
04.05.2016	60	119.892	60.212	60.294	2.005.266	2.008	998.646	2.84	23.53	25.81	1.01	23.033	-0.124	28.6264	28.4755	-0.210	28.6260	-0.129	3.530	-0.101	-0.164	
04.05.2016	60	119.771	60.258	60.342	2.004.766	2.008	998.606	2.94	23.66	25.90	1.01	23.038	-0.124	28.6265	28.4789	-0.165	28.6265	-0.168	3.660	-0.100	-0.137	
04.05.2016	60	119.804	60.226	60.312	2.004.265	2.007	998.580	2.90	23.74	25.96	1.01	23.025	-0.118	28.6198	28.4794	-0.183	28.6197	-0.188	3.740	-0.094	-0.135	
04.05.2016	60	119.879	60.183	60.270	2.004.066	2.007	998.555	2.87	23.82	25.74	1.01	23.026	-0.105	28.6200	28.4806	-0.172	28.6200	-0.172	3.469	-0.126	-0.123	
04.05.2016	110	97.692	110.746	110.889	3.005.267	3.009	998.714	2.20	23.32	26.54	1.01	344711	-0.4555	-0.257	43.2352	143.8648	-0.133	86.701	28.8125	0.043	0.043	
04.05.2016	110	98.387	109.982	110.132	3.005.769	3.010	998.634	2.27	23.57	26.38	1.01	344688	-0.1584	-0.232	43.2356	143.8420	-0.149	86.714	28.8098	0.034	0.034	
04.05.2016	110	98.123	110.259	110.421	3.005.276	3.010	998.542	2.26	23.86	25.83	1.01	344733	-0.1540	-0.270	43.2273	143.8381	-0.151	86.737	28.8195	0.068	0.068	
04.05.2016	110	98.156	110.211	110.377	3.004.975	3.009	998.499	2.24	23.99	25.89	1.01	344689	-0.1454	-0.285	43.2258	143.8475	-0.145	86.729	28.8185	0.064	0.064	
04.05.2016	110	98.262	110.089	110.260	3.004.877	3.010	998.446	2.29	24.15	25.66	1.01	344688	-0.1528	-0.280	43.2306	143.8681	-0.130	86.741	28.8219	0.076	0.076	
04.05.2016	110	97.715	110.694	110.871	3.004.265	3.009	998.578	2.20	24.28	25.61	1.01	344567	-0.1489	-0.306	43.2278	143.8731	-0.127	86.694	28.8079	0.027	0.027	
04.05.2016	110	97.926	110.482	110.669	3.005.282	3.010	998.306	2.25	24.56	25.23	1.01	344777	-0.14527	-0.281	43.2298	143.8461	-0.146	86.737	28.8126	0.044	0.044	
04.05.2016	110	98.357	110.056	110.248	3.006.881	3.012	998.260	2.22	24.69	25.24	1.01	344688	-0.157	-0.277	43.2357	143.8158	-0.167	86.797	28.8159	0.055	0.055	
04.05.2016	110	98.274	110.105	110.302	3.005.680	3.011	998.217	2.25	24.81	25.32	1.01	344681	-0.153	-0.293	43.2317	143.8333	-0.155	86.742	28.8079	0.027	0.027	
04.05.2016	110	98.230	110.132	110.333	3.005.081	3.011	998.184	2.19	24.90	25.32	1.01	344684	-0.143	-0.324	43.2281	143.8560	-0.143	86.744	28.8134	0.046	0.046	

INACAL Laboratory – Day#1

Data report INACAL: Day#1												*Original data set		Temperature correction of meter error						
Date	Nominal flowrate	Measurement time	Turbine meter						Coriolis_Mass			Coriolis_Vol			T_{nom}	20	°C			
			$K_{V,\text{nom}}$	11.4850	Pulses/Liter	$K_{m,\text{nom}}$	144.0560	Pulses/kg	$K_{V,\text{nom}}$	28.8000	Pulses/Liter	$K_{V,\text{nom}}$	28.8000	Pulses/Liter						
Laboratory reference																				
			Fluid	Ambient conditions																
				Standard volume flowrate	Mass	Volume	Water density	Line pressure	Air temp.	Air pressure	Pulse count	K-factor	Meter error	Pulse count	K-factor	Meter error	Corrected meter error			
			V^*_{ref}	m^*_{ref}	V_{ref}	m_{ref}	ρ_{fluid}	T_{air}	p_{air}	N	K_V	θ_V	N	K_m	θ_m	ΔT_{fluid}	Turbine meter			
			$[m^3/h]$	$[s]$	$[m^3]$	$[kg]$	$[kg/m^3]$	$[\text{bar}]$	$[\text{C}]$	[Pulses]	[Pulses]	[Pulses/Lef]	[Pulses]	[Pulses/kg]	[Pulses/Lef]	[°C]	$\theta_{\text{cor},m}$			
13.03.2017	10	118.482	10.302	338.086	0.339	987.161	2.15	25.57	24.80	3910	992.70	0.412	48779	144.2798	0.155	0.168	28.8484	0.384		
13.03.2017	10	141.597	10.210	401.595	0.403	987.272	2.15	25.00	992.40	4644	11.5323	0.412	57906	144.1899	0.093	0.124	28.8358	0.383		
13.03.2017	10	133.559	10.061	10.090	373.267	0.374	987.161	2.15	25.57	25.00	992.40	4338	11.5353	0.438	53803	144.1406	0.093	0.124	28.8275	0.386
13.03.2017	10	141.591	10.042	10.070	394.952	0.395	987.158	2.15	25.58	25.00	992.40	4567	11.5306	0.397	56924	144.1290	0.051	0.146	28.8227	0.379
13.03.2017	10	134.009	10.008	10.037	372.560	0.374	987.156	2.15	25.59	25.30	992.30	4310	11.5357	0.441	53722	144.1968	0.098	0.108	28.8312	0.394
13.03.2017	30	231.027	30.141	30.227	1934.260	1.940	987.141	2.19	25.65	25.30	991.80	22393	11.5439	0.513	278389	143.9305	-0.087	0.573	28.6487	-0.525
13.03.2017	30	230.808	30.121	30.208	1931.162	1.937	987.120	2.19	25.73	25.40	991.60	22354	11.5421	0.497	277988	143.9486	-0.075	0.547	28.6450	-0.538
13.03.2017	30	228.048	30.119	30.207	1907.970	1.914	987.096	2.19	25.82	25.40	991.40	22079	11.5384	0.465	274659	143.9535	-0.071	0.548	28.6461	-0.535
13.03.2017	30	227.785	30.104	30.194	1904.871	1.910	987.076	2.19	25.90	25.60	991.30	22045	11.5391	0.471	274040	144.0040	-0.036	0.545	28.6607	-0.484
13.03.2017	30	230.657	30.116	30.205	1929.562	1.935	987.041	2.19	26.03	25.60	991.10	22235	11.5357	0.442	277888	144.0161	-0.028	0.5454	28.6541	-0.506
13.03.2017	60	116.570	60.008	60.188	1949.755	1.956	987.001	2.02	26.18	25.70	990.90	22587	11.5498	0.564	280887	144.0627	0.005	0.5718	28.6192	-1.072
13.03.2017	60	117.683	60.011	60.194	1961.751	1.968	986.960	2.02	26.33	25.90	990.80	22709	11.5407	0.485	282661	144.0861	0.021	0.524	28.4983	6.333
13.03.2017	60	117.300	59.916	60.101	1952.254	1.958	986.922	2.01	26.47	25.90	990.80	22602	11.5418	0.494	281358	144.1196	0.044	0.534	28.5061	1.020
13.03.2017	60	117.230	59.961	60.148	1952.554	1.959	986.884	2.01	26.61	26.00	990.80	22614	11.5457	0.528	281414	144.1261	0.049	0.5833	28.5058	-1.022
13.03.2017	60	119.703	59.909	60.099	1992.040	1.958	986.845	2.01	26.76	26.00	990.60	23085	11.5521	0.584	282718	144.1327	0.053	0.5694	28.5056	-1.022
13.03.2017	100	72.162	99.363	99.685	1991.740	1.998	986.777	2.00	27.01	26.00	990.40	23074	11.5475	0.544	287080	144.1353	0.055	0.5744	28.8983	0.341
13.03.2017	100	70.122	99.386	100.317	1947.556	1.954	986.706	2.02	27.26	26.10	990.30	22552	11.5415	0.492	280663	144.1104	0.038	0.5644	28.8865	0.300
13.03.2017	100	70.300	100.572	100.912	1963.950	1.971	986.630	2.03	27.54	26.20	990.10	22739	11.5392	0.472	283034	144.1147	0.041	0.5693	28.8863	0.300
13.03.2017	100	70.982	99.712	100.095	1966.049	1.973	986.576	2.00	27.73	26.20	990.10	22779	11.5465	0.536	282337	144.1098	0.037	0.5697	28.8807	0.380
13.03.2017	100	70.817	100.051	100.400	1968.148	1.975	986.526	2.01	27.91	26.30	989.90	22802	11.5453	0.525	285856	144.0877	0.022	0.5704	28.8778	0.270
13.03.2017	130	54.974	129.147	129.608	1972.147	1.979	986.446	1.70	28.19	26.30	989.80	22869	11.5548	0.608	284193	144.1034	0.033	0.57167	28.8842	0.292
13.03.2017	130	55.121	129.561	130.034	1983.743	1.991	986.363	1.97	28.48	26.20	990.00	23007	11.5556	0.615	282821	144.0817	0.018	0.5746	28.8782	0.271
13.03.2017	130	54.080	129.332	129.829	1942.857	1.950	986.169	2.00	29.15	26.20	990.00	22498	11.5355	0.440	279933	144.0780	0.015	0.56326	28.8803	0.279
13.03.2017	130	54.571	129.738	130.249	1966.649	1.974	986.078	2.01	29.46	26.30	990.20	22774	11.5347	0.433	282824	144.0440	-0.008	0.5704	28.8717	0.249
13.03.2017	130	54.586	129.332	129.853	1961.051	1.969	995.993	1.99	29.75	26.30	990.20	22726	11.5422	0.498	282459	144.0345	-0.015	0.56838	28.8673	0.234

INACAL Laboratory – Day#2

Data report INACAL: Day#2												*Original data set												
												Temperature correction of meter error												
												Turbine meter												
												K _{V,nom}	11.4850	Pulses/Liter	K _{V,nom}	144.0560	Pulses/kg	K _{V,nom}	28.8000	Pulses/liter	T _{nom}	20	°C	
Date	Nominal flowrate	Measurement time	Standard mass flowrate	Standard volume flowrate	Mass	Volume	Water density	Line pressure	Air temp.	Air pressure	Ambient conditions													Corrected meter error
V _{nom} [m ³ /h]	t [s]	m _{ref} [kg/h]	V _{ref} [l/h]	m _{ref} [g]	m _{ref} [m ³]	V _{ref} [m ³]	ρ _{fluid} [kg/m ³]	p _{fluid} [bar]	T _{air} [°C]	P _{air} [Pulses]	K _V	e _V	N	K _m	e _m	N	K _V	e _V	N	K _m	e _m	Δ T _{fluid} [°C]	e _{cor,v} [%]	
14.03.2017	10	152.569	10.411	441.211	0.443	996.354	2.08	28.51	22.70	993.80	503	11.4786	-0.056	62986	142.7521	-0.902	12639	28.50472	-0.897	8.512	-0.955	-0.786		
14.03.2017	10	137.512	10.299	393.385	0.395	996.365	2.08	28.47	23.10	993.90	4537	11.4913	0.055	56167	142.7786	-0.887	11271	28.50472	-0.878	8.473	0.046	-0.771		
14.03.2017	10	137.043	10.302	392.160	0.384	996.365	2.08	28.47	22.70	993.70	4522	11.4891	0.036	56059	142.6943	-0.945	11229	28.50296	-0.939	8.473	0.026	-0.830		
14.03.2017	10	137.791	10.270	393.886	0.395	996.357	2.08	28.50	22.70	993.70	4535	11.4949	0.086	56052	142.5949	-1.014	11248	28.5104	-1.006	8.503	0.077	-0.899		
14.03.2017	10	141.501	10.311	403.801	0.405	996.352	2.08	28.52	22.70	993.70	4663	11.5056	0.180	57514	142.4317	-1.128	11539	28.4717	-1.140	8.520	0.171	-1.012		
14.03.2017	30	228.894	30.268	30.378	1.931	996.355	2.11	28.47	22.80	993.70	22228	11.5082	0.202	276072	143.4531	-0.419	55141	28.5083	-0.874	8.473	0.264	-0.303		
14.03.2017	30	228.168	30.258	30.369	1.925	996.370	2.10	28.46	23.60	993.50	22256	11.5111	0.227	275256	143.5290	-0.366	54983	28.5062	-0.812	8.456	-0.251	-0.251		
14.03.2017	30	230.767	30.241	30.351	1.938	996.485	2.10	28.46	23.60	993.50	22385	11.5057	0.181	278232	143.5306	-0.365	55573	28.50459	-0.819	8.459	0.242	-0.250		
14.03.2017	30	229.234	30.246	30.357	1.925	978.978	1.933	996.356	2.10	28.51	23.80	993.40	22241	11.5058	0.181	276469	143.5474	-0.353	55225	28.50693	-0.801	8.505	0.244	-0.237
14.03.2017	30	231.050	30.246	30.356	1.941	994.1187	1.948	996.363	2.10	28.48	24.00	993.30	22422	11.5087	0.206	278638	143.5400	-0.358	55657	28.5073	-0.808	8.481	0.268	-0.243
14.03.2017	60	119.022	59.335	59.553	1.969	996.341	2.00	28.56	24.00	993.30	22854	11.5058	0.181	282091	143.7982	-0.179	56000	28.4440	-1.243	8.558	0.233	-0.062		
14.03.2017	60	118.136	59.336	59.553	1.969	995.613	1.967	996.335	1.99	28.58	23.90	993.30	22638	11.5099	0.217	281968	143.8386	-0.151	55990	28.4444	-1.235	8.550	0.269	-0.034
14.03.2017	60	117.376	59.728	59.851	1.946	997.406	1.955	996.295	2.00	28.72	23.90	992.60	22897	11.5095	0.213	280118	143.8416	-0.149	55607	28.4486	-1.220	8.718	0.266	-0.030
14.03.2017	60	117.084	59.930	60.153	1.949	994.106	1.956	996.280	2.02	28.77	23.90	992.60	22520	11.5110	0.227	280350	143.8351	-0.153	55652	28.4463	-1.228	8.770	0.279	-0.034
14.03.2017	60	118.767	59.872	60.099	1.953	996.224	2.01	28.56	24.00	992.50	22826	11.5125	0.240	284077	143.8202	-0.164	56393	28.4434	-1.238	8.563	0.293	-0.041		
14.03.2017	100	71.046	100.112	100.497	1.975	975.711	1.983	996.168	2.06	29.15	24.50	992.10	22850	11.5211	0.315	284199	143.8465	-0.145	57194	28.8376	0.131	9.154	0.356	-0.020
14.03.2017	100	69.718	100.020	100.409	1.945	995.123	2.05	29.31	24.50	992.10	22298	11.5185	0.292	278618	143.8410	-0.149	56557	28.8281	0.098	9.308	0.333	-0.021		
14.03.2017	100	72.109	99.845	100.238	1.977	999.326	2.008	996.077	2.05	29.46	24.60	992.10	23129	11.5196	0.301	143.8268	-0.159	57880	28.8275	0.096	9.462	0.343	-0.029	
14.03.2017	100	71.751	99.967	100.367	1.992	992.322	2.000	996.014	2.05	29.58	24.20	992.10	23043	11.5192	0.298	286566	-0.158	57667	28.8278	0.097	9.567	0.341	-0.024	
14.03.2017	100	69.990	100.234	100.639	1.948	994.694	1.957	995.974	2.06	29.31	24.20	992.10	22548	11.5242	0.342	280300	143.8399	-0.150	56432	28.8423	0.147	9.809	0.366	-0.014
14.03.2017	130	55.043	129.734	129.703	130.336	1983.116	1.991	995.905	2.01	30.04	24.20	992.10	22948	11.5243	0.342	285317	143.8731	-0.127	57398	28.8246	0.096	10.039	0.383	0.013
14.03.2017	130	55.056	129.090	129.637	129.637	1974.210	1.983	995.783	2.06	30.44	24.00	992.00	22854	11.5275	0.370	283998	143.8540	-0.140	57164	28.8333	0.116	10.443	0.412	0.006
14.03.2017	130	54.796	129.226	129.792	129.792	1964.805	1.973	995.642	2.06	30.31	24.00	992.00	22755	11.5308	0.399	56959	143.8664	-0.134	56939	28.8311	0.178	10.905	0.443	0.020
14.03.2017	130	53.723	130.141	130.715	130.921	1942.090	1.951	995.603	2.08	31.03	23.70	992.00	22490	11.5294	0.386	279369	143.8496	-0.143	56211	28.8163	0.057	11.033	0.430	0.012
14.03.2017	130	54.280	129.987	130.565	130.565	1959.902	1.969	995.572	2.07	31.13	23.70	992.00	22699	11.5304	0.395	281923	143.8455	-0.146	56736	28.8202	0.070	11.131	0.440	0.011

INACAL Laboratory – Day#3

Data report INACAL: Day#3													Temperature correction of meter error								
													Corrected meter error								
													Coriolis Mass								
													$K_{m,nom}$	144.0560	Pulses/kg	$K_{V,nom}$	28.8000	Pulses/Liter			
Date	Nominal flowrate	Measurement time	Standard mass flowrate	Standard volume flowrate	Laboratory reference	Fluid	Ambient conditions	Water density	Water pressure	Air temp.	Air pressure	K-factor	Meter error	Pulse count	K-factor	Meter error	Pulse count	K-factor	Corrected meter error		
16.03.2017	10	133.411	10.294	10.329	381.468	0.83	996.616	2.04	27.59	24.60	99.40	4390	11.4692	-0.137	56931	144.1563	0.070	11031	28.8194	0.067	7.588
16.03.2017	10	129.440	10.186	10.221	366.248	0.867	996.617	2.05	27.58	24.70	99.40	4216	11.4724	-0.110	52800	144.1644	0.075	10593	28.8251	0.087	7.584
16.03.2017	10	134.707	10.207	10.242	381.949	0.883	996.617	2.05	27.58	24.90	99.40	4396	11.4704	-0.127	55069	144.1788	0.085	11047	28.8248	0.086	7.584
16.03.2017	10	125.138	10.258	10.292	356.557	0.358	996.617	2.05	27.58	24.90	99.40	4104	11.4711	-0.121	51413	144.1928	0.095	10314	28.8288	0.100	7.582
16.03.2017	10	119.761	10.257	10.292	341.214	0.342	996.615	2.05	27.59	25.10	99.30	3928	11.4729	-0.106	49192	144.1674	0.077	98688	28.8223	0.078	7.591
16.03.2017	10	118.457	10.249	10.283	337.231	0.338	996.615	2.05	27.59	25.10	99.30	3883	11.4754	-0.084	48605	144.1295	0.051	97483	28.8081	0.028	7.589
16.03.2017	10	113.721	10.256	10.291	323.982	0.325	996.613	2.05	27.60	25.10	99.30	3730	11.4740	-0.096	46717	144.1962	0.097	9372	28.8296	0.103	7.597
16.03.2017	10	126.534	10.174	10.208	357.594	0.359	996.614	2.05	27.59	25.20	99.30	4117	11.4741	-0.095	51545	144.1439	0.061	10341	28.8204	0.071	7.593
16.03.2017	10	115.743	10.195	10.230	327.776	0.329	996.615	2.05	27.59	25.20	99.30	3773	11.4719	-0.114	47236	144.1104	0.038	9476	28.8121	0.042	7.592
16.03.2017	10	126.548	10.249	10.284	360.285	0.362	996.611	2.05	27.60	25.30	99.30	4147	11.4713	-0.119	51944	144.1748	0.083	10421	28.8263	0.091	7.604
16.03.2017	60	112.450	59.412	59.614	1855.791	1.862	996.602	2.01	27.64	25.30	99.30	21458	11.5234	0.335	267415	144.0976	0.029	53067	28.4982	-1.048	7.636
16.03.2017	60	117.018	59.405	59.609	1930.964	1.1398	996.579	2.00	27.72	25.40	99.30	22350	11.5246	0.345	278250	144.0990	0.030	55207	28.5029	-1.032	7.721
16.03.2017	60	118.320	59.393	59.599	1952.057	1.059	996.552	2.01	27.81	25.50	99.30	22575	11.5249	0.347	281246	144.0768	0.014	55810	28.4918	-1.070	7.815
16.03.2017	60	117.762	59.329	59.537	1940.761	1.1348	996.531	2.00	27.93	25.70	99.30	22449	11.5269	0.365	279738	144.1383	0.057	55500	28.4975	-1.050	7.527
16.03.2017	60	112.842	59.419	59.628	1862.489	1.869	996.487	2.02	28.05	25.70	99.30	21540	11.5245	0.344	268243	144.0777	0.015	53264	28.4978	-1.049	8.046
16.03.2017	60	115.957	60.295	1935.163	1.1942	996.422	2.03	28.27	25.90	99.30	22400	11.5238	0.425	278865	144.1042	0.033	55536	28.5030	-1.031	8.275	
16.03.2017	60	116.281	60.128	60.347	1942.160	1.949	996.374	2.03	28.44	26.00	99.20	22481	11.5333	0.420	279834	144.0839	0.019	55554	28.5005	-1.040	8.441
16.03.2017	60	117.239	60.101	60.321	1957.255	1.1964	996.340	2.03	28.56	26.00	99.20	22652	11.5310	0.400	282012	144.0835	0.020	55982	28.4976	-1.050	8.561
16.03.2017	60	116.213	59.993	60.216	1936.663	1.944	996.296	2.02	28.71	26.00	99.20	22415	11.5312	0.402	279064	144.0953	0.027	55406	28.5031	-1.031	8.714
16.03.2017	60	116.838	59.971	60.196	1946.359	1.954	996.262	2.01	28.83	26.10	99.20	22529	11.5317	0.406	280470	144.0988	0.030	55679	28.4998	-1.042	8.000
16.03.2017	130	54.365	129.331	129.826	1960.251	1.1568	996.187	1.99	29.09	26.20	99.20	22703	11.5375	0.457	282299	144.0627	0.005	56833	28.8822	0.285	9.089
16.03.2017	130	53.996	128.808	129.321	1931.961	1.940	996.028	1.99	29.63	26.10	99.20	23374	11.5350	0.435	278263	143.9796	-0.053	55990	28.8658	0.229	9.627
16.03.2017	130	53.672	129.404	129.597	1929.262	1.1337	995.975	2.03	29.81	26.10	99.20	22341	11.5335	0.422	27789	143.9872	-0.048	55911	28.8639	0.222	9.462
16.03.2017	130	54.831	129.142	129.672	1966.949	1.975	995.909	2.03	30.03	26.10	99.20	22783	11.5355	0.440	283172	143.9651	-0.063	56979	28.8497	0.173	10.027
16.03.2017	130	54.177	128.643	129.182	1935.960	1.944	995.829	2.02	30.29	26.00	99.20	22439	11.5423	0.499	278722	143.9710	-0.059	56100	28.8570	0.198	10.291
16.03.2017	130	54.093	128.863	129.413	1936.260	1.945	995.750	2.02	30.55	26.10	99.20	22441	11.5406	0.484	278747	143.9616	-0.066	56106	28.8533	0.185	10.552
16.03.2017	130	54.003	129.083	129.646	1936.360	1.945	995.654	2.03	30.87	26.30	99.20	22443	11.5399	0.478	278786	143.9743	-0.057	56138	28.8655	0.227	10.866
16.03.2017	130	54.510	129.308	129.880	1957.952	1.967	995.596	2.04	31.05	26.30	99.20	22693	11.5391	0.471	281857	143.9550	-0.070	56775	28.8694	0.241	11.054
16.03.2017	130	53.547	129.765	130.341	1930.162	1.939	995.577	2.05	31.12	26.30	99.20	22376	11.5415	0.492	277826	143.9382	-0.081	55928	28.8476	0.165	11.116
16.03.2017	130	54.266	129.869	130.449	1957.662	1.966	995.556	2.03	31.18	26.30	99.20	22706	11.5470	0.540	281774	143.9347	-0.084	56716	28.8427	0.148	11.182

IBMETRO Laboratory – Day#1

Data report IBMETRO: Day#1																	
*Original data set																	
Turbine meter							Coriolis_Mass										
K _{V,non}							K _{m,non}	144.0560	Pulses/kg	K _{V,non}	28.8000	Pulses/Liter					
Temperature correction of meter error																	
T _{nom}							T _{nom}	20	°C								
Laboratory reference																	
Fluid							Ambient conditions										
Date	Nominal flowrate	Standard mass flowrate	Mass	Volume	Water density	Line pressure	Air temp.	Air pressure	Pulse count	K-factor	Meter error	Pulse count	K-factor				
	V _{nom}	t	m _{ref}	V _{ref}	m _{ref}	p _{fluid}	T _{fluid}	p _{air}	N	K _V	e _V	N	K _V				
	[m ³ /h]	[s]	[t/h]	[m ³]	[kg]	[kg/m ³]	[°C]	[bar]	[Pulses]	[Pulses/Liter]	[%]	[Pulses]	[Pulses/kg]	[%]			
01.03.2018	301.094	10.009	10.034	837.120	0.839	997.500	2.23	18.10	0.89	9425	-11.2307	-2.214	120455	143.8921	-0.114		
01.03.2018	30	300.871	10.014	10.039	836.310	0.839	997.500	2.21	16.80	0.89	9409	11.2144	-2.356	120456	143.9175	-0.096	
01.03.2018	30	301.337	10.008	837.777	0.840	997.700	2.23	16.90	18.00	0.89	9424	11.2236	-2.276	120589	143.9479	-0.075	
01.03.2018	30	300.454	10.014	10.034	835.742	0.837	998.000	2.23	16.90	18.00	0.89	9398	11.2226	-2.285	120291	143.9331	-0.085
01.03.2018	30	301.162	10.017	10.035	838.008	0.840	998.200	2.23	17.00	18.00	0.89	9414	11.2156	-2.353	120558	143.8626	-0.134
01.03.2018	30	299.817	29.902	29.956	2490.292	2.495	998.200	2.04	16.90	18.10	0.89	28376	11.1741	-0.965	358507	143.9618	-0.065
01.03.2018	30	300.843	29.903	29.954	2498.891	2.503	998.300	2.04	17.10	18.10	0.89	28467	11.3775	-0.980	359744	143.9535	-0.071
01.03.2018	30	301.602	29.890	29.955	2504.147	2.508	998.500	2.04	17.20	18.10	0.89	28533	11.3772	-0.939	360431	143.9336	-0.085
01.03.2018	30	301.830	29.916	29.946	2508.222	2.511	999.000	2.05	17.20	18.10	0.89	28522	11.3600	-1.088	360799	143.8425	-0.148
01.03.2018	30	300.953	29.923	29.950	2501.507	2.504	999.100	2.06	17.30	18.10	0.89	28459	11.3805	-0.893	358845	143.8433	-0.148
01.03.2018	60	301.088	59.728	59.782	4995.416	5.000	999.100	2.06	17.60	18.30	0.89	56991	11.3984	-0.754	718343	143.8004	-0.177
01.03.2018	60	301.136	59.569	59.638	4992.846	4.988	999.000	2.03	17.90	18.40	0.89	57117	11.4513	-0.294	716572	143.8078	-0.172
01.03.2018	60	301.185	59.520	59.587	4979.552	4.986	998.700	2.01	18.10	18.40	0.89	57099	11.4528	-0.289	716357	143.8597	-0.136
01.03.2018	60	301.161	59.483	59.567	4976.108	4.983	998.600	2.00	18.20	18.50	0.89	57051	11.4469	-0.314	715757	143.8468	-0.145
01.03.2018	60	301.642	59.425	59.521	4979.234	4.987	998.400	1.99	18.30	18.50	0.89	57124	11.4541	-0.269	716505	143.8986	-0.109
01.03.2018	100	301.361	97.148	97.313	8132.361	8.146	998.300	0.28	18.80	18.20	0.89	93355	11.1599	-0.218	116970	143.8332	-0.153
01.03.2018	100	301.093	96.482	96.636	8069.470	8.084	998.200	0.28	18.90	18.20	0.89	92669	11.4632	-0.190	1160540	143.8186	-0.165
01.03.2018	100	301.318	96.143	96.326	8047.091	8.062	998.100	0.27	19.00	18.10	0.89	92424	11.4636	-0.187	1157520	143.8433	-0.148
01.03.2018	100	301.492	96.290	96.483	8062.446	8.079	998.000	0.27	19.10	18.00	0.89	92650	11.4635	-0.186	1159710	143.8410	-0.149
02.03.2018	100	301.847	96.145	96.337	8061.365	8.078	998.000	0.27	19.30	18.00	0.89	92606	11.4647	-0.177	1159610	143.8478	-0.144

IBMETRO Laboratory – Day#2

Data report IBMETRO- Day#2											
*Original data set											
Date	Nominal flowrate	Measurement time	Laboratory reference	Fluid	Ambient conditions	Turbine meter	Coriolis Mass	Coriolis Vol	Corrected meter error		
	Standard mass flowrate	Standard volume flowrate		Water density	Water pressure	Air temp.	Air pressure	K-factor	Meter error	Turbine meter	Coriolis Mass
	m^* ref	V^* ref		ρ_{fluid}	ρ_{fluid}	T_{air}	p_{air}	N	κ_V	ϵ_V	κ_V
	[kg/h]	[m³/h]		[kg/m³]	[kg/m³]	[°C]	[bar]	[Pulses]	[Pulses]	[Pulses]	[Pulses]
02.03.2018	10	301.197	9.380	10.000	834.979	0.837	908.000	2.01	19.00	16.90	0.89
02.03.2018	10	301.007	9.390	9.390	833.556	0.835	908.000	1.99	19.00	17.00	0.89
02.03.2018	10	300.871	9.366	9.384	832.946	0.834	908.200	2.01	19.10	17.00	0.89
02.03.2018	10	301.032	9.362	9.380	833.027	0.835	908.200	2.00	19.20	17.00	0.89
02.03.2018	30	301.323	29.839	29.886	2497.573	2.502	908.100	2.01	19.00	17.20	0.89
02.03.2018	30	301.106	29.852	2492.104	2.497	908.100	2.01	19.10	17.20	0.89	287/09
02.03.2018	30	303.546	29.753	29.807	2508.762	2.513	908.200	2.01	19.20	17.20	0.89
02.03.2018	30	301.134	29.777	29.837	2094.949	2.500	908.000	2.01	19.20	17.30	0.89
02.03.2018	30	301.207	29.750	29.800	2489.105	2.493	908.300	1.99	19.30	17.30	0.89
02.03.2018	60	301.093	59.761	59.869	4996.229	5.007	908.200	1.97	19.50	17.50	0.89
02.03.2018	60	305.688	59.797	59.893	5070.580	5.079	908.400	1.93	19.80	17.70	0.89
02.03.2018	60	301.362	59.761	59.857	5002.675	5.011	908.400	1.90	19.90	17.70	0.89
02.03.2018	60	301.268	59.733	59.835	4998.796	5.007	908.300	1.86	20.00	17.80	0.89
02.03.2018	60	302.564	59.721	59.823	5019.278	5.028	908.300	1.90	20.10	17.90	0.89
02.03.2018	100	300.903	95.812	95.994	8005.691	8.021	908.100	0.26	20.60	18.50	0.89
02.03.2018	100	301.012	94.659	94.849	7914.889	7.931	908.000	0.26	20.80	18.80	0.88
02.03.2018	100	300.766	94.631	94.821	7006.057	7.922	908.000	0.26	20.90	18.90	0.88
02.03.2018	100	300.665	94.572	94.971	7931.785	7.947	908.100	0.26	21.00	19.10	0.88
02.03.2018	100	302.445	95.048	95.229	7985.202	8.000	908.100	0.27	21.10	19.20	0.88

IBMETRO Laboratory – Day#3

Data report IBMETRO: Day#3												*Original data set												
Laboratory reference												Turbine meter												
Date	Nominal flowrate	Standard conditions				Ambient conditions				Coriolis Mass				Coriolis Vol				Temperature correction of meter error				T _{nom}		T _{nom}
		Mass	Volume	Water density	Mass	Volume	Air pressure	Water temp.	Air temp.	Pulse count	K-factor	Meter error	Pulse count	K-factor	Meter error	Pulse count	K-factor	(T _{fluid} - T _{nom})	Turbine meter	Coriolis Mass	Coriolis Vol	20	°C	
		m _{ref}	V _{ref}	[m ³ /h]	m _{ref}	V _{ref}	p _{fluid}	T _{fluid}	T _{air}	N	K _V	e _V	N	K _m	e _m	N	K _V	e _V	ΔT _{fluid}	Corrected meter error	K _{m,nom}	28.8000	Pulses/liter	
		[kg]	[l/h]	[m ³ /h]	[kg]	[l/h]	[bar]	[°C]	[°C]	[Pulses]	[Pulses/Liter]	[%]	[Pulses]	[Pulses/Liter]	[%]	[Pulses]	[Pulses/Liter]	[%]	[°C]	[°C]	[%]	K _{m,nom}	28.8000	Pulses/liter
05.03.2018	10	300.658	10.018	10.040	836.645	0.838	99.800	2.04	19.00	16.80	0.89	9507	11.332	-1.278	119.789	143.1779	-0.610	239.91	28.6122	-0.052	-1.000	-1.292	-0.618	
05.03.2018	10	301.036	10.010	10.032	887.023	0.839	99.800	2.05	19.00	16.70	0.89	9507	11.331	-1.322	119.889	143.3520	-0.489	240.82	28.6481	-0.527	-1.000	-1.337	-0.497	
05.03.2018	10	299.869	9.994	10.015	832.437	0.834	99.790	2.05	19.10	16.70	0.89	9462	11.3428	-1.239	119.449	143.4932	-0.361	239.24	28.6794	-0.419	-0.900	-1.253	-0.398	
05.03.2018	10	299.809	9.990	10.012	831.933	0.834	99.780	2.05	19.20	16.70	0.89	9456	11.3413	-1.251	119.447	143.5777	-0.332	239.23	28.6927	-0.373	-0.800	-1.267	-0.338	
05.03.2018	10	299.990	10.005	10.027	833.706	0.836	99.780	2.06	19.20	16.70	0.89	9471	11.3351	-1.305	119.780	143.6718	-0.267	239.86	28.7070	-0.323	-0.800	-1.321	-0.273	
05.03.2018	10	301.555	9.994	10.015	887.156	0.839	99.790	2.05	19.50	16.70	0.89	9553	11.3873	-0.851	120.044	144.1189	-0.044	241.60	28.7990	-0.003	-0.500	-0.869	0.041	
05.03.2018	10	301.225	10.002	10.024	836.889	0.839	99.800	2.06	19.60	16.80	0.89	9523	11.3599	-1.090	120.084	143.9650	-0.063	241.26	28.7645	-0.123	-0.400	-1.108	-0.065	
05.03.2018	10	301.173	10.006	10.026	837.066	0.839	99.800	2.04	19.60	16.80	0.89	9542	11.3765	-0.944	120.428	143.8692	-0.130	241.18	28.7549	-0.157	-0.400	-0.963	-0.131	
05.03.2018	10	300.718	10.006	10.026	885.840	0.838	99.800	2.04	19.70	16.80	0.89	9530	11.3789	-0.924	120.245	143.8613	-0.135	240.84	28.7565	-0.151	-0.300	-0.943	-0.136	
05.03.2018	10	301.370	9.995	10.015	836.717	0.838	99.800	2.05	19.70	16.90	0.89	9549	11.3896	-0.830	120.892	144.0056	-0.035	241.30	28.7812	-0.065	-0.300	-0.850	-0.036	
05.03.2018	60	301.337	59.863	59.983	5610.824	5.021	999.000	1.94	19.70	17.00	0.88	57551	11.4624	-0.197	720.984	143.8853	-0.118	142.851	28.4515	-1.210	-0.300	-0.202	-0.119	
05.03.2018	60	300.832	59.859	59.979	5021.106	5.012	998.000	1.99	19.80	17.10	0.88	57422	11.4586	-0.230	719.734	143.8362	-0.118	142.8516	28.4542	-1.201	-0.200	-0.234	-0.117	
05.03.2018	60	301.769	59.946	59.946	5014.419	5.025	997.900	1.95	19.90	17.20	0.88	57564	11.4556	-0.256	721.478	143.8489	-0.122	142.8524	28.4489	-1.219	-0.100	-0.259	-0.120	
05.03.2018	60	301.067	59.673	59.794	4890.411	5.001	991.980	1.94	19.90	17.20	0.88	57290	11.4568	-0.245	718.011	143.8781	-0.123	142.8539	28.4539	-1.202	-0.100	-0.248	-0.122	
05.03.2018	60	301.229	59.381	59.707	4985.451	4.956	997.900	1.92	20.00	17.90	0.88	57241	11.4575	-0.239	717.327	143.8841	-0.119	142.8535	28.4501	-1.215	0.000	-0.242	-0.117	
05.03.2018	60	302.543	59.583	59.697	5007.372	5.017	998.100	1.92	20.10	17.40	0.89	57499	11.4591	-0.226	720.445	143.8769	-0.124	142.758	28.4554	-1.197	0.100	-0.227	-0.120	
05.03.2018	60	301.094	59.574	59.887	4982.655	4.992	998.100	1.93	20.20	17.40	0.88	57222	11.4625	-0.196	716.853	143.8703	-0.129	142.046	28.4540	-1.201	0.200	-0.197	-0.124	
05.03.2018	60	301.504	59.559	59.684	4988.137	4.999	997.900	1.93	20.20	17.40	0.88	57292	11.4613	-0.206	717.790	143.8994	-0.109	142.2226	28.4530	-1.205	0.200	-0.207	-0.104	
05.03.2018	60	301.283	59.328	59.547	4981.865	4.992	995.000	1.93	20.30	17.50	0.88	57222	11.4631	-0.191	716.846	143.8911	-0.114	142.044	28.4552	-1.197	0.300	-0.191	-0.108	
05.03.2018	60	300.933	59.305	59.630	4974.145	4.985	997.900	1.92	20.40	17.60	0.88	57124	11.4601	-0.217	715.623	143.8685	-0.130	141.789	28.4453	-1.231	0.000	-0.285	0.011	
05.03.2018	100	302.065	96.449	96.449	811.905	8.133	998.100	0.28	20.70	17.90	0.88	93135	11.4521	-0.286	1167620	143.8327	-0.155	234.216	28.7998	-0.001	0.700	-0.285	0.011	
05.03.2018	100	301.072	96.788	95.989	8010.815	8.028	999.000	0.26	20.90	18.20	0.88	91926	11.4511	-0.295	1152400	143.8855	-0.139	231.44	28.7934	-0.023	0.900	-0.293	0.013	
05.03.2018	100	302.564	94.791	94.991	7966.781	7.984	997.900	0.25	20.90	18.40	0.88	91387	11.4469	-0.332	1145910	143.8350	-0.153	229.660	28.7917	-0.029	0.900	-0.330	0.013	
05.03.2018	100	300.431	94.828	95.028	4981.375	7.930	997.900	0.26	21.00	18.40	0.88	90791	11.4486	-0.317	1138390	143.8510	-0.142	228.221	28.7909	-0.032	1.000	-0.315	0.014	
05.03.2018	100	301.541	95.327	95.528	7984.743	8.002	997.900	0.24	21.10	18.60	0.88	91609	11.4489	-0.314	1148370	143.8205	-0.163	230.340	28.7869	-0.045	1.100	-0.311	0.016	
05.03.2018	100	301.343	95.323	95.514	7979.115	7.955	998.000	0.28	21.20	18.70	0.88	91545	11.4501	-0.304	1147720	143.8405	-0.150	230.18	28.7949	-0.018	1.200	-0.300	0.017	
05.03.2018	100	300.707	95.374	95.566	7968.180	7.984	998.000	0.26	21.30	18.70	0.88	91390	11.4464	-0.336	1145880	143.8007	-0.177	229.836	28.7865	-0.047	1.300	-0.332	0.018	
05.03.2018	100	300.910	95.212	95.403	7958.447	7.974	998.000	0.26	21.40	18.80	0.88	91285	11.4473	-0.329	114470	143.8057	-0.174	229.875	28.8266	0.069	1.400	-0.334	0.019	
05.03.2018	100	301.115	95.198	95.391	7962.673	7.979	997.900	0.26	21.50	18.90	0.88	91340	11.4479	-0.323	1145630	143.7997	-0.178	229.701	28.7889	-0.038	1.500	-0.338	0.020	
05.03.2018	100	301.189	95.286	95.479	7971.986	7.988	997.900	0.27	21.60	19.00	0.88	91453	11.4486	-0.317	1146410	143.8048	-0.174	229.666	28.7885	-0.040	1.600	-0.311	0.022	

INTI Laboratory – Day#1

Data report INTI: Day#1														*Original data set																	
Turbine meter																Coriolis_Mass															
																$K_{V,nom}$	11.4850 Pulses/liter														
Date	Nominal flowrate	Measurement time	Standard mass flowrate	Fluid	Ambient conditions	Water density	Line pressure	Air temp.	Pulse count	K-factor	Meter error	Pulse count	K-factor	Meter error	e_V	K_V	e_m	K_m	e_m	$K_{V,nom}$	$K_{m,nom}$	e_V	ΔT_{fluid} - $(T_{fluid} - T_{nom})$	Turbine meter	Coriolis Mass	$e_{cor,V}$	$e_{cor,m}$	Corrected meter error			
V^* , nom	t	m^* , ref	V^* , ref	m^* , ref	ρ_{fluid}	V_{ref}	ρ_{fluid}	T_{air}	ρ_{air}	N	e_V	N	e_m	e_V	[Pulses/Liter]	[kg/m³]	[bar]	[°C]	[bar]	[Pulses]	[kg]	[Pulses]	[kg]	[%]	[%]	[%]	[%]	[%]	[%]		
06.12.2018	10	343.780	10.481	10.502	1000.888	1.003	986.024	21.40		11.4452	-0.347	144032	143.9042	-0.105	28.776	28.6936	-0.369	14.400	-0.375	-0.086											
06.12.2018	10	344.540	10.465	10.487	1001.603	1.004	997.979	21.60		11.4116	-0.639	144061	143.8304	-0.157	28.781	28.6769	-0.428	16.600	-0.668	-0.135											
06.12.2018	10	344.770	10.451	10.472	1000.904	1.003	993.979	21.60		11.4195	-0.570	143878	143.7480	-0.214	28.746	28.6620	-0.479	16.600	-0.599	-0.192											
06.12.2018	10	344.930	10.442	10.463	1000.505	1.003	997.979	21.60		11.484	-0.261	143985	143.8923	-0.114	28.764	28.6914	-0.377	16.600	-0.290	-0.092											
06.12.2018	10	345.160	10.437	10.458	1000.655	1.003	997.979	21.60		11.489	-0.233	143974	143.8798	-0.122	28.765	28.6881	-0.389	16.600	-0.261	-0.101											
06.12.2018	30	126.960	28.463	28.211	1003.799	1.006	993.979	21.60		11.6112	-11.547	144460	143.9133	-0.099	28.756	28.5893	-0.732	16.600	0.518	-0.078											
06.12.2018	30	123.900	29.211	29.270	1005.346	1.007	997.979	21.60		11.6113	-11.5279	144650	143.8609	-0.135	28.790	28.5790	-0.767	16.600	0.372	-0.114											
06.12.2018	30	124.330	29.041	29.099	1002.950	1.005	997.979	21.60		11.593	-11.5355	144339	143.9144	-0.098	28.723	28.5806	-0.762	16.600	0.438	-0.077											
06.12.2018	30	119.440	30.270	1001.705	1.003	997.512	22.60		11.593	-0.510	144250	143.9930	-0.044	28.745	28.6224	-0.617	16.600	0.523	0.003												
06.12.2018	30	124.490	29.017	29.077	1003.414	1.005	997.934	21.80		11.603	-11.5396	0.476	144391	143.8897	-0.108	28.746	28.5890	-0.733	18.800	0.475	-0.085										
06.12.2018	60	61.000	58.931	59.058	986.553	1.001	997.843	22.20		11.529	-11.5208	0.312	143741	143.9493	-0.074	28.572	28.5517	-0.862	2.200	0.325	-0.045										
06.12.2018	60	59.330	60.732	60.863	1000.898	1.003	997.843	22.20		11.552	-11.5167	0.276	144048	143.9188	-0.095	28.533	28.4459	-1.129	2.200	0.290	-0.066										
06.12.2018	60	59.340	60.897	61.025	1003.779	1.006	997.889	22.00		11.581	-11.5130	0.244	144616	144.0716	0.011	28.510	28.3427	-1.588	2.000	0.256	0.037										
06.12.2018	60	59.350	60.923	60.950	1007.705	1.004	997.512	22.00		11.514	-0.252	143568	143.9930	-0.044	28.440	28.4440	-1.236	2.000	0.264	-0.102											
06.12.2018	60	59.360	60.696	60.827	1002.934	1.005	997.843	22.20		11.581	-11.5256	0.318	144256	143.8652	-0.132	28.582	28.4352	-1.267	2.200	0.331	-0.104										
06.12.2018	100	184.580	98.414	98.638	5045.900	5.057	997.727	22.70		58342	-11.5360	0.444	72652	144.6030	0.380	146282	28.9244	0.432	2.700	0.455	0.415										
06.12.2018	100	182.550	99.536	99.763	5047.349	5.059	997.727	22.70		58375	-11.5393	0.472	729595	144.6231	0.394	146340	28.9277	0.443	2.700	0.484	0.429										
06.12.2018	100	184.360	98.524	98.748	5045.513	5.057	997.727	22.70		58342	-11.5369	0.452	72652	144.6061	0.382	146270	28.9242	0.431	2.700	0.463	0.417										
06.12.2018	100	183.230	99.160	99.386	5046.979	5.058	997.727	22.70		58365	-11.5381	0.462	729922	144.6255	0.395	146317	28.9251	0.434	2.700	0.473	0.430										
06.12.2018	100	184.380	98.529	98.753	5046.312	5.058	997.727	22.70		58349	-11.5364	0.448	72666	144.5939	0.373	146289	28.9234	0.428	2.700	0.459	0.408										
06.12.2018	130	142.260	128.199	128.494	5065.995	5.078	997.704	22.80		58505	-11.5221	0.323	731943	144.4816	0.295	146578	28.8673	0.234	2.800	0.334	0.332										
06.12.2018	130	141.790	128.616	128.912	5065.608	5.077	997.704	22.80		58449	-11.5118	0.233	731882	144.4789	0.294	146341	28.8224	0.078	2.800	0.245	0.330										
06.12.2018	130	142.500	127.946	128.240	5064.554	5.076	997.704	22.80		58484	-11.5213	0.316	731651	144.4662	0.285	146530	28.8663	0.230	2.800	0.327	0.321										
06.12.2018	130	142.440	128.002	128.297	5064.610	5.076	997.704	22.80		58488	-11.5219	0.321	731749	144.4828	0.296	146451	28.8501	0.174	2.800	0.332	0.333										
06.12.2018	130	140.760	129.833	129.535	5064.805	5.076	997.704	22.80		58485	-11.5208	0.312	731761	144.4796	0.294	146649	28.8380	0.306	2.800	0.323	0.330										

INTI Laboratory – Day#2

Data report INTI: Day#2												*Original data set																	
Date	Nominal flowrate	Laboratory reference						Fluid						Ambient conditions			Turbine meter			Coriolis_Mass			Coriolis_Vol			Temperature correction of meter error			
		Standard mass flowrate	Mass	Volume	Water density	Line pressure	Air temp.	T_{air}	P_{air}	κ_{v}	e_v	N	κ_m	e_m	N	κ_v	e_v	$K_{V,\text{nom}}$	144.0560 [Pulses/liter]	$K_{V,\text{nom}}$	28.8000 [Pulses/liter]	$K_{V,\text{nom}}$	28.8000 [Pulses/liter]	ΔT_{fluid}	T_{nom}	20 °C			
12.12.2018	10	367.640	9.794	9.817	1000.202	1.003	997.556	23.00	[bar]	[°C]	[bar]	[bar]	[bar]	[bar]	[bar]	[bar]	[bar]	[Pulses]	[Pulses/Liter]	[Pulses]	[Pulses]	[Pulses]	[Pulses/Liter]	[%]	[°C]	[%]			
12.12.2018	10	366.680	9.810	9.833	999.055	1.001	997.056	23.00										11.4647	-0.176	143.7939	-0.181	28767	28.6938	-0.369	3.000	-0.208	-0.142		
12.12.2018	10	368.130	9.784	9.808	1000.457	1.003	997.536	23.50										11.529	0.243	143.8089	-0.172	28735	28.6948	-0.365	3.000	0.211	-0.133		
12.12.2018	10	367.430	9.794	9.819	999.659	1.002	997.536	23.50										11.5033	0.159	143.8053	-0.174	28772	28.6880	-0.389	3.500	0.128	-0.129		
12.12.2018	10	367.600	9.788	9.822	1000.457	1.003	997.536	23.50										11.543	0.292	143.7901	-0.185	28750	28.6889	-0.386	3.500	0.260	-0.139		
12.12.2018	30	116.570	30.906	30.975	999.030	1.001	997.751	22.60										11.553	0.298	143.738	-0.266	28751	28.6671	-0.462	3.500	0.267	-0.221		
12.12.2018	30	116.280	30.786	30.855	994.390	0.997	997.751	22.60										11.564	0.159	143.8866	-0.118	28630	28.5933	-0.718	2.600	0.164	-0.084		
12.12.2018	30	117.920	30.501	30.570	999.080	1.001	997.751	22.60										11.565	0.1051	144.0652	0.006	28494	28.5903	-0.728	2.600	1.051	0.040		
12.12.2018	30	116.740	30.794	30.863	998.581	1.001	997.751	22.60										11.563	0.545	143.8194	-0.164	28619	28.5809	-0.761	2.600	0.550	-0.130		
12.12.2018	30	116.500	30.799	30.863	996.984	0.999	997.751	22.60										11.562	0.587	143.8462	-0.246	28608	28.5842	-0.749	2.600	0.592	-0.112		
12.12.2018	60	60.310	59.329	60.067	1003.982	1.006	997.704	22.80										11.560	0.150	143.8655	-0.120	28567	28.5869	-0.733	2.600	0.561	-0.056		
12.12.2018	60	60.100	60.010	60.148	1001.837	1.004	997.704	22.80										11.613	0.1046	143.257	0.006	28494	28.5944	-0.728	2.600	1.051	0.040		
12.12.2018	60	60.970	58.954	59.089	998.444	1.001	997.704	22.80										11.576	0.15674	143.6887	-0.164	28619	28.5809	-0.761	2.600	0.550	-0.130		
12.12.2018	60	60.290	59.388	60.126	1004.631	1.007	997.704	22.80										11.621	0.15049	143.6462	-0.146	28608	28.5842	-0.749	2.600	0.592	-0.112		
12.12.2018	60	60.260	59.631	59.771	998.157	1.001	997.556	23.00										11.565	0.556	143.8639	-0.120	28567	28.5869	-0.733	2.600	0.561	-0.056		
12.12.2018	100	183.890	98.765	99.019	5044.978	5.058	997.438	23.50										11.539	0.478	144.6330	0.401	28698	28.5185	-0.977	2.800	0.500	0.437		
12.12.2018	100	181.740	99.963	100.220	5046.204	5.059	997.438	23.50										11.584	0.4362	144.4646	0.446	28560	28.4422	-1.242	2.800	0.463	-0.082		
12.12.2018	100	183.710	98.849	99.098	5044.338	5.057	997.487	23.70										11.576	0.718	143.9159	-0.097	28469	28.4479	-1.223	2.800	0.755	-0.061		
12.12.2018	100	183.530	98.968	99.219	5045.424	5.058	997.463	23.80										11.621	0.486	144.6063	-0.083	28641	28.4435	-1.238	2.800	0.504	-0.047		
12.12.2018	100	183.360	99.045	99.302	5044.684	5.058	997.413	24.00										11.595	0.646	143.721	-0.048	28461	28.4467	-1.227	3.000	0.665	-0.009		
12.12.2018	130	142.300	128.113	128.445	5064.024	5.077	997.413	23.90										11.539	0.478	144.7958	0.413	144.6504	0.413	14536	28.9339	0.455	3.000	0.463	0.435
12.12.2018	130	143.210	127.250	127.580	5062.080	5.075	997.413	23.90										11.540	0.481	144.5402	0.424	144.6568	0.424	14538	28.9352	0.459	3.000	0.474	0.448
12.12.2018	130	143.510	127.019	127.349	5063.490	5.077	997.413	23.70										11.520	0.324	143.650	0.400	144.6325	0.400	14538	28.9315	0.457	3.700	0.481	0.448
12.12.2018	130	143.150	127.351	127.681	5063.970	5.077	997.413	23.80										11.592	0.466	143.727	0.399	144.6315	0.399	14530	28.9309	0.455	3.800	0.493	0.449
12.12.2018	130	142.280	128.129	128.461	5063.924	5.077	997.413	24.00										11.534	0.447	143.7632	0.401	144.6338	0.401	14530	28.9398	0.451	4.000	0.465	0.453
12.12.2018	130	142.300	128.113	128.445	5064.024	5.077	997.413	23.90										11.524	0.341	144.4965	0.306	144.4965	0.306	14538	28.8268	0.093	3.300	0.357	0.356
12.12.2018	130	143.210	127.250	127.580	5062.080	5.075	997.413	23.90										11.524	0.340	143.423	0.342	144.4960	0.342	14538	28.8319	0.111	3.300	0.356	0.352
12.12.2018	130	143.510	127.019	127.349	5063.490	5.077	997.413	23.70										11.524	0.324	143.650	0.302	144.4913	0.302	14530	28.8501	0.174	3.700	0.340	0.350
12.12.2018	130	143.150	127.351	127.681	5063.970	5.077	997.413	23.80										11.592	0.297	143.587	0.287	144.4921	0.287	14530	28.8539	0.187	3.800	0.333	0.336
12.12.2018	130	142.280	128.129	128.461	5063.924	5.077	997.413	24.00										11.526	0.326	731609	0.291	144.4747	0.291	14530	28.8724	0.252	4.000	0.342	0.342

INTI Laboratory – Day#3

Data report INTI: Dev#3												Temperature correction of meter error													
Original data set												Turbine meter													
Date	Nominal flowrate	Measurement time	Laboratory/reference	Fluid	Ambient conditions	Coriolis_Mass				Coriolis_Vol				Turbine meter				Coriolis_Mass				Turbine meter			
V _{nom}	m _{ref}	t	Standard mass flowrate	Mass	Water density	Pulse count	K-factor	Meter error	Pulse count	Pulse count	K-factor	Meter error	Pulse count	T _{fluid} - T _{nom}	T _{nom}	e _{cor,v}	Pulses/Liter	K _{V,nom}	Pulses/kg	K _{V,nom}	Pulses/kg	K _{V,nom}	Pulses/Liter	T _{nom}	20 °C
V _{nom}	m _{ref}	t	V _{ref}	m _{ref}	ρ _{fluid}	N	ε _m	ε _v	N	[Pulses]	[Pulses]	N	Δ T _{fluid}	T _{nom}	e _{cor,v}	%	[Pulses]	[Pulses]	[Pulses]	[Pulses]	[Pulses]	[Pulses]	T _{nom}	20 °C	
14.12.2018	10	347.430	10.360	10.385	990.815	1.002	1.002	0.292	11544	11.5195	11.5195	143.8456	-0.146	287654	28.7005	-0.345	3.200	0.261	3.200	28.7005	28.7005	0.261	-0.105		
14.12.2018	10	348.840	10.316	10.341	999.627	1.002	997.560	0.149	11526	11.5022	11.5022	144.1654	0.112	288337	28.7774	-0.079	3.400	0.118	3.400	0.118	0.118	0.118	0.156		
14.12.2018	10	350.950	10.284	10.309	1002.521	1.005	997.560	0.328	11580	11.5227	11.5227	143.9883	-0.302	288000	28.6575	-0.495	3.400	0.297	3.400	0.297	0.297	0.297	-0.258		
14.12.2018	10	348.990	10.335	10.361	1001.923	1.004	997.560	0.249	11564	11.5137	11.5137	140.0205	0.220	28805	28.6795	-0.418	3.400	0.218	3.400	0.218	0.218	0.218	-0.176		
14.12.2018	10	347.530	10.359	10.384	1000.026	1.002	997.560	0.266	11544	11.5155	11.5155	143.720	-0.236	28745	28.6741	-0.437	3.400	0.234	3.400	0.234	0.234	0.234	-0.192		
14.12.2018	10	347.480	10.357	10.383	999.727	1.002	997.560	0.270	11541	11.5160	11.5160	143.734	-0.196	28748	28.6857	-0.397	3.400	0.238	3.400	0.238	0.238	0.238	-0.152		
14.12.2018	10	347.690	10.355	10.380	1000.076	1.003	997.560	0.278	11546	11.5170	11.5170	143.673	-0.273	28737	28.6647	-0.470	3.400	0.247	3.400	0.247	0.247	0.247	-0.229		
14.12.2018	10	349.100	10.345	10.370	1003.170	1.006	997.560	0.229	11576	11.5113	11.5113	144.181	0.229	28837	28.6758	-0.431	3.400	0.197	3.400	0.197	0.197	0.197	-0.185		
14.12.2018	10	347.500	10.358	10.384	999.877	1.002	997.560	0.263	11542	11.5153	11.5153	143.799	-0.166	28765	28.6884	-0.353	3.400	0.232	3.400	0.232	0.232	0.232	-0.122		
14.12.2018	10	347.440	10.361	10.387	999.976	1.002	997.560	0.253	11542	11.5141	11.5141	143.6567	0.247	28899	28.8292	0.101	3.400	0.222	3.400	0.222	0.222	0.222	-0.203		
14.12.2018	60	59.950	60.303	60.455	1004.209	1.007	997.487	0.412	11610	11.5323	11.5323	143.8844	-0.119	28634	28.4423	-1.242	3.700	0.435	3.700	0.435	0.435	0.435	-0.071		
14.12.2018	60	59.780	60.096	60.270	997.924	1.000	997.487	0.444	11541	11.5359	11.5359	143.9308	-0.087	28456	28.4435	-1.238	3.700	0.467	3.700	0.467	0.467	0.467	-0.039		
14.12.2018	60	59.330	60.990	61.144	1005.157	1.008	997.487	0.516	11633	11.5442	11.5442	144.6532	0.115	28675	28.4562	-1.194	3.700	0.539	3.700	0.539	0.539	0.539	-0.067		
14.12.2018	60	59.330	60.530	60.683	991.575	1.000	997.487	0.540	11548	11.5470	11.5470	143.9210	-0.094	28869	28.8665	0.231	3.700	0.563	3.700	0.563	0.563	0.563	-0.046		
14.12.2018	60	58.910	60.904	61.057	996.627	0.999	997.487	0.531	11536	11.5460	11.5460	143.8241	-0.161	28800	28.8248	0.086	3.700	0.554	3.700	0.554	0.554	0.554	-0.113		
14.12.2018	60	59.910	60.027	60.184	993.942	1.002	997.388	0.531	11564	11.5460	11.5460	143.9002	-0.108	28483	28.4387	-1.255	4.100	0.557	4.100	0.557	0.557	0.557	-0.055		
14.12.2018	60	58.840	61.136	61.297	999.242	1.002	997.388	0.353	11547	11.5256	11.5256	143.7975	0.119	28444	28.3912	-1.419	4.100	0.379	4.100	0.379	0.379	0.379	-0.066		
14.12.2018	60	59.950	60.994	61.153	999.072	1.002	997.383	0.550	11568	11.5482	11.5482	143.8835	-0.120	28335	28.2865	-1.783	4.200	0.577	4.200	0.577	0.577	0.577	-0.065		
14.12.2018	60	59.170	60.990	61.153	1002.444	1.005	997.383	0.559	11606	11.5469	11.5469	144.1177	0.160	28435	28.2892	-1.774	4.300	0.566	4.300	0.566	0.566	0.566	-0.104		
14.12.2018	60	59.280	60.849	61.013	1001.975	1.005	997.313	0.595	11590	11.5361	11.5361	144.191	-0.104	28438	28.3057	-1.716	4.400	0.473	4.400	0.473	0.473	0.473	-0.046		
14.12.2018	130	141.010	129.245	129.603	5062.454	5.076	997.237	0.329	58495	11.5227	11.5227	143.404	0.292	146326	28.8243	0.084	4.700	0.348	4.700	0.348	0.348	0.348	-0.033		
14.12.2018	130	142.550	127.859	128.213	5062.846	5.077	997.237	0.372	58525	11.5278	11.5278	144.7456	0.291	146313	28.8195	0.068	4.700	0.392	4.700	0.392	0.392	0.392	-0.032		
14.12.2018	130	142.170	128.465	128.520	5061.430	5.075	997.237	0.322	58495	11.5231	11.5231	144.4528	0.275	146410	28.8467	0.162	4.700	0.351	4.700	0.351	0.351	0.351	-0.037		
14.12.2018	130	143.170	127.276	127.628	5061.683	5.076	997.237	0.322	58482	11.5219	11.5219	144.4302	0.260	146324	28.8283	0.098	4.700	0.341	4.700	0.341	0.341	0.341	-0.046		
14.12.2018	130	143.240	127.246	127.589	5062.583	5.077	997.237	0.321	58492	11.5219	11.5219	144.4539	0.276	145843	28.7284	-0.248	4.700	0.341	4.700	0.341	0.341	0.341	-0.037		
14.12.2018	130	142.460	127.937	128.291	5062.741	5.077	997.237	0.321	58494	11.5219	11.5219	144.4401	0.267	143218	28.2105	-2.047	4.700	0.341	4.700	0.341	0.341	0.341	-0.038		
14.12.2018	130	143.210	127.278	127.630	5063.179	5.077	997.237	0.326	58502	11.5225	11.5225	144.4488	0.273	142900	28.1454	-2.273	4.700	0.346	4.700	0.346	0.346	0.346	-0.037		
14.12.2018	130	143.450	127.048	127.400	5062.494	5.077	997.237	0.319	58490	11.5217	11.5217	144.4107	0.246	146431	28.8448	0.155	4.700	0.339	4.700	0.339	0.339	0.339	-0.037		
14.12.2018	130	143.450	127.018	127.369	5061.298	5.075	997.237	0.328	58481	11.5226	11.5226	144.4481	0.272	145830	28.7529	-0.164	4.700	0.347	4.700	0.347	0.347	0.347	-0.033		
14.12.2018	130	143.380	127.115	127.467	5062.689	5.077	997.237	0.333	58500	11.5232	11.5232	144.4264	0.257	146307	28.8192	0.067	4.700	0.352	4.700	0.352	0.352	0.352	-0.038		

CENAM Laboratory – Day#1

Data report CENAM: Day#1											
Original data set											
Date	Nominal mass flowrate	Standard volume flowrate	Fluid	Ambient conditions	Turbine meter	Coriolis Mass	Coriolis Vol	Coriolis Vol	Coriolis Mass	Coriolis Mass	Temperature correction of meter error
V_{nom}	t	m_{ref}	ρ_{fluid}	T_{air}	$K_{v,corr}$	$K_{m,corr}$	$K_{v,corr}$	$K_{m,corr}$	$K_{v,corr}$	$K_{m,corr}$	ΔT_{nom}
[m³/h]	[s]	[kg/h]	[kg/m³]	[°C]	11.4850	Pulses/Liter	140.0560	Pulses/kg	28.8000	Pulses/liter	T _{nom} - T _{corr}
03.06.2019	10	423.090	9.912	9.941	1164.861	1.168	997.016	2.90	27.62	25.70	0.81
03.06.2019	10	422.990	9.946	1156.927	1.160	997.007	2.90	27.65	25.80	0.81	-0.047
03.06.2019	10	423.070	9.922	9.882	1154.225	1.158	996.996	2.90	27.69	26.00	0.81
03.06.2019	10	422.929	9.995	9.845	150.763	1.154	996.996	2.90	27.69	25.90	0.81
03.06.2019	10	422.993	9.986	9.816	1149.853	1.153	996.988	2.90	27.72	25.90	0.81
03.06.2019	30	178.095	30.195	30.186	1488.629	1.493	996.993	2.93	27.74	26.10	0.81
03.06.2019	30	177.791	30.129	30.221	1487.978	1.492	996.981	2.93	27.75	26.10	0.81
03.06.2019	30	177.998	30.147	30.238	1490.778	1.495	996.980	2.92	27.75	26.20	0.81
03.06.2019	30	177.998	30.162	30.253	1491.388	1.496	996.983	2.92	27.74	26.20	0.81
03.06.2019	30	178.096	30.148	30.240	1491.478	1.496	996.980	2.92	27.75	26.30	0.81
03.06.2019	60	88.091	59.987	60.169	1484.519	1.489	996.978	2.88	27.75	26.50	0.81
03.06.2019	60	88.094	59.964	60.146	1484.038	1.489	996.976	2.89	27.76	26.50	0.81
03.06.2019	60	88.951	60.110	60.293	1485.239	1.490	996.976	2.88	27.76	26.70	0.81
03.06.2019	60	88.976	60.122	60.304	1485.949	1.490	996.982	2.89	27.74	26.70	0.81
03.06.2019	60	88.975	60.102	60.284	1485.388	1.490	996.982	2.89	27.74	26.80	0.81
03.06.2019	100	53.194	100.024	100.329	147.957	1.482	996.964	2.75	27.78	26.89	0.81
03.06.2019	100	52.902	99.682	99.986	1464.823	1.469	996.964	2.76	27.78	26.89	0.81
03.06.2019	100	53.004	99.393	100.297	1472.215	1.477	996.967	2.75	27.77	26.89	0.81
03.06.2019	100	52.999	99.884	100.189	1470.485	1.475	996.964	2.76	27.78	26.89	0.81
03.06.2019	100	53.025	99.818	100.122	1470.224	1.475	996.967	2.75	27.77	26.89	0.81
03.06.2019	130	275.076	130.161	130.561	994.628	9.976	996.956	2.70	27.87	27.98	0.81
03.06.2019	130	275.155	130.165	130.566	994.732	9.979	996.958	2.70	27.90	28.08	0.81
03.06.2019	130	274.847	130.046	130.447	992.541	9.959	996.925	2.70	27.91	28.18	0.81
03.06.2019	130	275.065	129.965	130.367	993.033	9.961	996.921	2.67	27.92	28.28	0.81
03.06.2019	130	274.947	130.178	130.381	994.224	9.973	996.914	2.70	27.95	28.38	0.81
03.06.2019	150	239.075	150.412	150.882	998.876	10.020	996.886	2.53	28.02	28.08	0.81
03.06.2019	150	239.003	150.120	150.590	996.605	9.988	996.880	2.53	28.04	28.28	0.81
03.06.2019	150	239.084	150.411	150.885	998.239	10.019	996.869	2.53	28.08	28.38	0.81
03.06.2019	150	238.917	150.411	150.885	998.239	10.014	996.860	2.53	28.11	28.48	0.81
03.06.2019	150	239.008	150.047	150.520	996.1798	9.993	996.858	2.53	28.12	28.48	0.81
03.06.2019	150	239.008	150.047	150.520	996.1798	9.993	996.856	2.53	28.12	28.48	0.81

CENAM Laboratory – Day#2

CENAM Laboratory – Day#3

Data report CENAM: Day#3										Original data set		Temperature correction of meter error										
Turbine meter										Coriolis Mass					Coriolis Vol					Coriolis Coriolis meter		
Laboratory reference					Fluid					Ambient conditions					K _{ν,corr}					Pulses/Liter		
Date	Nominal flowrate	Standard mass flowrate	Standard volume flowrate	Mass	Volume	Water density	Line pressure	Air temp.	Air pressure	Pulse count	Kfactor	Meter error	Pulse count	K-factor	Meter error	Pulse count	K-factor	Meter error	Pulse count	T _{nom}	20 °C	
V _{ν,corr}	t	m [*] _{ref}	V [*] _{ref}	m _{ref}	V _{ref}	[kg/m ³]	[bar]	[°C]	[bar]	p _{Air}	T _{air}	e _v	N	K _m	e _m	N	K _v	e _v	e _{corr,m}	e _{corr,v}		
05.06.2019	10	432.959	9.910	1.191.532	1.146	996.955	2.90	27.30	25.30	0.81	171314	143.7280	-0.233	34395	28.7689	-0.120	7.800	-0.124	0.033			
05.06.2019	10	433.027	9.901	1.190.891	1.195	996.959	2.90	27.82	25.40	0.81	171156	143.7209	-0.193	34363	28.7671	-0.114	7.820	-0.103	0.028			
05.06.2019	10	432.963	9.891	1.189.920	1.193	996.951	2.90	27.85	25.50	0.81	171033	143.7711	-0.193	34339	28.7775	-0.078	7.850	-0.143	0.064			
05.06.2019	10	433.079	9.883	1.188.910	1.193	996.945	2.90	27.87	25.60	0.81	170881	143.7292	-0.227	34309	28.7694	-0.106	7.870	-0.098	0.035			
05.06.2019	10	432.913	9.872	1.187.098	1.191	996.934	2.90	27.91	25.70	0.81	170562	143.6792	-0.261	34245	28.7592	-0.142	7.910	-0.163	0.002			
05.06.2019	10	433.048	9.880	1.188.489	1.192	996.934	2.91	27.91	25.80	0.81	170749	143.6690	-0.269	34283	28.7574	-0.148	7.910	-0.129	-0.006			
05.06.2019	10	432.947	9.875	1.187.748	1.191	996.928	2.91	27.93	25.80	0.81	170998	143.6557	-0.273	34253	28.7549	-0.157	7.930	-0.116	-0.015			
05.06.2019	10	433.006	9.904	1.187.658	1.191	996.925	2.90	27.94	25.80	0.81	170612	143.6651	-0.271	34257	28.7527	-0.116	7.940	-0.111	-0.008			
05.06.2019	10	432.995	9.885	1.186.816	1.190	996.917	2.90	27.97	25.90	0.81	170435	143.6432	-0.287	34221	28.7521	-0.164	7.970	-0.132	-0.023			
05.06.2019	10	432.968	9.859	1.185.736	1.189	996.914	2.90	27.98	26.00	0.81	170270	143.5956	-0.313	34189	28.7446	-0.192	7.980	-0.125	-0.054			
05.06.2019	100	53.093	10.025	1.475.772	1.480	996.900	2.72	28.00	26.30	0.81	212275	143.8885	-0.109	42733	28.8784	-0.272	8.000	-0.173	0.014			
05.06.2019	100	53.063	10.024	1.472.950	1.478	996.899	2.69	28.00	26.40	0.81	212093	143.8209	-0.087	42669	28.8796	-0.273	8.000	-0.176	0.017			
05.06.2019	100	52.965	99.833	10.0143	1468.799	1.473	996.902	2.69	27.99	26.40	0.81	211940	143.9203	-0.094	42549	28.8788	-0.274	7.990	-0.171	0.029		
05.06.2019	100	53.002	100.034	10.01345	1472.780	1.477	996.905	2.69	27.98	26.50	0.81	211874	143.8599	-0.136	42557	28.8739	-0.257	7.980	-0.117	-0.013		
05.06.2019	100	53.029	100.060	10.01371	1473.916	1.478	996.902	2.70	27.99	26.60	0.81	212055	143.8724	-0.127	42680	28.8731	-0.118	7.990	-0.132	-0.004		
05.06.2019	100	52.981	99.968	10.01278	1471.209	1.476	996.908	2.70	27.97	26.60	0.81	211681	143.8823	-0.121	42611	28.8737	0.255	7.970	-0.163	0.003		
05.06.2019	100	52.993	99.871	10.01381	1470.139	1.475	996.910	2.68	27.96	26.50	0.81	211509	143.8700	-0.129	42577	28.8717	0.249	7.960	-0.150	-0.006		
05.06.2019	100	53.134	99.869	10.01778	1474.010	1.479	996.913	2.68	27.95	26.60	0.81	212059	143.8654	-0.132	42680	28.8656	0.228	7.950	-0.139	-0.010		
05.06.2019	100	52.864	99.912	10.02222	1467.157	1.472	996.910	2.69	27.96	26.70	0.81	211085	143.8735	-0.127	42482	28.8658	0.229	7.960	-0.140	-0.004		
05.06.2019	150	239.059	149.891	150.366	995.5102	9.987	996.841	2.43	28.16	27.09	0.81	1432466	143.8912	-0.114	288361	28.8744	0.253	8.160	-0.692	0.006		
05.06.2019	150	238.974	150.014	150.048	150.523	995.6163	9.950	996.842	2.44	28.16	27.19	0.81	1433011	143.9026	-0.105	288511	28.8807	0.280	8.160	-0.689	0.014	
05.06.2019	150	239.002	150.048	150.048	150.523	995.6163	9.950	996.841	2.43	28.16	27.19	0.81	1433482	143.9027	-0.108	288505	28.8762	0.265	8.160	-0.654	0.013	
05.06.2019	150	239.078	150.281	150.528	998.029	10.012	996.838	2.48	28.18	27.19	0.81	1456144	143.8890	-0.110	288094	28.8749	0.260	8.180	-0.664	0.011		
05.06.2019	150	238.921	149.869	150.446	995.3008	9.985	996.830	2.43	28.20	27.19	0.81	1452292	143.9054	-0.105	288338	28.8781	0.271	8.200	-0.671	0.017		
05.06.2019	150	239.200	150.158	150.040	997.715	10.009	996.801	2.48	28.31	27.39	0.81	145526	143.8910	-0.115	288019	28.8753	0.262	8.310	-0.601	0.009		
05.06.2019	150	239.079	149.945	150.429	995.7983	9.990	996.781	2.42	28.37	27.39	0.81	145288	143.8934	-0.113	288460	28.8745	0.259	8.370	-0.628	0.011		
05.06.2019	150	238.987	150.113	150.599	995.6182	9.998	996.772	2.48	28.41	27.29	0.81	1453076	143.8914	-0.114	288698	28.8757	0.263	8.410	-0.657	0.010		
05.06.2019	150	239.006	150.187	150.175	997.0180	10.003	996.761	2.42	28.44	27.29	0.81	145134	143.8810	-0.115	288852	28.8734	0.255	8.440	-0.665	0.010		
05.06.2019	150	238.991	149.863	150.353	994.8392	9.981	996.746	2.42	28.49	27.29	0.81	1451406	143.8759	-0.125	288171	28.8709	0.246	8.490	-0.609	0.001		

PTB Laboratory – Day#1

Data report PTB: Day#1																	
*Original data set																	
Turbine meter																	
Coriolis Mass										Coriolis Vol							
$K_{V,nom}$										$K_{V,nom}$							
11.4850 pulses/Liter										28.8000 pulses/liter							
Coriolis Mass																	
Coriolis Vol																	
Corr. meter error																	
Corr. meter error																	
Temperature correction of meter error																	
T_{nom} 20 °C																	
Fluid																	
Ambient conditions																	
Date	Nominal flowrate	Standard volume flowrate	Mass	Volume	Water density	Line pressure	Air temp.	Air pressure	Pulse count	K-factor	Meter error	Pulse count	K-factor	Meter error			
V_{nom}	m_{ref}	V_{ref}	m_{ref}	V_{ref}	ρ_{fluid}	p_{fluid}	T_{air}	p_{air}	N	K_m	e_v	N	K_m	e_v			
08.08.2019	10.972.108	10.067	10.084	2718.304	2.723	998.311	3.00	20.01	22.25	1.00	31275	11.4859	0.007	392944	144.5548	0.346	
08.08.2019	10.972.106	9.966	9.983	2691.085	2.696	998.313	3.00	20.00	22.28	1.00	30957	11.4851	-0.008	38913	144.6045	0.381	
08.08.2019	10.972.132	9.946	9.963	2685.814	2.690	998.313	3.00	20.00	22.32	1.00	30896	11.4840	-0.006	38295	144.5726	0.359	
08.08.2019	10.972.109	10.008	10.025	2702.589	2.707	998.314	3.00	20.00	22.32	1.00	31090	11.4844	-0.006	39067	144.5899	0.371	
08.08.2019	10.972.132	10.006	10.023	2701.974	2.707	998.312	3.00	20.00	22.36	1.00	31083	11.4844	-0.006	390701	144.5984	0.377	
08.08.2019	30.324.129	30.191	30.242	2718.290	2.723	998.312	2.99	20.00	22.47	1.00	31316	11.5010	0.139	391908	144.1745	0.082	
08.08.2019	30.324.111	30.068	30.119	2707.026	2.712	998.314	3.01	19.99	22.49	1.00	31184	11.5002	0.132	39287	144.1746	0.083	
08.08.2019	30.324.114	30.058	30.108	2706.142	2.711	998.313	3.01	20.00	22.50	1.00	31175	11.5007	0.135	391517	144.1746	0.082	
08.08.2019	30.324.111	29.966	30.037	2699.682	2.704	998.313	3.02	20.00	22.51	1.00	31011	11.5008	0.137	389263	144.1885	0.092	
08.08.2019	30.324.109	30.054	30.105	2705.784	2.710	998.312	3.01	20.00	22.53	1.00	31172	11.5011	0.139	391014	144.1747	0.085	
08.08.2019	60.162.117	60.243	60.315	2711.537	2.716	998.308	3.00	20.02	22.53	1.00	31244	11.5011	0.157	39031	144.0839	0.019	
08.08.2019	60.162.094	59.890	59.992	2696.594	2.701	998.296	3.01	20.08	22.55	1.00	31071	11.5027	0.153	389584	144.0985	0.023	
08.08.2019	60.162.137	60.129	60.231	2708.110	2.713	998.311	3.00	20.01	22.55	1.00	31204	11.5030	0.156	392655	144.1097	0.037	
08.08.2019	60.162.095	60.267	60.369	2713.620	2.718	998.310	2.98	20.01	22.57	1.00	31268	11.5031	0.157	391053	144.1075	0.036	
08.08.2019	60.162.113	59.771	59.872	2691.568	2.696	998.312	3.02	20.00	22.59	1.00	31013	11.5028	0.154	387857	144.1098	0.031	
08.08.2019	100.97.319	95.872	100.043	2699.848	2.704	998.294	3.00	20.09	22.58	1.00	31110	11.5032	0.158	388982	144.0755	0.014	
08.08.2019	100.97.318	100.282	100.453	2710.894	2.716	998.294	2.99	20.09	22.61	1.00	31239	11.5038	0.163	390591	144.0820	0.018	
08.08.2019	100.97.339	100.146	100.387	2715.092	2.720	998.294	3.02	20.09	22.61	1.00	31287	11.5037	0.162	391202	144.0842	0.020	
08.08.2019	100.97.339	100.040	100.612	2717.759	2.720	998.294	2.99	20.09	22.63	1.00	31293	11.5031	0.157	391300	144.0849	0.020	
08.08.2019	100.97.319	100.785	100.550	2714.331	2.729	998.293	2.99	20.10	22.62	1.00	31394	11.5039	0.164	392532	144.0838	0.019	
08.08.2019	130.74.860	131.555	131.330	2730.918	2.736	998.290	2.95	20.11	22.67	1.00	31476	11.5061	0.183	39472	144.0805	0.017	
08.08.2019	130.74.883	131.833	132.114	2735.437	2.750	998.289	2.93	20.11	22.69	1.00	31643	11.5059	0.162	39559	144.0896	0.023	
08.08.2019	130.74.905	128.615	128.536	2676.073	2.681	998.289	2.99	20.11	22.70	1.00	30844	11.5061	0.183	38562	144.0776	0.015	
08.08.2019	130.74.882	128.851	129.172	2682.238	2.687	998.289	3.01	20.11	22.69	1.00	30915	11.5061	0.183	386472	144.0857	0.021	
08.08.2019	130.74.883	128.900	129.121	2681.206	2.686	998.288	3.01	20.12	22.69	1.00	30903	11.5061	0.182	386328	144.0874	0.022	

PTB Laboratory – Day#2

Data report PTB: Day#2												*Original data set
Date	Nominal flowrate	Measurement time	Standard mass flowrate	Standard volume flowrate	Fluid	Ambient conditions	Turbine meter	Coriolis Mass	Coriolis Vol	Coriolis Mass	Coriolis Vol	Temperature correction of meter error
09.08.2019	10	972.127	9.983	10.000	2695.514	2.700	998.313	3.00	20.00	21.90	1.00	$K_{v, nom}$
09.08.2019	10	972.118	10.091	10.108	2724.423	2.730	998.315	3.00	19.99	21.97	1.00	$K_{v, nom}$
09.08.2019	10	972.116	10.016	10.033	2704.742	2.709	998.311	3.01	20.01	22.03	1.00	$K_{v, nom}$
09.08.2019	10	972.138	10.020	10.036	2705.651	2.710	998.312	3.00	20.00	22.09	1.00	$K_{v, nom}$
09.08.2019	10	972.106	10.052	10.069	2714.458	2.719	998.314	3.00	19.99	22.15	1.00	$K_{v, nom}$
09.08.2019	30	324.110	30.084	30.135	2704.986	2.713	998.318	3.00	19.97	22.24	1.00	$K_{v, nom}$
09.08.2019	30	324.109	30.024	30.075	2703.099	2.708	998.325	2.99	19.94	22.27	1.00	$K_{v, nom}$
09.08.2019	30	324.111	30.065	30.116	2706.925	2.711	998.314	3.00	19.99	22.29	1.00	$K_{v, nom}$
09.08.2019	30	324.113	30.092	30.143	2709.156	2.714	998.307	3.00	20.03	22.31	1.00	$K_{v, nom}$
09.08.2019	30	324.114	30.078	30.129	2707.992	2.713	998.318	3.00	19.98	22.33	1.00	$K_{v, nom}$
09.08.2019	60	162.136	60.130	60.232	2708.114	2.713	998.309	3.00	20.02	22.35	1.00	$K_{v, nom}$
09.08.2019	60	162.095	60.064	60.166	2704.484	2.709	998.308	3.00	20.02	22.37	1.00	$K_{v, nom}$
09.08.2019	60	162.118	60.366	60.468	2718.435	2.723	998.310	2.99	20.01	22.39	1.00	$K_{v, nom}$
09.08.2019	60	162.095	60.544	60.647	2726.688	2.731	998.312	2.98	20.00	22.40	1.00	$K_{v, nom}$
09.08.2019	60	162.073	60.065	60.166	2704.132	2.709	998.311	3.00	20.01	22.42	1.00	$K_{v, nom}$
09.08.2019	100	97.197	100.812	100.984	2742.419	2.729	998.292	3.01	20.10	22.44	1.00	$K_{v, nom}$
09.08.2019	100	97.320	102.340	102.515	2766.582	2.771	998.294	3.00	20.09	22.47	1.00	$K_{v, nom}$
09.08.2019	100	97.297	100.057	100.228	2704.426	2.709	998.294	3.00	20.09	22.47	1.00	$K_{v, nom}$
09.08.2019	100	97.321	100.028	100.199	2704.103	2.709	998.293	3.00	20.10	22.46	1.00	$K_{v, nom}$
09.08.2019	100	97.319	99.994	100.165	2703.335	2.708	998.295	2.99	20.09	22.47	1.00	$K_{v, nom}$
09.08.2019	130	74.882	130.406	130.629	2712.496	2.717	998.289	2.99	20.12	22.49	1.00	$K_{v, nom}$
09.08.2019	130	74.966	129.764	129.987	2698.682	2.703	998.289	2.98	20.12	22.50	1.00	$K_{v, nom}$
09.08.2019	130	74.885	129.917	130.140	2704.335	2.707	998.289	2.98	20.11	22.52	1.00	$K_{v, nom}$
09.08.2019	130	74.881	130.464	130.920	2709.021	2.714	998.289	3.00	20.11	22.54	1.00	$K_{v, nom}$
09.08.2019	130	74.883	130.104	130.327	2706.949	2.711	998.289	2.99	20.12	22.54	1.00	$K_{v, nom}$
09.08.2019	150	64.818	150.843	151.105	2720.138	2.725	998.267	3.02	20.22	22.55	1.00	$K_{v, nom}$
09.08.2019	150	64.899	147.519	147.772	2659.373	2.664	998.284	2.99	20.14	22.57	1.00	$K_{v, nom}$
09.08.2019	150	64.897	147.180	147.433	2653.324	2.658	998.285	2.96	20.13	22.57	1.00	$K_{v, nom}$
09.08.2019	150	64.918	151.346	151.606	2729.912	2.734	998.283	2.93	20.14	22.57	1.00	$K_{v, nom}$
09.08.2019	150	64.922	151.419	151.680	273.057	2.735	998.282	2.99	20.15	22.57	1.00	$K_{v, nom}$
09.08.2019	150	64.922	151.419	151.680	273.057	2.735	998.282	2.99	20.15	22.57	1.00	$K_{v, nom}$

PTB Laboratory – Day#3

Data report PTB: Day#3												*Original data set															
Turbine meter														Coriolis Mass		Coriolis_Vol		Coriolis_Mass		Coriolis_Vol		Coriolis_Mass		Coriolis_Vol			
Ambient conditions														K _{V,corr}		K _{m,corr}		K _{V,corr}		K _{m,corr}		K _{V,corr}		K _{m,corr}			
Date	Nominal flowrate	t	m [*] _{ref}	V [*] _{ref}	m _{ref}	V _{ref}	p _{ref}	T _{ref}	p _{ref}	T _{ref}	p _{ref}	T _{ref}	K _{V,corr}	Pulses/liter	K _{m,corr}	Pulses/kg	K _{V,corr}	Pulses/liter	K _{m,corr}	Pulses/kg	K _{V,corr}	Pulses/liter	K _{m,corr}	Pulses/kg			
Measurement reference	Standard volume flowrate	Mass	Volume	Water density	Water pressure	Line pressure	Air temp.	Air pressure	Air temp.	Air pressure	Air temp.	Air pressure															
12.08.2019	10	972.111	9.967	9.983	2691.382	2.696	988.311	3.00	20.01	22.68	1.01	31161	11.4852	0.007	391340	144.0560	144.0560	144.0560	145.0551	0.659	0.013	0.009	-0.012	-0.014	-0.021		
12.08.2019	10	972.133	9.967	9.946	2708.332	2.713	988.319	3.00	19.97	22.63	1.01	30965	[Pulses]	[%]	392722	[Pulses/kg]	[%]	[Pulses]	[%]	[%]	[%]	[%]	[%]	[%]	[%]		
12.08.2019	10	972.111	10.030	10.047	2681.208	2.686	988.306	3.00	20.03	22.63	1.01	30847	11.4854	0.003	388851	145.0283	0.675	0.022	0.034	-0.024	-0.031	-0.019	-0.014	-0.025			
12.08.2019	10	972.114	10.029	10.046	2708.083	2.713	988.314	3.00	20.00	22.72	1.01	31159	11.4865	0.012	392712	145.0148	0.666	0.019	-0.004	-0.009	-0.001	-0.007	-0.007	-0.022			
12.08.2019	10	972.109	10.033	10.049	2709.090	2.714	988.313	3.00	20.00	22.79	1.01	31171	11.4867	0.014	392798	144.9926	0.650	0.014	-0.001	-0.007	-0.001	-0.007	-0.009	-0.020			
12.08.2019	10	972.114	10.002	10.019	2700.880	2.705	988.311	3.00	20.01	22.81	1.01	31076	11.4865	0.012	391653	144.9983	0.654	0.006	0.008	-0.001	-0.003	-0.001	-0.006	-0.009	-0.019		
12.08.2019	10	972.112	10.066	10.083	2718.086	2.723	988.313	3.00	20.00	22.84	1.01	31275	11.4868	0.015	394073	144.9818	0.643	0.003	0.001	-0.001	-0.001	-0.001	-0.001	-0.003	-0.019		
12.08.2019	10	972.116	10.039	10.056	2710.910	2.715	988.313	3.00	20.00	22.86	1.01	31193	11.4871	0.017	393106	145.0089	0.661	0.016	-0.002	-0.004	-0.004	-0.004	-0.002	-0.019			
12.08.2019	10	972.148	9.946	9.962	2685.711	2.690	988.313	3.00	20.00	22.88	1.01	30591	11.4863	0.010	389521	145.0346	0.679	0.028	0.001	-0.011	-0.011	-0.009	-0.001	-0.020			
12.08.2019	10	972.124	10.006	10.023	2701.922	2.706	988.313	3.00	20.00	22.88	1.01	31088	11.4865	0.012	391911	145.0490	0.659	0.041	0.000	-0.009	-0.004	-0.001	-0.001	-0.023			
12.08.2019	100	97.297	100.284	100.456	2710.362	2.715	988.292	3.01	20.10	22.88	1.01	31234	11.5042	0.167	391052	144.1106	0.038	0.101	0.101	0.101	0.164	-0.023	0.001	-0.023			
12.08.2019	100	97.318	100.459	100.631	2715.688	2.720	988.292	3.00	20.10	22.90	1.01	31295	11.5041	0.165	391323	144.0972	0.029	0.032	0.032	0.032	0.163	-0.032	0.001	-0.032			
12.08.2019	100	97.299	99.929	99.107	2647.051	2.652	988.293	3.00	20.10	22.91	1.01	30594	11.5041	0.165	381466	144.1058	0.037	0.029	0.029	0.029	0.163	-0.032	0.001	-0.032			
12.08.2019	100	97.318	99.647	99.817	2633.721	2.698	988.293	2.99	20.10	22.91	1.01	31042	11.5042	0.166	383824	144.1218	0.046	0.036	0.036	0.036	0.164	-0.035	0.001	-0.035			
12.08.2019	100	97.319	99.646	99.816	2685.726	2.698	988.295	2.99	20.09	22.92	1.01	31068	11.5043	0.167	388502	144.1054	0.659	0.087	-0.007	-0.002	-0.002	-0.002	-0.008	-0.026			
12.08.2019	100	97.296	99.752	99.923	2695.958	2.701	988.294	3.00	20.09	22.93	1.01	31086	11.5043	0.167	391450	144.1054	0.659	0.091	0.065	-0.007	-0.007	-0.007	-0.007	-0.027			
12.08.2019	100	97.319	99.758	99.958	2697.556	2.702	988.293	3.00	20.10	22.94	1.01	31086	11.5041	0.165	383784	144.1245	0.048	0.097	0.097	0.097	0.163	-0.014	0.001	-0.014			
12.08.2019	100	97.318	99.870	100.041	2659.746	2.704	988.292	3.00	20.10	22.94	1.00	31112	11.5044	0.168	383960	144.1099	0.037	0.028	0.028	0.028	0.166	-0.024	0.001	-0.024			
12.08.2019	100	97.298	99.671	99.842	2693.829	2.698	988.293	2.99	20.10	22.96	1.00	31044	11.5044	0.168	383228	144.1175	0.043	0.098	0.098	0.098	0.166	-0.022	0.001	-0.022			
12.08.2019	100	97.297	99.561	99.731	2690.810	2.695	988.294	2.99	20.09	22.96	1.00	31009	11.5044	0.168	383733	144.1250	0.048	0.091	0.091	0.091	0.166	-0.021	0.001	-0.021			
12.08.2019	150	64.519	151.582	151.842	2733.468	2.738	988.285	2.95	20.13	22.96	1.00	31514	11.5092	0.210	393852	144.0997	0.030	0.134	0.134	0.134	0.210	-0.008	0.001	-0.008			
12.08.2019	150	64.920	150.555	150.813	2714.980	2.720	988.286	2.99	20.13	22.96	1.00	31320	11.5089	0.207	391241	144.1046	0.034	0.132	0.132	0.132	0.207	-0.005	0.001	-0.005			
12.08.2019	150	64.899	150.675	150.934	2716.275	2.721	988.285	2.99	20.14	22.97	1.00	31315	11.5089	0.207	391473	144.1213	0.045	0.135	0.135	0.135	0.208	-0.005	0.001	-0.005			
12.08.2019	150	64.896	150.375	150.634	2710.784	2.715	988.285	2.98	20.14	22.96	1.00	31252	11.5090	0.208	390554	144.0742	0.013	0.136	0.136	0.136	0.209	-0.026	0.001	-0.026			
12.08.2019	150	64.920	150.902	151.161	2721.249	2.726	988.285	3.00	20.13	22.97	1.00	31373	11.5091	0.209	392102	144.0890	0.023	0.134	0.134	0.134	0.210	-0.016	0.001	-0.016			
12.08.2019	150	64.896	150.822	151.091	2719.011	2.724	988.283	3.00	20.14	22.96	1.00	31347	11.5091	0.208	391753	144.0940	0.026	0.133	0.133	0.133	0.209	-0.012	0.001	-0.012			
12.08.2019	150	64.898	151.011	151.271	2722.291	2.727	988.284	3.01	20.14	22.96	1.00	31385	11.5091	0.209	392325	144.1157	0.041	0.142	0.142	0.142	0.210	-0.003	0.001	-0.003			
12.08.2019	150	64.898	150.289	150.548	2709.280	2.714	988.285	2.98	20.13	22.96	1.00	31325	11.5091	0.209	390428	144.1077	0.036	0.134	0.134	0.134	0.210	-0.003	0.001	-0.003			
12.08.2019	150	64.899	150.171	150.429	2707.227	2.712	988.284	2.97	20.14	22.96	1.00	31210	11.5086	0.205	390689	144.0917	0.025	0.142	0.142	0.142	0.205	-0.014	0.001	-0.014			
12.08.2019	150	64.921	151.133	151.382	2725.309	2.730	988.285	3.01	20.14	22.96	1.00	31320	11.5087	0.205	393668	144.0820	0.018	0.135	0.135	0.135	0.201	-0.021	0.001	-0.021			