## Rockwell Hardness HR45N Scale Definition

| Reference values for HR45N |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Symbol | Test parameter | Reference value | Start measurement | Stop measurement |
| $F_{0}$ | Preliminary test force | 29,419 95 N ${ }^{1}$ |  |  |
| $F$ | Total test force | 441,299 $25 \mathrm{~N}^{1}$ |  | - |
| $\alpha$ | Included angle of the indenter cone (between surface axial-plane line segments) | $120^{\circ}$ | Line segment start: $\pm 30^{\circ}$ (from the axis) ${ }^{2}$ | Line segment end: $400 \mu \mathrm{~m}$ on conical surface |
| $r$ | Spherical tip radius of the indenter | $200 \mu \mathrm{~m}$ | $-30^{\circ}$ (from the axis) ${ }^{2}$ | $+30^{\circ}$ (from the axis) ${ }^{2}$ |
| $t_{\text {pa }}$ | Application time of preliminary test force | $0,2 \mathrm{~s} \leq t_{\mathrm{pa}} \leq 2 \mathrm{~s}$ | $\sim 1 \%{ }_{0}$ | $\sim 99 \% F_{0}$ |
| $t_{\text {pd }}$ | Duration time of constant preliminary test force before initial measurement | $\left(3-t_{\mathrm{pa}} / 2\right) \mathrm{s}$ | $\sim 99 \% F_{0}$ | Measurement |
| $t_{\text {aa }}$ | Application time of additional test force | $\leq 4 \mathrm{~s}^{3}$ | $\sim 101 \%{ }_{0}$ | ~99 \% F (loading) |
| $V_{\text {fa }}$ | Mean indentation velocity of final additional test force application | $30 \mu \mathrm{~m} \cdot \mathrm{~s}^{-1}$ | $\sim 80$ \% F | ~99 \% F |
| $t_{\text {td }}$ | Duration time of total test force | 5 s | ~99 \% F (loading) | ~99 \% F (unloading) |
| $t_{\text {ar }}$ | Removal time of additional test force | $\leq 2$ s | ~99 \% F (unloading) | $\sim 101$ \% Fo |
| $t_{\text {rd }}$ | Duration time of recovery force before final measurement | 4 s | $\sim 101$ \% Fo | Measurement |
| T | Temperature of test | $23^{\circ} \mathrm{C}$ | Start of test | End of test |
|  | ${ }^{1}$ The defined values of preliminary test force and total test force are the SI equivalents of the original Rockwell hardness method-defined forces of 3 kgf and 45 kgf , respectively, converted to N by multiplying the kgf values by the conversion factor 9,80665 . <br> ${ }^{2}$ These dimensions define the theoretical points of blend between the spherical tip and conical surface of the diamond indenter (see Figure 2). The actual points of blend are usually different; therefore, the blend areas should not be included in the measurement of the tip radius or cone angle. <br> ${ }^{3}$ The value of $t_{a a}$ is dependent on the hardness of the material under test. The stated range of $\leq 4 s$ is to maintain compliance with consensus standards. |  |  |  |

Figure 1. Illustrations of the applied force and the resulting indentationdepth occurring during the HR45N test cycle.


Figure 2. Illustration of the axial cross-section of an ideally-shaped diamond indenter indicating the dimensions specified above and the theoretical points of blend between the spherical tip and conical surface.


