

CCM.FF-K3.2011.1

CIPM Key Comparison of Air Speed, 0.5 m/s to 40 m/s

Final Report

Pilots

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Abstract

The bilateral key comparison between PTB and VNIIM (CCM.FF-K3.2011.1) was performed as direct follow-up of the CIPM Air speed Key Comparison (CCM.FF-K3.2011) which was organized to determine the degree of equivalence of the national standards for air speed covering the range 0.5 m/s to 40 m/s under ambient conditions. An ultrasonic anemometer and a laser Doppler anemometer were used as transfer standards. The measurement procedures in the technical protocol as well as the transfer standards for the bilateral key comparison (CCM.FF-K3.2011.1) were identical to the CIPM Key Comparison (CCM.FF-K3.2011) with nine participants from three RMOs. Thus, the measurement results were directly linked to the key comparison reference values published in the final report of the (CCM.FF-K3.2011) for each standard and each air speed separately. The degree of equivalence of each result with the key comparison reference value (KCRV) was calculated. All reported results of the bilateral key comparison were consistent with the KCRV results of the (CCM.FF-K3.2011).

Graphical summary of results

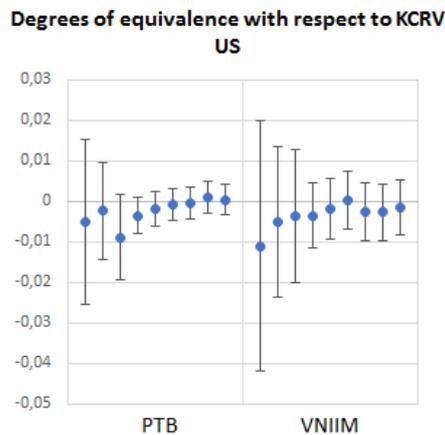


Figure 1 – Degrees of equivalence with respect to KCRV (CCM.FF-K3.2011) of PTB and VNIIM for the ultrasonic anemometer at the different air speeds. The error bars show the expanded uncertainty of the degree of equivalence for each calibrated value.

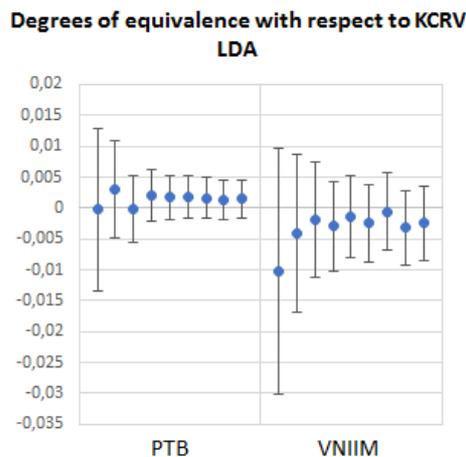


Figure 2 – Degrees of equivalence with respect to KCRV (CCM.FF-K3.2011) of PTB and VNIIM for the laser Doppler anemometer at the different air speeds. The error bars show the expanded uncertainty of the degree of equivalence for each calibrated value.

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1. INTRODUCTION

The Key Comparison CCM.FF.K3.2011 for air speed and its follow-up, the bilateral key comparison CCM.FF.K.2011.1 between VNIIM and PTB, have been undertaken by CCM (Consultative Committee for Mass and related quantities) Working Group for Fluid Flow (WGFF) and were piloted by PTB (National Metrology Institute of Germany) and LNE-CETIAT (Designated Institute for Air Speed of France). Two transfer standards were used. The first one was an ultrasonic anemometer similar to the one used in the Key Comparison CCM.FF-K3 [1]. The second one was a laser Doppler anemometer, known as the best transfer standard in the field which had already shown its interest during the EURAMET comparison 827 [2]. It was especially designed to avoid unintentional changes of the LDA operating parameters by the laboratories during the calibration.

The objective of the key comparisons is to determine the key comparison reference values (KCRVs) for air speed measurement and to demonstrate the degree of equivalence among the participating National Metrology Institutes (NMIs) and Designated Institutes (DIs). The participants calibrated the transfer standards and compared the calibration results.

This report was prepared in accordance with the relevant guidelines [3 – 7].

2. PARTICIPANTS AND ORGANIZATION OF THE COMPARISON

2.1. Participants

The participants are listed in table 1.

Table 1 - List of the participating NMIs, facilities used, dates of test and independence of the participant's traceability from other participants

Participant (Country)	Type of reference standard	Date of tests	Independent traceability?
PTB (Germany)	LDA standard	Test period: July 2013, ... October 2016, ... February 2017	Yes
VNIIM (Russia)	LDA standard	January 2017	Yes

2.2. Organization of the comparison

According to the technical protocol (CCM.FF-K3.2011.1) and the corresponding contract between PTB and VNIIM from October 2016, the shipping of the transfer standards, the assumption of costs due to the transportation costs, custom clearance and delivery affairs were conjointly arranged.

2.3. Unexpected events

Thanks to the meticulous assistance of VNIIM concerning an unobstructed custom clearance and delivery, no unexpected events occurred. No influence on the stability of the travelling standards was observed.

3. TRAVELLING STANDARDS

3.1. Ultrasonic anemometer

The ultrasonic anemometer which has been used in this key comparison (KC) was manufactured by SONIC CORPORATION. The probe has three pairs of ultrasonic transducers and measures the three dimensional velocity vector derived from the time of the ultrasonic waves between pairs of transducers. The projected area of the probe is 1287 mm² and a photo is shown below.



Figure 3 - Ultrasonic Anemometer sensing element; the arrow indicates the flow direction

The arrangement of the instrument is such that the flow reaches the sensor along its main axis as shown in Figure 3. This way, the disturbance of the instrument to the flow is minimized; also, no influence of the emitters' supports on the measurements is noticeable.

Although the overall blockage effect of the instrument is quite reduced, the overall dimension of the sensor implies a diameter of about 10 cm. In order to minimize the effects of wall interaction, it is recommended to have any walls at a distance of at least 10 cm from the instrument. Therefore, only test sections of at least 30 cm diameter (or 30 cm minimum transverse direction for square/rectangular section wind tunnels) should be used.

3.2. Laser Doppler anemometer

The laser Doppler anemometer system was manufactured by ILA GmbH. The focal lens allows a working distance of approximately 500 mm. The distance between the two beams at the front lens of the LDA probe is 45 mm.

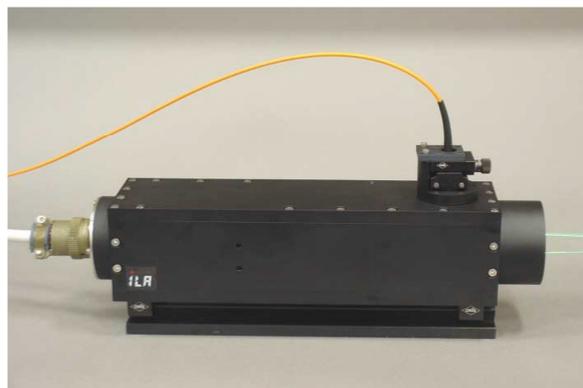


Figure 4 - Laser Doppler Anemometer probe; power 75 mW, wavelength 532 nm

The LDA system includes the controller, the signal processing unit and the software specially developed to ensure an uniform operation. A portable measurement PC specified as signal processing unit is also enclosed in the LDA-transportation box to record the data from the laser Doppler anemometer as well as from the ultrasonic anemometer.

4. MEASUREMENT INSTRUCTIONS

The measurements had to be performed at ambient conditions.

The participants performed the calibration of the transfer standards for the velocities 0.5 m/s, 1.0 m/s, 2.0 m/s, 5.0 m/s, 10.0 m/s, 15.0 m/s, 20.0 m/s, 30.0 m/s and 40.0 m/s or within their own velocity range if the full range of set points is not possible.

At each speed, five repeated measurements were recorded according to the procedure of each laboratory. Both transfer standards were completely calibrated separately as two different meters under test.

Additionally, if possible, the laser Doppler anemometer could be calibrated with a primary standard according to the measurement possibility of each partner.

The participants calculated K factors at each velocity and for the both instruments, expressed as:

$$K = \frac{V_{ref}}{V_{ts}} \quad (1)$$

With:

- V_{ref} , the reference velocity measured by the participant (m/s)
- V_{ts} , the reading of the transfer standard (m/s)

5. METHODS OF MEASUREMENT

A summary of the calibration methods used by the participants is presented in Table 2.

Table 2 – Calibration method

Participant Lab (Country)	Calibration method	Reference standard
PTB (Germany)	Wind tunnel: closed loop, open test section	LDA calibrated with a rotating disk
VNIIM (Russia)	Aerodynamic facility: loop tube, open test section	LDA calibrated

6. UNCERTAINTY DUE TO THE TRANSFER STANDARDS

From the measurements at the pilot institute, PTB, the stability and reproducibility of the transfer standards were evaluated.

6.1. Ultrasonic anemometer

The stability of the K factor for each velocity is shown in Figure 5 for the ultrasonic anemometer over a time period from July 2013 to February 2017.

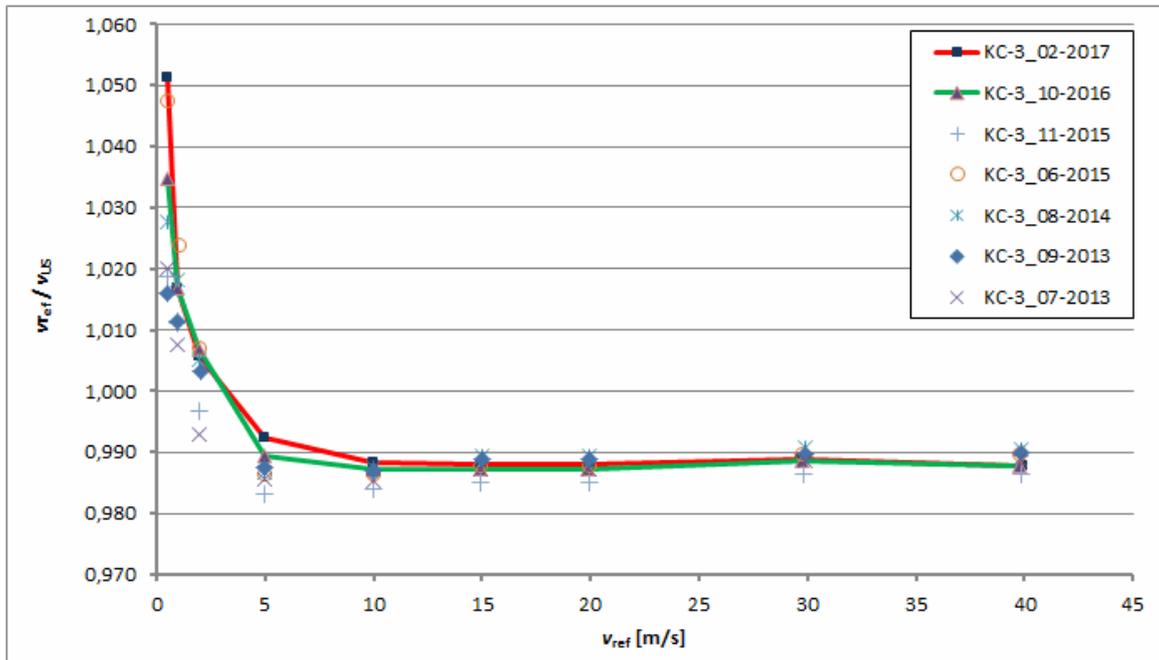


Figure 5 – K factor for the different calibrations at PTB for the ultrasonic anemometer

Five of the seven calibrations were performed at PTB between June 2013 and November 2015 and used in the CCM.FF.K3.2011 evaluation to calculate the stability of the transfer standard for each velocity and expressed as:

$$\frac{Max(K_i) - Min(K_i)}{K_{mean}} \times 100 (\%)$$

(2)

With:

- K_i , the K factor obtained by PTB at the date i
- K_{mean} , the mean K factor obtained by PTB considering all the performed calibrations.

Furthermore, the standard uncertainty at each velocity was calculated, considering a rectangular law, as the observed maximum deviation divided by the square root of 12.

The subsequent calibrations, one before (Fig. 6: green line) and one after (Fig. 6: red line) the bilateral comparison with VNIIM, are consistent with the data for the ultrasonic anemometer stability tests during the CCM.FF.K3.2011. Hence the standard uncertainty for the stability contribution was taken according to table 3 identical to the CCM.FF.K3.2011.

Considering the results obtained at PTB, this additional contribution of uncertainty due to the stability of the transfer standard was included when calculating the degree of equivalence with the KCRV from the CCM.FF.K3.2011.

Table 3 – Standard uncertainty of the ultrasonic anemometer

Nominal air speed (m/s)	Standard uncertainty for the transfer standard (%)
0.5	0.9
1	0.5
2	0.5
5	0.13
10	0.13
15	0.13
20	0.13
30	0.13
40	0.13

6.2. Laser Doppler Anemometer

The stability of the laser Doppler anemometer has been evaluated through the recalibration of the fringe spacing against the rotating wheel facility at PTB.

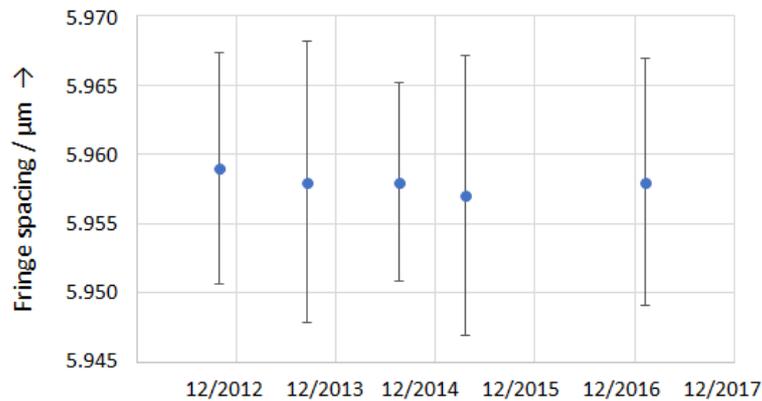


Figure 6 – Calibration of the fringe spacing at PTB over the duration of K3

With an analysis similar to the one performed for the ultrasonic anemometer an additional contribution of uncertainty due to the stability of the transfer standard has been included when calculating the uncertainty of the KCRV. The value of this standard uncertainty is 0.01% over the whole range of velocity.

7. DATA PROCESSING AND COMPUTATION OF THE DEGREE OF EQUIVALENCE TO THE KCRV

7.1. Results of the participants

7.1.1. Ultrasonic anemometer

Measurement results of PTB

The PTB measurement results were taken from the key comparison as the stability of both transfer standards was checked by PTB before and after the bilateral comparison with VNIIM and proven to be as stable as documented in the CCM.FF-K3.2011 final report.

Table 4 – PTB results for the ultrasonic anemometer

AVERAGE DATA					
Institute 's results - US anemometer					
Nominal airspeed V_{nom} [m/s]	Reference air speed V_{ref} [m/s]	Indicated air speed V_{US} [m/s]	Standard deviation air speed [m/s]	Calibration result V_{ref}/V_{US}	Lab Uncertainty $U(V_{ref}/V_{US})$
0,5	0,5014	0,492	0,001	1,0201	0,0136
1	0,9984	0,991	0,006	1,0076	0,0085
2	1,9821	1,996	0,005	0,9930	0,0060
5	5,0075	5,081	0,002	0,9855	0,0045
10	9,9997	10,148	0,009	0,9854	0,0040
15	14,9615	15,154	0,040	0,9873	0,0038
20	19,9419	20,171	0,005	0,9886	0,0038
30	29,8843	30,224	0,007	0,9887	0,0037
40	39,8130	40,238	0,005	0,9894	0,0036

Measurement results of VNIIM

Table 5 – VNIIM results for the ultrasonic anemometer

AVERAGE DATA					
Institute 's results - US anemometer					
Nominal airspeed V_{nom} [m/s]	Reference air speed V_{ref} [m/s]	Indicated air speed V_{US} [m/s]	Standard deviation air speed [m/s]	Calibration result V_{ref}/V_{US}	Lab Uncertainty $U(V_{ref}/V_{US})$
0,5	0,5343	0,527	0,014	1,0143	0,0144
1	0,9819	0,977	0,024	1,0049	0,0101
2	2,0492	2,053	0,023	0,9983	0,0074
5	5,0021	5,076	0,029	0,9854	0,0060
10	9,9713	10,120	0,055	0,9853	0,0055
15	14,8045	14,978	0,082	0,9884	0,0053
20	19,7311	20,003	0,107	0,9864	0,0053
30	30,6018	31,063	0,170	0,9852	0,0052
40	40,7300	41,247	0,245	0,9875	0,0051

7.1.2. Laser Doppler anemometer

Measurement results of PTB

The PTB measurement results were taken from the key comparison as the stability of both transfer standards was checked by PTB before and after the bilateral comparison with VNIIM and proven to be as stable as documented in the CCM.FF-K3.2011 final report.

Table 6 – PTB results for the laser Doppler anemometer

AVERAGE DATA					
Institute 's results - Laser Doppler anemometer					
Nominal airspeed V_{nom} [m/s]	Reference air speed V_{ref} [m/s]	Indicated air speed V_{LDA} [m/s]	Standard deviation air speed [m/s]	Calibration result V_{ref}/V_{LDA}	Lab Uncertainty $U(V_{ref}/V_{LDA})$
0,5	0,4904	0,491	0,011	0,9990	0,0136
1	0,9954	0,992	0,003	1,0030	0,0085
2	1,9991	1,997	0,001	1,0011	0,0060
5	4,9936	4,980	0,004	1,0027	0,0045
10	9,9975	9,965	0,007	1,0033	0,0040
15	14,9865	14,937	0,007	1,0033	0,0038
20	19,9487	19,885	0,006	1,0032	0,0037
30	29,8838	29,806	0,012	1,0026	0,0037
40	39,8588	39,774	0,010	1,0021	0,0036

Measurement results of VNIIM

Table 7 – VNIIM results for the laser Doppler anemometer

AVERAGE DATA					
Institute 's results - Laser Doppler anemometer					
Nominal airspeed V_{nom} [m/s]	Reference air speed V_{ref} [m/s]	Indicated air speed V_{LDA} [m/s]	Standard deviation air speed [m/s]	Calibration result V_{ref}/V_{LDA}	Lab Uncertainty $U(V_{ref}/V_{LDA})$
0,5	0,5003	0,506	0,004	0,9890	0,0150
1	0,9862	0,990	0,003	0,9959	0,0101
2	1,9980	1,999	0,001	0,9994	0,0075
5	4,9383	4,950	0,008	0,9977	0,0060
10	9,8276	9,825	0,004	1,0003	0,0055
15	15,0527	15,066	0,009	0,9991	0,0053
20	20,0500	20,030	0,014	1,0010	0,0052
30	29,9162	29,976	0,042	0,9980	0,0052
40	40,1341	40,207	0,052	0,9982	0,0051

7.2. Input data considering the stability of the transfer standards

The tables 8 - 11 show the input data of PTB and VNIIM considering the uncertainty contribution related to the stability of the transfer standards. The PTB data were the input data for the calculation of the *KCRV* (CCM.FF-K3.2011) and the VNIIM data for the calculation of the degree of equivalence of the VNIIM results to the *KCRV* (CCM.FF-K3.2011) (see chapter 7.3). The expanded uncertainties including the stability of the transfer standards (see chapter 6) are and listed in the tables in the columns "Pilot calculation" according to:

$$U(K)_{PC} = \sqrt{U^2(K) \text{ "Lab Uncertainty" } + U^2(\text{transfer standard})} \quad (3)$$

7.2.1. Ultrasonic anemometer

Table 8 – PTB data set

Nominal airspeed V_{nom} [m/s]	Institute 's results - Ultrasonic anemometer					Pilot calculation
	Reference air speed V_{ref} [m/s]	Indicated air speed V_{US} [m/s]	Standard deviation air speed [m/s]	Calibration result V_{ref}/V_{US}	Lab Uncertainty $U(K)$	Expanded Uncertainty $U(K)_{PC}$
0,5	0,5014	0,492	0,001	1,0201	0,0136	0,0229
1,0	0,9984	0,991	0,006	1,0076	0,0085	0,0132
2,0	1,9821	1,996	0,005	0,9930	0,0060	0,0116
5,0	5,0075	5,081	0,002	0,9855	0,0045	0,0052
10,0	9,9997	10,148	0,009	0,9854	0,0040	0,0047
15,0	14,9615	15,154	0,040	0,9873	0,0038	0,0046
20,0	19,9419	20,171	0,005	0,9886	0,0038	0,0045
30,0	29,8843	30,224	0,007	0,9887	0,0037	0,0045
40,0	39,8130	40,238	0,005	0,9894	0,0036	0,0044

Table 9 – VNIIM data set

Nominal airspeed V_{nom} [m/s]	Institute 's results - Ultrasonic anemometer					Pilot calculation
	Reference air speed V_{ref} [m/s]	Indicated air speed V_{US} [m/s]	Standard deviation air speed [m/s]	Calibration result V_{ref}/V_{US}	Lab Uncertainty $U(K)$	Expanded Uncertainty $U(K)_{PC}$
0,5	0,5343	0,527	0,014	1,0143	0,0144	0,0232
1,0	0,9819	0,977	0,024	1,0049	0,0101	0,0142
2,0	2,0492	2,053	0,023	0,9983	0,0074	0,0125
5,0	5,0021	5,076	0,029	0,9854	0,0060	0,0065
10,0	9,9713	10,120	0,055	0,9853	0,0055	0,0061
15,0	14,8045	14,978	0,082	0,9884	0,0053	0,0059
20,0	19,7311	20,003	0,107	0,9864	0,0053	0,0058
30,0	30,6018	31,063	0,170	0,9852	0,0052	0,0058
40,0	40,7300	41,247	0,245	0,9875	0,0051	0,0057

7.2.2. Laser Doppler anemometer

Table 10 – PTB data set

Nominal airspeed V_{nom} [m/s]	Institute 's results - Laser Doppler anemometer					Pilot calculation
	Reference air speed V_{ref} [m/s]	Indicated air speed V_{LDA} [m/s]	Standard deviation air speed [m/s]	Calibration result $K=V_{ref}/V_{LDA}$	Lab Uncertainty $U(K)$	Expanded Uncertainty $U(K)_{PC}$
0,5	0,4904	0,491	0,011	0,9990	0,0136	0,0136
1,0	0,9954	0,992	0,003	1,0030	0,0085	0,0085
2,0	1,9991	1,997	0,001	1,0011	0,0060	0,0060
5,0	4,9936	4,980	0,004	1,0027	0,0045	0,0045
10,0	9,9975	9,965	0,007	1,0033	0,0040	0,0040
15,0	14,9865	14,937	0,007	1,0033	0,0038	0,0038
20,0	19,9487	19,885	0,006	1,0032	0,0037	0,0038
30,0	29,8838	29,806	0,012	1,0026	0,0037	0,0037
40,0	39,8588	39,774	0,010	1,0021	0,0036	0,0036

Table 11 – VNIIM data set

Nominal airspeed V_{nom} [m/s]	Institute 's results - Laser Doppler anemometer					Pilot calculation
	Reference air speed V_{ref} [m/s]	Indicated air speed V_{LDA} [m/s]	Standard deviation air speed [m/s]	Calibration result $K=V_{ref}/V_{LDA}$	Lab Uncertainty $U(K)$	Expanded Uncertainty $U(K)_{PC}$
0,5	0,5003	0,506	0,004	0,9890	0,0150	0,0150
1,0	0,9862	0,990	0,003	0,9959	0,0101	0,0101
2,0	1,9980	1,999	0,001	0,9994	0,0075	0,0075
5,0	4,9383	4,950	0,008	0,9977	0,0060	0,0060
10,0	9,8276	9,825	0,004	1,0003	0,0055	0,0055
15,0	15,0527	15,066	0,009	0,9991	0,0053	0,0053
20,0	20,0500	20,030	0,014	1,0010	0,0052	0,0053
30,0	29,9162	29,976	0,042	0,9980	0,0052	0,0052
40,0	40,1341	40,207	0,052	0,9982	0,0051	0,0051

7.3. Degree of equivalence and linkage to the KCRV

The degree of equivalence of VNIIM to the KCRV is given by the degree of equivalence d_{PTB} as the PTB deviation from the key comparison reference value KCRV (CCM.FF-K3.2011) at each velocity point according to:

$$d_{PTB, KCRV} = K_{PTB} - KCRV \quad (4)$$

with the uncertainty of the deviation at 95 % level of confidence:

$$U(d_{PTB, KCRV}) = 2 \times u(d) \quad \text{and} \quad u(d) = \sqrt{u^2(K) - u^2(KCRV)} \quad (5)$$

(see final report CCM.FF-K3.2011, table 6 and 7)

and the VNIIM deviation from PTB:

$$d_{VNIIM, PTB} = K_{VNIIM} - K_{PTB} \quad (6)$$

resulting in:

$$d_{VNIIM, KCRV} = d_{PTB, KCRV} + d_{VNIIM, PTB} \quad (7)$$

with:

$$U(d_{VNIIM, KCRV}) = \sqrt{U^2(d_{PTB, KCRV}) + U^2(d_{VNIIM})} \quad (8)$$

and:

$$U(d_{VNIIM}) = U(K_{VNIIM})_{PC} \quad \text{according to (3)} \quad (9)$$

Taking the key comparison result KCRV(CCM.FF-K3.2011) values for PTB, the bilateral comparison results from VNIIM and considering that $U(d_{VNIIM;PTB}) = U_{VNIIM, "Pilot calculation"}$ including the transfer standard stability the normalized error E_n expressed as

$$E_n = \left| \frac{d_{VNIIM, KCRV}}{U(d_{VNIIM, KCRV})} \right| \quad (10)$$

describes the degree of equivalence of VNIIM related to the KCRV. The results are considered as consistent with the KCRV if $E_n \leq 1$.

7.3.1. Ultrasonic anemometer

The degree of equivalence with respect to the KCRV of CCM.FF-K3.2011 at each velocity for the ultrasonic anemometer is shown in Table 12.

Table 12 – Degree of equivalence of PTB and VNIIM with respect to the KCRV

AVERAGE DATA											
US											
Nominal air speed V_{nom} [m/s]	KKCRV	$U(KKCRV)$	PTB		VNIIM	Calibration result V_{ref}/US	Calibration result V_{ref}/US				
			$d_{i,PTB,KCRV}$	$U(d_{i,PTB,KCRV})$	$U(d_{i,VNIIM})$	PTB	VNIIM	$d_{i,VNIIM,PTB}$	$d_{i,VNIIM,KCRV}$	$U(d_{i,VNIIM,KCRV})$	$E_{i,VNIIM,KCRV}$
0,5	1,0253	0,0103	-0,0051	0,0204	0,0232	1,0201	1,0143	-0,0058	-0,0109	0,0309	0,35
1,0	1,0099	0,0056	-0,0023	0,0120	0,0142	1,0076	1,0049	-0,0027	-0,0050	0,0186	0,27
2,0	1,0018	0,0046	-0,0088	0,0106	0,0125	0,9930	0,9983	0,0053	-0,0036	0,0164	0,22
5,0	0,9890	0,0024	-0,0034	0,0046	0,0065	0,9855	0,9854	-0,0001	-0,0035	0,0080	0,44
10,0	0,9871	0,0022	-0,0018	0,0042	0,0061	0,9854	0,9853	0,0000	-0,0018	0,0074	0,24
15,0	0,9881	0,0022	-0,0008	0,0041	0,0059	0,9873	0,9884	0,0011	0,0003	0,0072	0,04
20,0	0,9890	0,0022	-0,0004	0,0040	0,0058	0,9886	0,9864	-0,0022	-0,0026	0,0071	0,36
30,0	0,9878	0,0023	0,0009	0,0039	0,0058	0,9887	0,9852	-0,0036	-0,0027	0,0069	0,38
40,0	0,9895	0,0025	0,0000	0,0037	0,0057	0,9894	0,9875	-0,0020	-0,0020	0,0068	0,29

7.3.2. Laser Doppler anemometer

The degree of equivalence with respect to the KCRV of CCM.FF-K3.2011 at each velocity for the laser Doppler anemometer is shown in Table 13.

Table 13 – Degree of equivalence of PTB and VNIIM with respect to the KCRV

AVERAGE DATA											
LDA											
Nominal air speed V_{nom} [m/s]	KKCRV	$U(KKCRV)$	PTB		VNIIM	Calibration result V_{ref}/V_{LDA}	Calibration result V_{ref}/V_{LDA}				
			$d_{i,PTB,KCRV}$	$U(d_{i,PTB,KCRV})$	$U(d_{i,VNIIM})$	PTB	VNIIM	$d_{i,VNIIM,PTB}$	$d_{i,VNIIM,KCRV}$	$U(d_{i,VNIIM,KCRV})$	$E_{i,VNIIM,KCRV}$
0,5	0,9993	0,0034	-0,0003	0,0132	0,0150	0,9990	0,9890	-0,0100	-0,0103	0,0200	0,51
1,0	1,0000	0,0032	0,0030	0,0079	0,0101	1,0030	0,9959	-0,0071	-0,0041	0,0128	0,32
2,0	1,0013	0,0024	-0,0002	0,0055	0,0075	1,0011	0,9994	-0,0017	-0,0019	0,0093	0,20
5,0	1,0006	0,0018	0,0021	0,0041	0,0060	1,0027	0,9977	-0,0050	-0,0029	0,0073	0,40
10,0	1,0016	0,0017	0,0017	0,0036	0,0055	1,0033	1,0003	-0,0031	-0,0013	0,0066	0,20
15,0	1,0016	0,0018	0,0018	0,0034	0,0053	1,0033	0,9991	-0,0042	-0,0024	0,0063	0,39
20,0	1,0016	0,0017	0,0017	0,0034	0,0053	1,0032	1,0010	-0,0022	-0,0006	0,0062	0,09
30,0	1,0012	0,0019	0,0014	0,0032	0,0052	1,0026	0,9980	-0,0046	-0,0032	0,0061	0,53
40,0	1,0009	0,0019	0,0012	0,0031	0,0051	1,0021	0,9982	-0,0039	-0,0027	0,0060	0,46

7.4. Discussion

As both transfer standards - the ultrasonic anemometer and the laser Doppler anemometer - had shown a high stability during the term of both key comparisons CCM.FF-K3.2011 and CCM.FF-K3.2011.1, the comparison results of PTB were taken from CCM.FF-K3.2011 to allow a direct linkage of the VNIIM results to the KCRV-(CCM.FF-K3.2011)-values.

The resulting E_n -values according to (10) show that all VNIIM results are consistent to the KCRV-values.

8. OPTIONAL LDA CALIBRATION WITH A PRIMARY STANDARD

Optionally, a calibration of the LDA with a primary standard was proposed but was not subject of the bilateral key comparison CCM.FF-K3.2011.1.

9. SUMMARY AND CONCLUSIONS

The bilateral key comparison CCM.FF-K3.2011.1 between VNIIM and PTB followed up the CCM.FF-K3.2011 key comparison and its protocol with identical transfer standards. As the stability of the transfer standards has been proven by measurements at PTB before and after the bilateral comparison and the data during the key comparison, a direct linkage between the VNIIM-results and the key comparison reference values via PTB's data from the key comparison was possible.

The VNIIM data for both transfer standards and all velocity values are consistent with the KCRV of the CCM.FF-K3.2011.

Nine institutes took part in the key comparison CCM.FF-K3-2011 for air speed measurement. Two transfer standards were used. The first one was an ultrasonic anemometer similar to the one used during the first run in 2005. The second one was a laser Doppler anemometer, known as the best transfer standard in the field which had already shown its interest during the EURAMET comparison 827.

The following table 14 checks the compliance of the results obtained by each participating laboratory to its claimed CMCs.

Table 44 – Comparison of the results with the declared CMCs for the calibration of an anemometer

Country NMI	Range as declared in CMCs tables	Expanded uncertainty	Result
Germany PTB	0.5 m/s to 40 m/s	(0.005 m/s + 0.0035v), v speed in m/s	In accordance
Russian Federation VNIIM	0.5 m/s to 25 m/s	0.5 %	In accordance
	10 m/s to 100 m/s	0.55 % to 1.0 %	In accordance

10. NOMENCLATURE

V_{ref}	Reference air speed measurement (m/s)
$V_{ts} (V_{UA}, V_{LDA})$	Transfer standard (Ultrasonic anemometer, Laser Doppler anemometer) measurement (m/s)
K	Ratio between the reference air speed and the transfer standard measurements (-)
$KCRV$	Comparison reference value (-)
$u(X)$	Standard uncertainty of the mesurand X
$U(X)$	Expanded uncertainty of the mesurand X with approximately 95% confidence level
d	Degree of equivalence = $K - KCRV$ (-)
E_n	Standardized degree of equivalence between a lab and the key comparison reference value, = $ d/2u(d) $

11. REFERENCES

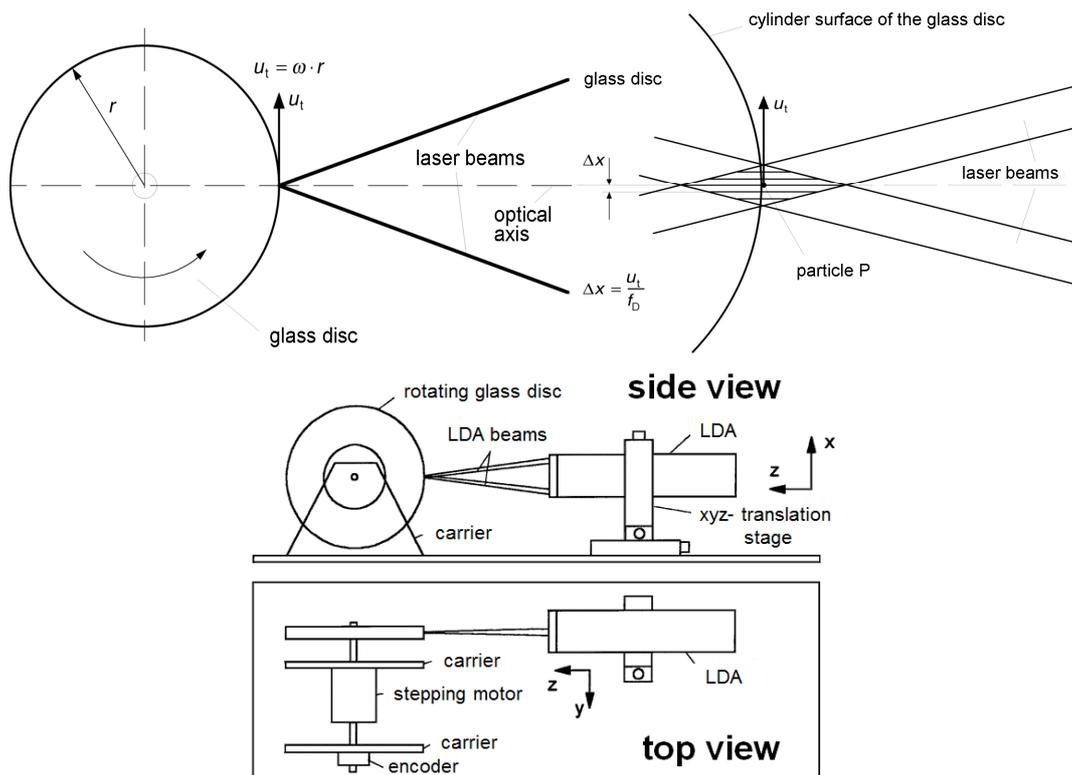
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APPENDIX – DESCRIPTION OF THE FACILITIES

PTB

PTB velocity primary standard for LDA

At PTB's LDA calibration facility the velocity of a set of single scattering particles adhered to the lateral surface of a polished glass cylinder represents the "standard" velocity u_t which is given by the angular speed ω and the radius r of a rotating glass disc ($2r = 184 \text{ mm}$).



Principle: LDA calibration via particle velocities u_t generated by a rotating glass disc.

Calibration results are provided in two different formats:

- as LDA measuring head specific calibration constant represented by the fringe spacing,
- as LDA calibration factor derived from the standard velocity of the rotating disc facility and the indicated LDA velocity of the associated LDA signal processing unit.

with relative expanded uncertainties ($k = 2$) for the calibration (best available DUT) according to the CMCs:

Flow speed. Laser Doppler Velocimeter (LDV), 0.1 m/s to 15 m/s

Relative expanded uncertainty ($k = 2$, level of confidence 95%) in %: 0.1

NMI service identifier: DE39

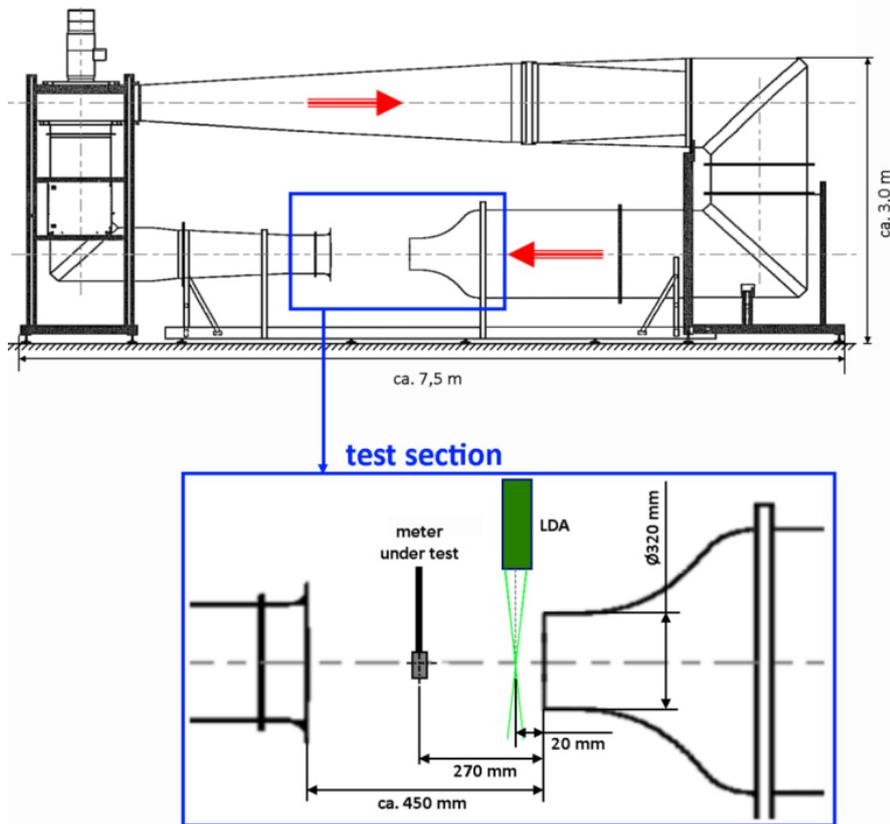
Flow speed. Laser Doppler Velocimeter (LDV), 1 μm to 15 μm

Relative expanded uncertainty ($k = 2$, level of confidence 95%) in %: 0.05

NMI service identifier: DE42

PTB calibration facility for air speed anemometers

Calibrations of air speed anemometers according to the PTB service identifier DE41 are performed in the Göttingen type wind tunnel at PTB. The reference velocity v_{ref} is determined by the use of a Laser Doppler Anemometer as reference standard and represents the velocity at the position of the probe in the measurement section of the wind tunnel (see figure and table below).



Setup of the Göttingen type wind tunnel at PTB

Data for anemometer's calibration in the Göttingen type wind tunnel at PTB

Type:	Göttingen, open test section
Range:	0.5, ..., 65 m/s
Uncertainty:	$(0.005 + 0.0035 \cdot U)$, U speed in m/s
Dimensions measuring section:	nozzle diameter: $\varnothing 320$ mm test section length: 450 mm
Reference:	LDA
Traceability:	PTB, rotating glass wheel surface for fringe calibration, frequency standard

Facility and uncertainty budget for the calibration of anemometers

Calibration of transfer standard – ultrasonic anemometer – has been performed by measuring the anemometer indicated speed and the VNIIM standard reading simultaneously. Measurements accomplished at aerodynamic facility: loop tube with open test section. Nozzle diameter is 700 mm, range 0.05 – 100 m/s. Means of air speed measuring:

- 0.1 – 20 m/s LDA
- 5 - 100 m/s Pitot static tube with differential manometer.

Distance between nozzle exit plane and ultrasonic anemometer sensors was 70 mm.

While using LDA air speed determined as

$$V_s = K_l * K_b * K_d * V_l, \text{ [m/s]} \quad (1)$$

K_l – LDA calibration factor

K_b – correction factor due to duct blockage

K_d – correction factor due to velocity distribution across the duct

V_l – air speed indicated by LDA, [m/s]

The relative uncertainty

$$\frac{u_c(V_s)}{V_s} = \left(\left(\frac{u(K_l)}{K_l} \right)^2 + \left(\frac{u(K_b)}{K_b} \right)^2 + \left(\frac{u(K_d)}{K_d} \right)^2 \right)^{1/2} \quad (2)$$

Expanded uncertainty sources and values

Sources		$u(X_i)/X_i, \%$
LDA calibration factor	$\left(\frac{u(K_l)}{K_l} \right)$	0.05
Correction factor due to duct blockage	$\left(\frac{u(K_b)}{K_b} \right)$	0.10
Correction factor due to velocity distribution across the duct	$\left(\frac{u(K_d)}{K_d} \right)$	0.25
Combined standard uncertainty	$\frac{u_c(V_s)}{V_s}$	0.27
	k	2
Expanded uncertainty		0.54

