



Final report

CCM.FF-K1.2015

Water flow: 30 m³/h ... 200 m³/h

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1 Introduction and purpose

The purpose of Key Comparison KC1 for water flow measurement (CCM.FF-K1.2015) was to support and prove the Calibration and Measurement Capabilities (CMC) of the participating National Metrology Institutes and Designated institutes as part of CIPM MRA.

The CMC-values of participating laboratories (Table 1) was evaluated by establishing a “Key Comparison Reference Value” (*KCRV*) and the Degree of Equivalence (E_N) between laboratories and *KCRV*.

In former versions, this comparison was labeled as CCM.FF-K1.2011. The official KCDB identifier was updated to **CCM.FF-K1.2015** (<http://kcdb.bipm.org>).

The basic subject of the calibrations was to determine the **meter K-factor** of the transfer flowmeters. Depending on the operating principle of the used flowmeters, following meter-*K*-factors were the subject of measurements and had to be determined during calibrations:

Meter #1:

Turbine flowmeter - volume-related frequency output:
 K_v (pulses/unit volume)

Meter #2:

Coriolis flowmeter:

- a) mass-related frequency output:
 K_m (pulses/unit mass)
- b) volume-related frequency output:
 K_v (pulses/unit volume)

Notes:

- As discussed during meeting of WGFF / Lisbon 2019, within this report the Coriolis_{mass} output was analyzed as the main meter for calibration results. Coriolis_{volume} output was not considered for evaluation of CMC values, because this output was not an independent measurand compared to Coriolis_{Mass}. Both values were based on the same flow meter instrument, linked with an internal value conversion.
- NEL declared to withdraw from key comparison CCM.FF-K1.2015. The communication to pilot laboratory is attached on page 99.

Acknowledgements

We would like to thank all participants of the comparison for their support. This round robin would not be possible without all your help, discussions und organization. Our acknowledgements include all participated staff of the laboratories - scientists, technicians and administration.

Special thanks go to Sejong Chun from KRISS for supporting the Draft by additional analysis on Reynolds number in Section 10.4., as well to Tao Meng from NIM for data and analysis on turbine meter hysteresis in Section 6.7.

2 Participants and measurement schedule

Participant list and measurement schedule are presented in Table 1. After three years of preparation the comparison started officially in December 2015.

Table 1: Participant list and measurement periods of standard calibration program (day #1 until day #3 of Table 4) (* pilot laboratory). Additional calibrations at pilot laboratory are listed in Table 6 and Table 7.

NMI/DI	Country	RMO	Contact	Calibration period
PTB*	Germany	EURAMET	enrico.frahm@ptb.de	02.12. - 04.12.2015
NEL	UK	EURAMET	Chris.Mills@tuvsud.com	15.12. - 17.12.2015
VSL	Netherlands	EURAMET	fsmits@vsl.nl	13.01. - 15.01.2016
RISE	Sweden	EURAMET	Oliver.Buker@ri.se	24.02. – 26.02.2016
PTB*	Germany	EURAMET	enrico.frahm@ptb.de	13.04. – 15.04.2016
UME	Turkey	EURAMET	basak.akselli@tubitak.gov.tr	26.05. – 28.05.2016
PTB*	Germany	EURAMET	enrico.frahm@ptb.de	19.07. – 27.07.2016
NIST	USA	SIM/Noramet	losif.Shinder@nist.gov	28.09 – 29.09.2016
CENAM	Mexico	SIM/Noramet	rarias@cenam.mx	21.02. – 22.02.2017
PTB*	Germany	EURAMET	enrico.frahm@ptb.de	24.04. – 26.04.2017
ITRI	Chinese Taipei	APMP	ctyang@itri.org.tw	27.06. – 29.06.2017
NIM	P.R. China	APMP	mengt@nim.ac.cn	29.08. – 31.08.2017
PTB*	Germany	EURAMET	enrico.frahm@ptb.de	24.10. – 06.11.2017
NMIJ/AIST	Japan	APMP	furuichi.noriyuki@aist.go.jp	05.12. – 07.12.2017
KRISS	Korea	APMP	sjchun@kriss.re.kr	24.01. – 02.02.2018
PTB*	Germany	EURAMET	enrico.frahm@ptb.de	03.04. – 12.04.2018

3 Description of the transfer standard

3.1 Transfer meter setup

The transfer meter setup (Figure 1) consisted a turbine flowmeter (Figure 2) at the inflow and a Coriolis flowmeter (Figure 3) at the outflow. The technical details of the meters are listed in Table 2 and Table 3. For flow conditioning, tube bundles were installed before and after turbine meter. Beside the two transfer flowmeters, all additional items were provided by the pilot laboratory:

- Pipework for meter installation (Figure 4)
- Cables for connecting transfer meters and the auxiliary devices to electronic boxes
- Electronic boxes 1 and 2 (Figure 5).

To provide optimum reproducibility conditions, the flowmeters and the inter-connecting pipework were equipped with pin-in-hole alignment capabilities. All elements of pipework were manufactured in stainless steel.

In addition to the used flowmeters, auxiliary measurands for diagnostic purposes were included in the transfer meter setup:

- Water density (based on a signal delivered by the Coriolis flowmeter)
- Fluid temperature by temperature transmitter
- Fluid pressure by pressure transmitter
- Pressure drop across the turbine meter by differential pressure transmitter

A detailed description of the setup is given in the Technical Protocol of KC1 [1].

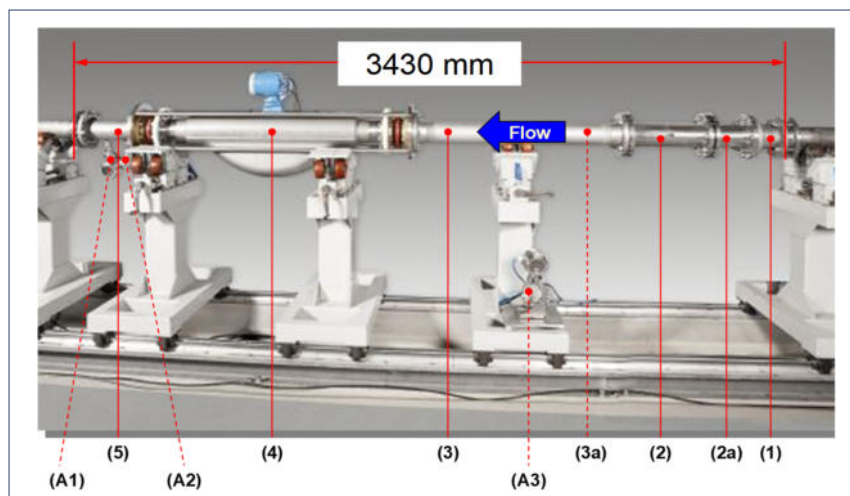


Figure 1: Transfer meter setup and pipework - Sample installation at pilot laboratory

- | | |
|--|--|
| (1) Inlet pipe section | (2) Turbine meter |
| (2a) Tube-bundle flow conditioner dedicated to the turbine | |
| (3) Connecting pipe section with | (3a) Integrated tube-bundle flow conditioner |
| (4) Coriolis flowmeter | (5) Outlet pipe section |

Auxiliary devices:

- (A1) Pressure transmitter
- (A2) Temperature transmitter
- (A3) Differential pressure transmitter

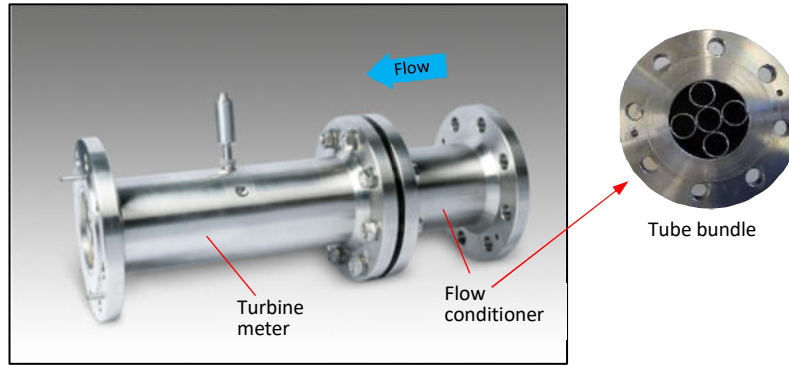


Figure 2: Transfer meter #1 - Turbine meter, DN100 mm

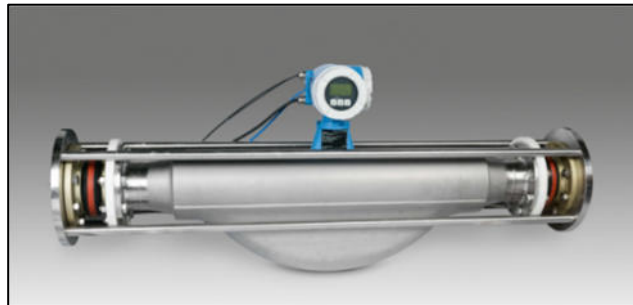


Figure 3: Transfer meter #2 - Coriolis flowmeter, DN100 mm

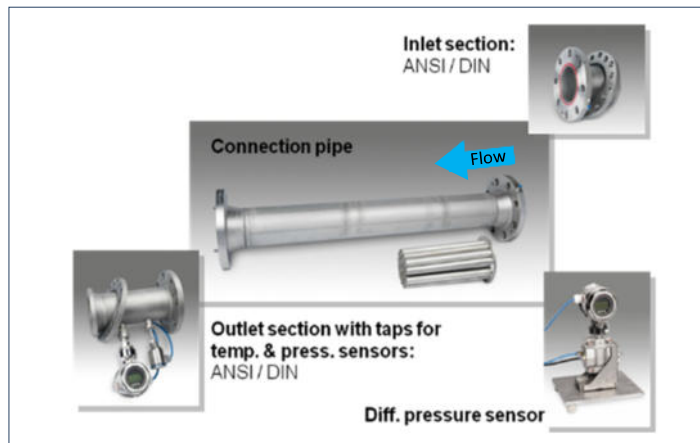


Figure 4: Transfer setup – pipework

Table 2: Transfer meter #1 - Turbine flowmeter (Figure 2)

Manufacturer:	KEM Küppers Elektromechanik GmbH	Germany
Type:	HM 100.71.FDB40-TS15-P	
Serial No.:	010995521	
Pipe size:	DN100	Nominal: 100 mm
Signal pick-up:	Type: VTE*/P-Ex Carrier-frequency pulse amplifier Serial No.: 02497623	Signal voltage: ca. 24 V
Output signal:	Frequency	(0 Hz) ... 450 Hz (at 240 m ³ /h)
	Nominal meter <i>K</i> -factor: $K_{V,nom}$	6.633 pulses/L
Additional equipment:	Tube-bundle flow conditioner	Permanently installed at the inflow to meter
Special provision:	Pin-in-hole alignment	Steel pins located in precision holes on both ends

Table 3: Transfer meter #2 - Coriolis flowmeter (Figure 3)

Manufacturer:	ENDRESS + HAUSER	Switzerland
Type:	Proline Promass 83 F	
Serial No.:	D702C102000	
Pipe size:	DN100	Nominal: 100 mm
Signal output #1:	Mass-flowrate related: frequency	0 kHz ... 10 kHz
	Nominal meter K -factor: $K_{m,nom}$	100 pulses/kg
Signal output #2:	Volume-flowrate related: frequency	0 kHz ... 10 kHz
	Nominal meter K -factor: $K_{v,nom}$	100 pulses/L
Signal output #3:	Fluid density: current signal	4 mA ... 20 mA
Communication line:	Reading parameters from flow meter	HART protocol (current output)
Special adoptions:	A cage-like meter extension in order to isolate the meter from external forces and torques	rubber damping elements included
Special provision:	Pin-in-hole alignment	Steel pins located in precision holes on both ends

3.2 Additional data logging - Electronic boxes 1 and 2

For the reported KC1 an additional datalogging system was designed. Beside standard impulse logging of the laboratory, an electronic device was provided by the pilot laboratory for a separate and independent data recording. Depending on electrical compatibility, the transfer setup and the auxiliary devices were connected by the laboratories, either to electronic box 1 or box 2.

Basically, electric pulses from transfer meters and additional process parameters, measured by the auxiliary devices (chapter 3.1), were logged by electronic box 1 (Figure 5a and Figure 6a). Also, power supply of the measurement instruments was provided by the box. The detailed use of electronic box 1 is described in the Technical Protocol of KC1 [1].

Due to the diverse conditions of the laboratories (e.g. electrical compatibility) it was necessary to provide an alternative junction device. For the scenario, if the use of electronic box 1 did not operate in the intended function (power supply of the transfer meters and data logging), electronic box 2 (Figure 5b and Figure 6b) had to be used. In that case, power supply of both flow meters and auto zero setting of Coriolis meter were provided by electronic box 2. A detailed description of the box is also given in the Technical Protocol [1].

Both boxes were developed as parallel working systems, which do not affect the standard pulse count recording of the laboratories. Tests at pilot laboratory verified the use of both boxes. Negative influences of the electronics or a significant deviation in pulse counting between the use of both boxes were not detected (Figure 7).

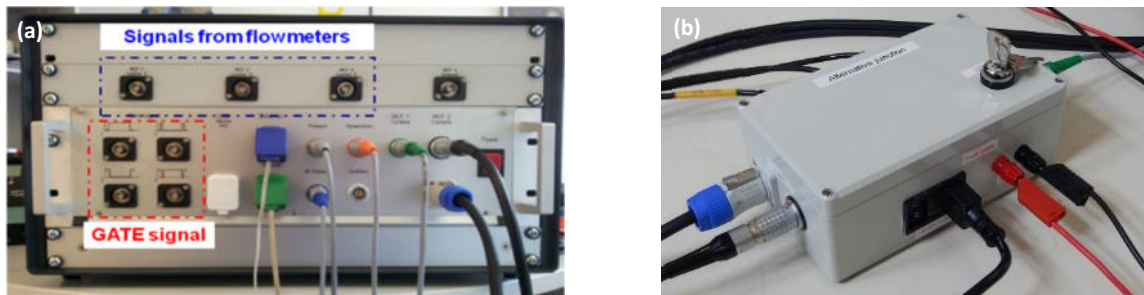


Figure 5: (a) Front side of electronic box 1
 (b) Electronic box 2 (alternative junction) for power supply of both transfer meters and auto zero setting for Coriolis meter

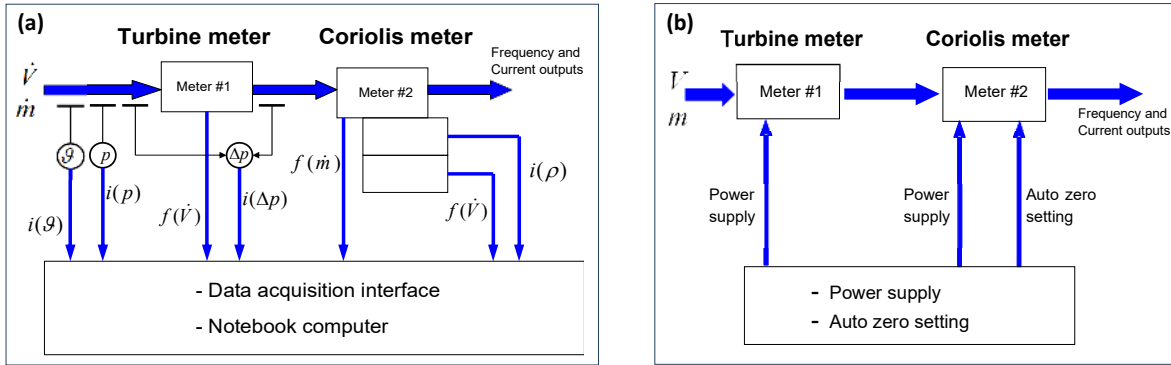


Figure 6: (a) Electronic Box 1 - Signal acquisition
(b) Electronic Box 2 - Power supply and function of auto zero setting

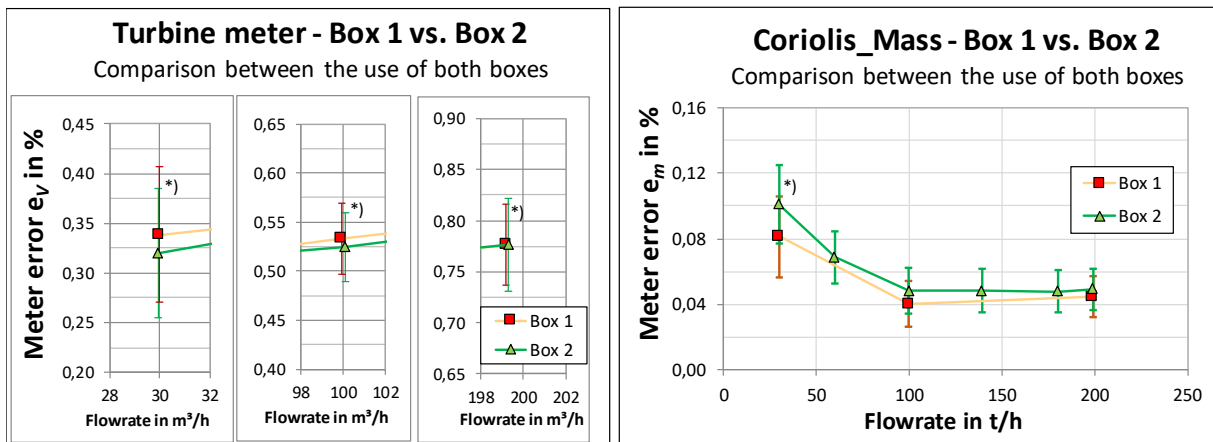


Figure 7: Meter error of repeated calibrations of turbine meter and Coriolis_Mass at pilot laboratory – Calibrations for using electronic box 1 and box 2 in 08/2016. *) are representing uncertainties $u_{x,i}$

4 Measurement program

4.1 Calibration program at participating laboratories

The objective of the measurement program was to verify the CMC entries of the participating laboratories. Therefore, it was necessary for all laboratories to calibrate the setup under comparable measurement conditions. All participants were asked to calibrate the transfer setup as far as possible under the following KC1 reference conditions.

KC1 reference conditions:

Fluid temperature: 20 °C

Line pressure: 3 bar (measured as positive back pressure after Coriolis meter)

Nominal flowrates: listed in Table 4

Setup: using the complete KC1 setup (Figure 1).

Table 4: Main tasks and flowrates of calibration days in participating laboratories as defined in [1]

Calibration day	Main task	Preparations before calibration	Auto zero setting at Coriolis meter		Repeated measurements	Nominal flowrate in m ³ /h	Post-processing
Day #1	Lab-to-lab reproducibility	Installation of transfer meters	yes		5	30, 60, 100, 140, 180, 200	Transfer package remains in calibration line
Day #2	Main calibration of KC1 and Day-to-day reproducibility	-	no		5	30, 60, 100, 140, 180, 200	Transfer package remains in calibration line
Day #3	Repeatability at selected flowrates	-	no		10	30, 100, 200	Transfer package is removed from calibration line

4.2 Methods used for calibration in participating laboratories

Each laboratory had to calibrate the setup by using their standard calibration method, which was subjected to the CMC entry (Table 5). Each laboratory provided the pilot laboratory with a description of the calibration procedure and an overview to the used calibration rig (Chapter 10.1.) All laboratories had an independent traceability in realization of their standards.

Table 5: Participating laboratories, calibration methods and CMC-values within the range of KC1 flowrates

NMI/DI	Country	Calibration method and reference	CMC Water CIPM MRA (k = 2)	
			U(Mass) in %	U(Volume) in %
NEL	United Kingdom	Gravimetric / flying-start-stop	0.100	0.100
VSL	The Netherlands	Gravimetric / standing-start-stop	0.030 (m ≤ 30 t/h) 0.015 (m > 30 t/h)	0.045
RISE	Sweden	Volumetric Prover/ flying-start-stop	0.080	0.060
UME	Turkey	Gravimetric / flying-start-stop	0.070	0.070
PTB	Germany	Gravimetric / flying-start-stop	0.020	0.020
NIST	USA	Gravimetric / flying-start-stop	0.030	0.030
CENAM	Mexico	Gravimetric / flying-start-stop	0.030	0.038
ITRI	Chinese Taipei	Gravimetric / flying-start-stop	0.040	0.040
NIM	P.R.O. China	Gravimetric / flying-start-stop	0.050	0.050
NMIJ/AIST	Japan	Gravimetric / flying-start-stop	0.042	0.042
KRISS	Korea	Gravimetric / flying-start-stop	0.060	0.060

4.3 Meter characterisation at pilot laboratory

The transfer setup was subjected to extensive characterisation measurements at pilot laboratory (Table 6 and Table 7). These calibrations were made under clearly defined conditions, which were basically derived from KC1 reference conditions (Chapter 4.1). The goal of the characterisation measurements was to analyze the impact of the following parameters to transfer meter setup: fluid temperature, line pressure, reproducibility and changing inflow conditions. The results aimed in a detailed knowledge about the transfer meter uncertainties u_{TS} .

During meter characterisation, the influences of different inflow conditions to meter setup were evaluated. In order to simulate a wide range of real inflow conditions, the setup was calibrated with several flow disturber (Figure 8) and changing inflow lengths (Figure 9). The calibrations were made under KC1 reference conditions, as listed in chapter 4.1.

Table 6: Extended calibration days at pilot laboratory

Calibration day	Main Task	Preparations before calibration	Auto zero setting at Coriolis meter	Repeated measurements	Nominal flow-rate in m ³ /h	Post-processing	Measurement periods at pilot laboratory
Day #4	Laboratory-internal reproducibility (I)	Installation of transfer meters	yes	5	30 60 100 140 180 200	Transfer package was removed from calibration line after each calibration day	25.07.2016 - 27.07.2016
Day #5	Laboratory-internal reproducibility (II)	Installation of transfer meters	yes		02.11.2017 - 06.11.2017		
Day #6	Day-to-day reproducibility (III)	-	no		09.04.2018 - 12.04.2018		

Table 7: Characterisation measurements at pilot laboratory

Task of calibrations	Nominal flowrate in m ³ /h	Temperature in °C	Line pressure in bar	Repeated measurements	Measurement periods at pilot laboratory
Temperature dependency	30, 60, 100, 140, 180	10, 15, 20, 25, 30	3	5	13.03.2013 - 02.04.2013
	30, 60, 100, 140, 180, 200	15, 20, 25	3	5	13.01.2015 - 19.01.2015
	30, 60, 100, 140, 180, 200	10, 20, 30	3	5	22.02.2019 - 01.03.2019
Pressure dependency	30, 60, 100, 140, 180	20	2, 3, 4	5	02.04.2013 - 04.04.2013
	30, 60, 100, 140, 180, 200	20	2, 3, 4	5	13.04.2018 - 18.04.2018
Inflow conditions	30, 100, 200	20	3	5	11.03.2019 - 29.03.2019

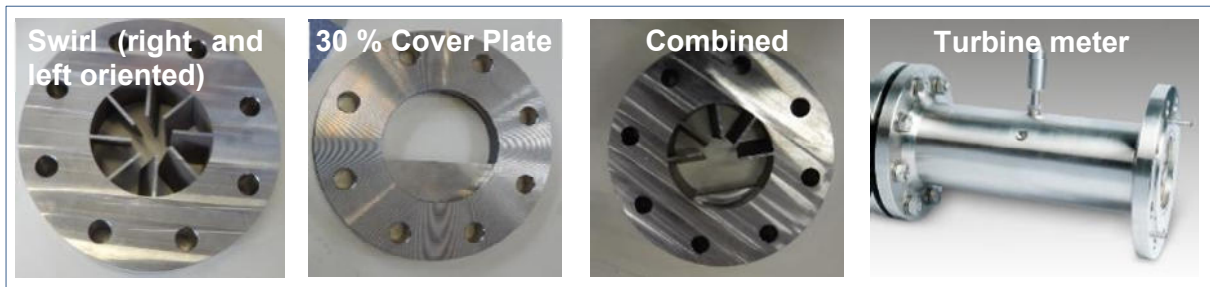


Figure 8: Used flow disturber for meter characterisation - inner pipe diameter: 100 mm

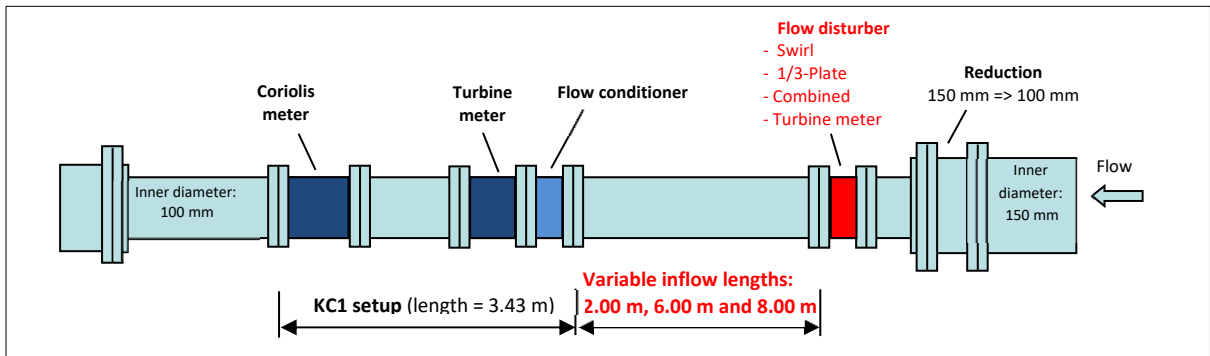


Figure 9: Calibration setup for meter characterisation – influences of different inflow lengths to transfer setup

5 Data calculation and evaluation criteria

5.1 Meter K -factor and temperature correction for final meter error x_i

According to the flowrates of Table 4, the meter K -factor was calculated for each calibration by using Equation (1) for turbine meter and, respectively, by Equation (2) for Coriolis meter.

$$K_V = \frac{N}{(V_{\text{ref}} \cdot 1000)} \quad (1)$$

$$K_m = \frac{N}{m_{\text{ref}}} \quad (2)$$

where	K_V	- K -factor of turbine meter (pulses/L)
	K_m	- K -factor of Coriolis meter (pulses/kg)
	N	- Counted number of pulses of the transfer meter (pulses)
	V_{ref}	- Volume, measured by the reference standard (m ³)
	m_{ref}	- Mass, measured by the reference standard (kg)

The relative measurement error e was calculated for each K -factor by:

$$e_V = \frac{K_V - K_{V,\text{nom}}}{K_{V,\text{nom}}} \cdot 100 \% \quad (3)$$

$$e_m = \frac{K_m - K_{m,\text{nom}}}{K_{m,\text{nom}}} \cdot 100 \% \quad (4)$$

where	e_V	- Relative measurement error of turbine meter (%)
	e_m	- Relative measurement error of Coriolis meter (%)
	$K_{V,\text{nom}}$	- Nominal K -factor of turbine meter (pulses/L)
	$K_{m,\text{nom}}$	- Nominal K -factor of Coriolis mass (pulses/kg)

Both transfer meters were characterised by a systematic temperature dependency in meter error (Section 6.3). **All reported meter error of participating laboratories were corrected by applying Equation (22) until Equation (25) and Table 13**, to aim a temperature corrected meter error $e_{V,\text{cor}}$ for volume and $e_{m,\text{cor}}$ for mass.

For final evaluation of E_N , a mean meter error (x_i) was calculated separately for each laboratory, transfer meter and flowrate (Equation 5), **based on calibration results of day #1 and day #2** (Table 4).

$$x_i = \frac{\sum_{k=1}^n (e_{\text{cor},k})}{n} \quad (5)$$

where	x_i	- Temperature corrected meter error for E_N -value evaluation
	n	- Number of measurements at calibrated test point
	i	- Laboratory index

5.2 Uncertainty $u_{x,i}$ of reported and temperature corrected value x_i

As described in [2], [3] and [4], the uncertainty of reported value x_i includes uncertainties introduced by the participant's flow reference ($u_{\text{base},i}$), by transfer meter (u_{TS}) and by repeatability of the reported value (Equation 6). The used input parameter of $u_{\text{base},i}$ do represent the CMC values of Table 5 which were under evaluation during this comparison. Uncertainty calculations of u_{TS} were based on Equation (18), for Turbine meter, respectively for Coriolis meter, on Equation (19). Final values of u_{TS}

are presented in Table 8 and Table 9. The term $\frac{s}{\sqrt{n}}$ (Equation 6) represents the repeatability of measurements made in the participants laboratory [3], based on calibration results of day #1 and day #2 (Table 4).

$$u_{x,i} = \sqrt{u_{\text{base},i}^2 + u_{\text{comp}}^2} = \sqrt{u_{\text{base},i}^2 + u_{\text{TS}}^2 + \frac{s^2}{n}} \quad (6)$$

where

- $u_{x,i}$ - Uncertainty of reported and temperature corrected meter error (%)
- $u_{\text{base},i}$ - Uncertainty of laboratory reference, here it is equal to CMC_i (%)
- u_{comp} - Uncertainty of transfer meter measurements (%)
- s - Standard deviation of the mean of measurements at one flowrate point (%)
- n - Number of calibrations at one flowrate point (-)

All values of u are valid for $k = 1$.

5.3 Determination of Key Comparison reference value (KCRV) and its uncertainty

The Key Comparison reference value was calculated at each flowrate of Table 4, following the procedure A of [5]. All reported calibration results (day #1 and day #2) were used for the determination of KCRV and its uncertainty, because all participating laboratories declared their independent traceability chains to SI. The determination of KCRV included a consistency check according to [6].

The reference value y was calculated as weighted mean error of the participating laboratories, including standard uncertainties $u(x_i)$ of the measurements as the weights:

$$y = \frac{\left(\frac{x_1}{u_{x,1}^2} + \frac{x_2}{u_{x,2}^2} + \dots + \frac{x_i}{u_{x,i}^2} \right)}{\left(\frac{1}{u_{x,1}^2} + \frac{1}{u_{x,2}^2} + \dots + \frac{1}{u_{x,i}^2} \right)} \quad (7)$$

where y - Reference value of the comparison (%)

The standard uncertainty u_y is given with:

$$\frac{1}{u_y^2} = \frac{1}{u_{x,1}^2} + \frac{1}{u_{x,2}^2} + \dots + \frac{1}{u_{x,i}^2} \quad (8)$$

where u_y - Standard uncertainty of y with $k = 1$ (%)

The expanded uncertainty of y was calculated with:

$$U(y) = 2 \cdot u_y \quad (9)$$

where $U(y)$ - Expanded uncertainty of y with $k = 2$ (%)

Based on [5] and [6], at each flow rate the chi-squared test was applied for a consistency check of the laboratory results. The chi-squared value was calculated with:

$$X_{\text{obs}}^2 = \frac{(x_1 - y)^2}{u_{x,1}^2} + \frac{(x_2 - y)^2}{u_{x,2}^2} + \dots + \frac{(x_i - y)^2}{u_{x,i}^2} \quad (10)$$

where X_{obs}^2 - Observed chi-squared value

The degrees of freedom ν were estimated with:

$$\nu = n_i - 1 \quad (11)$$

where n_i - number of evaluated laboratories

For data evaluation the CHINV(0.05; ν) function of MS Excel was used. The consistency check failed if CHINV(0.05; ν) gives values < than X_{obs}^2 .

$$Pr\{X_{\nu}^2 > X_{obs}^2\} < 0.05 \quad (12)$$

where X_{ν}^2 - Chi-squared test value

If consistency check of Equation (12) passed, y was accepted as the Key Comparison Reference value x_{KCRV} and $U(y)$ was accepted as the expanded uncertainty $U(x_{KCRV})$.

If the test of Equation (12) failed, the laboratory with highest value of $(x_i - y)^2 / u_{x,i}^2$ would be excluded for the next evaluation round. New values of y , $U(y)$ and X_{obs}^2 were calculated and the consistency check of Equation (12) was repeated.

5.4 Determination of differences „Lab to KCRV“ as degree of equivalence (DoE)

Differences between laboratories results (x_i) and KCRV (x_{KCRV}) were calculated in accordance with Equation (13), separately for each flowmeter and flowrate. The results give the degree of equivalence (DoE) of each laboratory.

$$d_i = x_i - x_{KCRV} \quad (13)$$

where d_i - Degree of equivalence (DoE) for each laboratory i in %
 x_{KCRV} - Key Comparison Reference value in %

Based on differences d_i , the normalized Degree of Equivalence $E_{N,i}$ was calculated for each laboratory and flowrate with:

$$E_{N,i} = \left| \frac{d_i}{U(d_i)} \right| \quad (14)$$

where $E_{N,i}$ - Normalized Degree of Equivalence

The calculated differences of d_i are followed by specific uncertainties, which can be basically analyzed by a consideration of the general problem of the difference between two values x_1 and x_2 . The pure propagation of the uncertainty (with $k = 1$) is given by Equation (15). Finally, the uncertainty of the difference is the quadratic sum of the uncertainties of u_1 and u_2 and subtracting twice the covariance between the two input values.

$$u_{x_1-x_2}^2 = \begin{bmatrix} \frac{\partial(x_1 - x_2)}{\partial x_1} & \frac{\partial(x_1 - x_2)}{\partial x_2} \end{bmatrix} \begin{pmatrix} u_1^2 & cov \\ cov & u_2^2 \end{pmatrix} \begin{bmatrix} \frac{\partial(x_1 - x_2)}{\partial x_1} \\ \frac{\partial(x_1 - x_2)}{\partial x_2} \end{bmatrix} = u_1^2 + u_2^2 - 2 \cdot cov \quad (15)$$

The value of covariance is identical to the value of measurement uncertainty related to KCRV for the independent participating labs which took part in the KCRV determination. Based on Equation (15), the extended uncertainty of d_i was calculated with Equation (16) for laboratories with contribution to

the KCRV. Participating labs, which were excluded from the KCRV determination, do not have any interference. In that case the value of $U(d_i)$ would be calculated according to equation (17).

$$U(d_i) = 2 \cdot \sqrt{u_{x,i}^2 + u_{KCRV}^2 - 2 \cdot u_{KCRV}^2} = 2 \cdot \sqrt{u_{x,i}^2 - u_{KCRV}^2} \quad (16)$$

$$U(d_i) = 2 \cdot \sqrt{u_{x,i}^2 + u_{KCRV}^2} \quad (17)$$

Note: An evaluation of “Lab to Lab differences” is not included in this report, because: “The 14th CCM meeting (February, 2013) agreed that pair wise degrees of equivalence should no longer be published in the KCDB. Information on pair-wise degrees of equivalence published in KC reports should be limited to the equations needed to calculate them, with the addition of any information on correlations that may be necessary to estimate them accurately.” [14th CCM meeting in February 2013]

5.5 Evaluation of comparison data

For final data evaluation and decision table the following criteria were used - based on [3], [4] and [5]:

- **Chi-squared test**
Data evaluation and consistency check, based on Equations (10) to Equations (12)
- The participant **passes the comparison if $E_{N,i} \leq 1.0$ and $u_{\text{comp}}/u_{\text{base},i} \leq 2$**
The results of participating laboratory i agrees within 95 % confidence level uncertainty expectations with the *KCRV* ($k = 2$).
- The participant passes the comparison at “**warning level**” if **$1.0 < E_{N,i} \leq 1.2$ and $u_{\text{comp}}/u_{\text{base},i} \leq 2$**
- The participant **fails the comparison if $E_{N,i} \leq 1.2$ and $u_{\text{comp}}/u_{\text{base},i} > 2$**
The results are inconclusive, because the transfer meter did not show sufficient low uncertainties to discern lab to *KCRV* below certain level. The transfer meter is not suitable for a confirmation of the declared CMC values.
- The participant **fails the comparison if $E_{N,i} > 1.2$**
The results do indicate that the agreement is outside of uncertainty expectations.

5.6 Alternative evaluation of the comparison data - based on Reynolds number

Especially for Turbine meter, comparison analysis based on Reynolds number are commonly practiced. For this report an additional data analysis was submitted by KRISS institute in January 2021. Procedure and results are presented in Appendix 10.4.

6 Laboratory conditions, transfer meter characteristics and meter uncertainties

In accordance to the WGFF recommendation for comparison calculations [3], the standard uncertainty u_{TS} of the transfer meter is the root-sum-of-squares (RSS) of several transfer meter characteristics. For this comparison the considered meter characteristics and input uncertainties of turbine meter are listed in Equation (18), for Coriolis meter in Equation (19). The final values of u_{TS} were calculated separately for each flowrate (Table 8 and Table 9).

Note: The uncertainties of u_{TS} are specified and valid for the presented comparison under the given measurement conditions. The values of u_{TS} may change if the setup or calibration conditions do deviate to this comparison.

$$\text{Turbine meter: } u_{TS} = \sqrt{u_{\text{drift}}^2 + u_{\text{reprod}}^2 + u_{\text{temp}}^2 + u_{\text{pres}}^2 + u_{\text{flow}}^2 + u_{\text{inflow}}^2 + u_{\text{hyst}}^2} \quad (18)$$

$$\text{Coriolis}_{\text{Mass}}: u_{TS} = \sqrt{u_{\text{drift}}^2 + u_{\text{reprod}}^2 + u_{\text{temp}}^2 + u_{\text{pres}}^2 + u_{\text{flow}}^2} \quad (19)$$

where	u_{TS}	- Uncertainty of transfer meter (%)
	u_{drift}	- Uncertainty due to drift of transfer meter (%)
	u_{reprod}	- Uncertainty due to reproducibility characteristics of transfer meter (%)
	u_{temp}	- Uncertainty caused by temperature characteristics of transfer meter (%)
	u_{pres}	- Uncertainty caused by pressure characteristics of transfer meter (%)
	u_{flow}	- Uncertainty due to sensitivity of transfer meter to instable flow conditions (%)
	u_{inflow}	- Uncertainty due to sensitivity of turbine meter to different inflow conditions (%)
	u_{hyst}	- Uncertainty due to hysteresis effect (%)

All values of u are valid for $k = 1$.

Table 8: Final values of meter uncertainties u_{TS} for turbine meter (with $k = 1$)

Nominal flowrate in m ³ /h	Meter uncertainty u_{TS}		Input uncertainties for u_{TS}						
	Turbine meter considering u_{inflow} in %	Turbine meter without u_{inflow} in %	u_{drift} in %	u_{reprod} in %	u_{temp} in %	u_{pres} in %	u_{flow} in %	u_{inflow} in %	u_{hyst}
30	0.123	0.077	0.008	0.011	0.012	0.012	0.003	0.096	0.074
60	0.106	0.043	0.006	0.003	0.005	0.012	0.003	0.096	0.041
100	0.102	0.032	0.004	0.005	0.009	0.012	0.003	0.096	0.028
140	0.099	0.024	0.005	0.011	0.010	0.012	0.003	0.096	0.015
180	0.098	0.017	0.004	0.011	0.003	0.012	0.003	0.096	0.001
200	0.099	0.021	0.005	0.010	0.002	0.012	0.003	0.096	0.013

Table 9: Final values of meter uncertainties u_{TS} for Coriolis_Mass (with $k = 1$)

Nominal flowrate in t/h	Meter uncertainty u_{TS}		Input uncertainties for u_{TS}				
	Coriolis_Mass in %		u_{drift} in %	u_{reprod} in %	u_{temp} in %	u_{pres} in %	u_{flow} in %
30	0.022		0.012	0.011	0.013	0.006	0.001
60	0.012		0.006	0.005	0.007	0.006	0.001
100	0.010		0.005	0.004	0.005	0.006	0.001
140	0.009		0.004	0.003	0.004	0.006	0.001
180	0.008		0.004	0.002	0.002	0.006	0.001
200	0.007		0.004	0.002	0.001	0.006	0.001

6.1 Drift of transfer meter - uncertainty u_{drift}

The uncertainty due to meter drift u_{drift} was quantified by performing repeated calibrations at pilot laboratory (Table 1 and Table 6), using the reference standard as described in Figure 1. For each calibration period a mean value was calculated (Figure 10 and Figure 11). The final values of u_{drift} (Table 10) were calculated by using Equation (20), separately for each flowmeter and flowrate.

$$u_{drift} = \frac{Max(x_i) - Min(x_i)}{2 \cdot \sqrt{3}} \tag{20}$$

where u_{drift} - Uncertainty (k = 1) due to long term stability of transfer meter (%)
 x_i - Averaged and temperature corrected meter error (%)

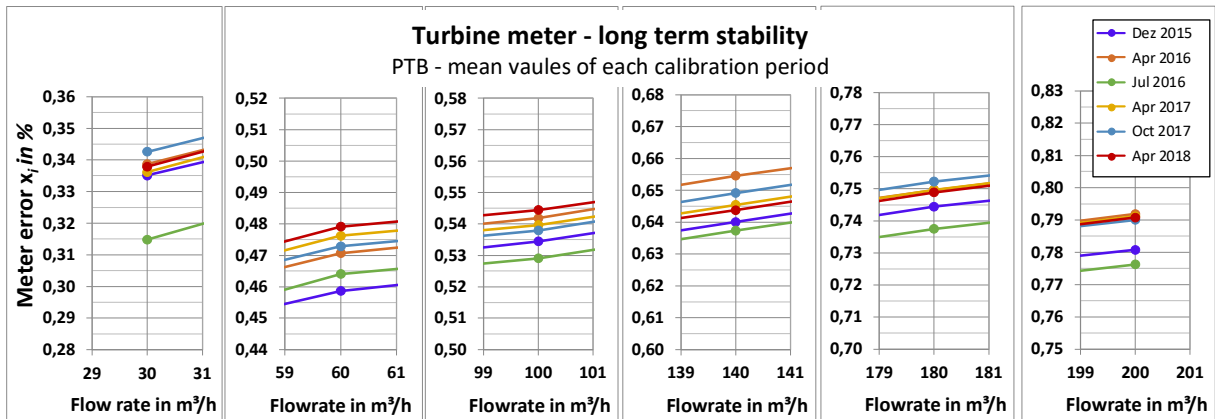


Figure 10: Long term stability of turbine meter - Mean values of temperature corrected meter error x_i for each calibration period, measured at PTB laboratory (day #1 until day# 3)

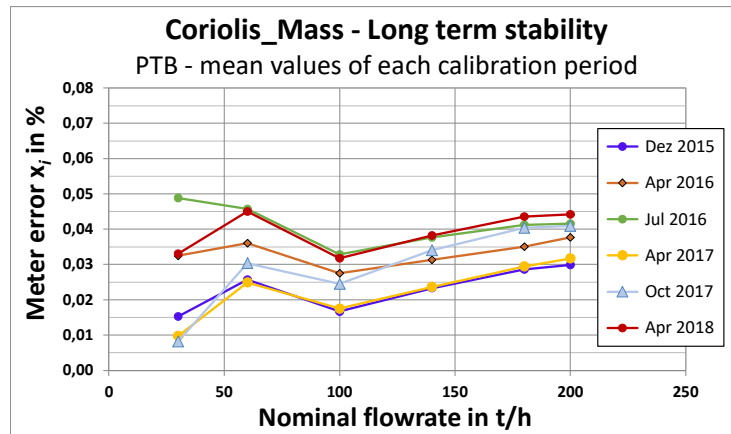


Figure 11: Long term stability of Coriolis_Mass - Mean values of temperature corrected meter error x_i for each calibration period, measured at PTB laboratory (day #1 until day# 3)

Table 10: Uncertainties u_{drift} caused by drift of meter error - turbine meter and Coriolis_Mass

$k = 1$	Nominal Flowrate					
	30 m ³ /h	60 m ³ /h	100 m ³ /h	140 m ³ /h	180 m ³ /h	200 m ³ /h
u_{drift} Turbine meter in %	0.008	0.006	0.004	0.005	0.004	0.005
u_{drift} Coriolis_Mass in %	0.012	0.006	0.005	0.004	0.004	0.004

6.2 Quantification of reproducibility - uncertainty u_{reprod}

The uncertainty due to reproducibility characteristics u_{reprod} of the transfer meter were estimated at pilot laboratory by calibrations on day #4 until day #6 (Table 6). For each period, a span of meter error $[\max(x_i) - \min(x_i)]$ was calculated (Figure 12). Because of non-normal distributed data, the uncertainty u_{reprod} was calculated separately for each flow rate by using maximum values of observed span (Equation 21). It was assumed that the final values of u_{reprod} (Table 11) did include the following sources of uncertainty: short term drift, setting of auto zero (at Coriolis meter) and reassembly of the transfer meter setup.

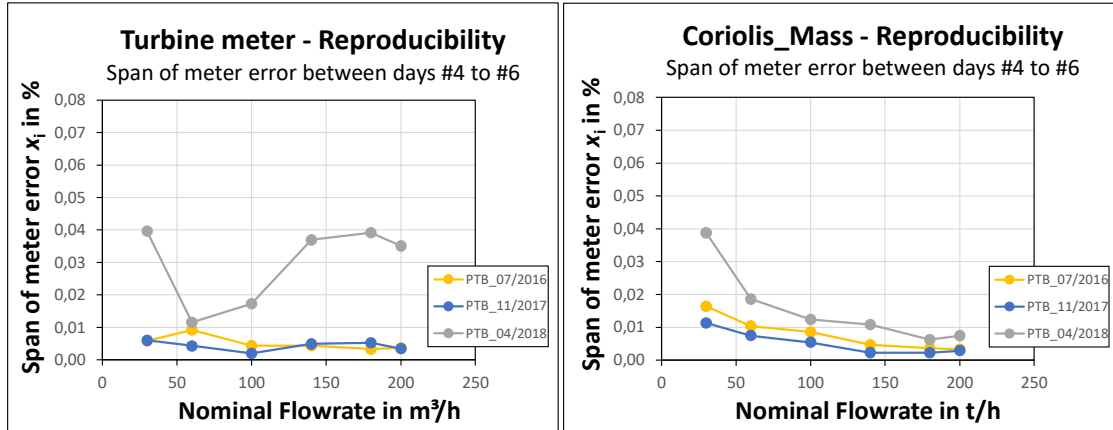


Figure 12: Results of reproducibility calibrations at pilot laboratory - Span of meter error (max - min) between calibration day #4 until day #6

$$u_{\text{reprod}} = \frac{\max [\max(x_i) - \min(x_i)]}{2 \cdot \sqrt{3}} \quad (21)$$

where u_{reprod} - Uncertainty ($k = 1$) due to reproducibility characteristics of transfer meter (%)

Table 11: Uncertainties u_{reprod} due to reproducibility characteristics of the transfer meters

$k = 1$	Nominal Flowrate					
	30 m ³ /h	60 m ³ /h	100 m ³ /h	140 m ³ /h	180 m ³ /h	200 m ³ /h
u_{reprod} Turbine meter in %	0.011	0.003	0.005	0.011	0.011	0.010
u_{reprod} Coriolis_Mass in %	0.011	0.005	0.004	0.003	0.002	0.002

6.3 Temperature dependency - uncertainty u_{temp}

Laboratory conditions

During calibrations in participating laboratories, the span of fluid temperature ranged between 10.95 °C and 30.10 °C. The maximum variation of fluid temperature within one participating lab, expressed as $\max(T_{fluid}) - \min(T_{fluid})$, was reported with 4.51 °C (Table 12, Figure 13).

Table 12: Fluid temperatures T_{fluid} (°C) in participating laboratories during calibrations

	NMI	VSL	RISE	PTB 4	UME	NIST	CENAM	ITRI	NIM	NMIJ	KRISS
Max		18.16	20.26	20.27	17.30	24.55	25.22	30.10	27.22	14.44	11.78
Min		17.37	19.94	19.93	16.50	23.45	23.53	25.59	26.21	13.50	10.95
Max - Min		0.79	0.32	0.34	0.80	1.09	1.69	4.51	1.01	0.94	0.83
Mean		17.71	20.14	19.99	16.89	24.04	24.13	27.63	26.53	13.98	11.40

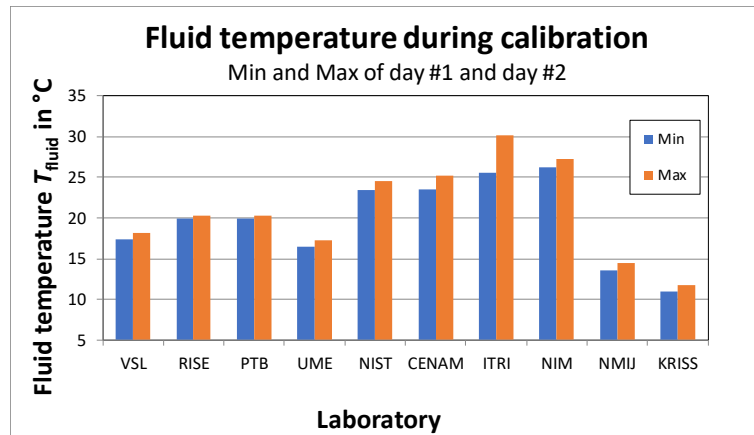


Figure 13: Fluid temperature T_{fluid} during calibrations in participating laboratories - Maximum and minimum of calibration on day #1 and day #2

Meter characteristics

The main temperature characterisation measurements were realised in pilot laboratory in 2013. The results were evaluated by calibrations in 2015 and 2019 (Table 7). The goal of characterisation measurements was to analyze meter error characteristics if the fluid temperature deviates from nominal temperature of 20 °C. Both meters showed a distinctive dependency of meter error due to changes in fluid temperature (Figure 14). The maximum range of +/-10 °C in fluid temperature T_{fluid} at participating laboratories (Figure 13), is followed by a maximum change in meter error for turbine meter with 0.055 %, respectively for Coriolis_Mass, with 0.077 %. This maximum amounts of meter error deviation would lead to a meter uncertainty u_{temp} (with $k = 1$) of 0.025 % for turbine meter and 0.033 % for Coriolis_Mass (Figure 17). Both high values of u_{temp} demonstrate the need of a temperature corrected meter error. The procedure of this correction was practiced as follows.

The correction is based on the relationship between a) deviation ΔT_{Fluid} (Equation 22) of current fluid temperature T_{Fluid} to nominal temperature T_{nom} and b) deviation Δe_{nom} (Equation 23) of meter error at current temperature conditions e to meter error e_{nom} , calibrated at nominal temperature. The relationship between ΔT and Δe_{nom} was analyzed separately for each transfer meter and flowrate by fitting a second-degree polynomial function using least squares fits (Figure 15). The resulting model parameter of Table (19) were used to calculate a correction value of meter error Δe_{cor} (Equation 24). Finally, the meter error e at current temperature conditions was corrected to meter error e_{cor} at nominal temperature conditions by applying Equation (25).

$$\Delta T_{fluid} = T_{fluid} - T_{nom} \tag{22}$$

where ΔT_{fluid} - Difference of current fluid temperature to nominal temperature of 20 °C (°C)
 T_{fluid} - Current fluid temperature (°C)
 T_{nom} - Nominal temperature of 20°C

$$\Delta e_{nom} = e - e_{nom} \tag{23}$$

where Δe_{nom} - Difference of meter error (%)
 e - Meter error at current temperature conditions (%)
 e_{nom} - Meter error at nominal temperature of 20 °C (%)

$$\Delta e_{cor} = a + b \cdot \Delta T_{fluid} + c \cdot \Delta T_{fluid}^2 \tag{24}$$

where Δe_{cor} - Correction value of meter error (%)
 a, b, c - Parameter of fitted polynomial model (Table 13) (-)

$$e_{cor} = e - \Delta e_{cor} \tag{25}$$

where e_{cor} - Temperature corrected meter error (%)

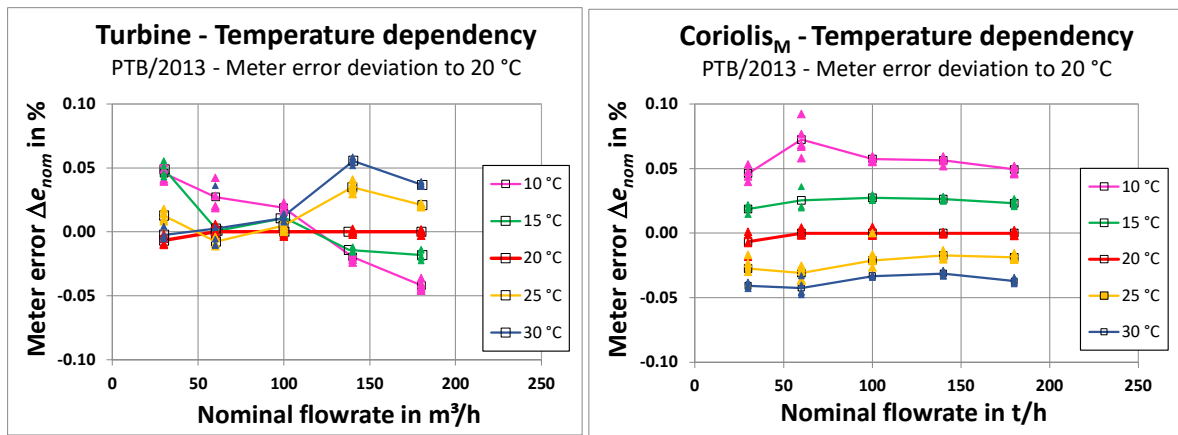


Figure 14: Temperature dependencies of turbine meter and Coriolis_Mass - Differences of meter error Δe_{nom} , expressed as results of Equation (23). All calibrations made at pilot laboratory/PTB in 2013.

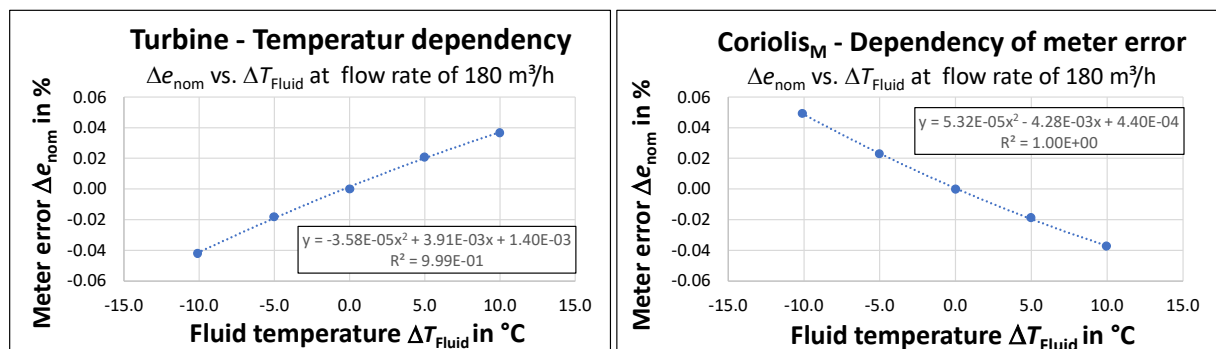


Figure 15: Temperature dependencies of Turbine meter and Coriolis_Mass - Example relationships between ΔT_{fluid} and Δe_{nom} at flowrate of 180 m³/h (Equation 22 and Equation 23) in order to estimate model parameters of Equation (24).

Table 13: Model Parameter for temperature dependent correction of meter error e by using Equation (13) until Equation (25). (*) Because no calibrations at 200 m³/h were made in 2013, parameter at flowrate of 200 m³/h were assumed to be equal to parameter at 180 m³/h.

Nominal flowrate in m ³ /h	Turbine meter model parameter			Coriolis_Mass model parameter		
	a	b	c	a	b	c
30	1.41E-02	-2.64E-03	1.09E-04	-6.69E-03	-4.38E-03	9.32E-05
60	-4.89E-03	-1.15E-03	1.89E-04	-4.44E-03	-5.71E-03	1.86E-04
100	2.89E-03	-4.52E-04	1.21E-04	-1.77E-05	-4.57E-03	1.18E-04
140	4.06E-03	3.97E-03	1.44E-04	9.29E-04	-4.36E-03	1.15E-04
180	1.40E-03	3.91E-03	-3.58E-05	4.40E-04	-4.28E-03	5.32E-05
200(*)	1.40E-03	3.91E-03	-3.58E-05	4.40E-04	-4.28E-03	5.32E-05

Meter uncertainty u_{temp}

The presented method was successfully applied during model evaluation by using the temperature characterisation measurements at pilot laboratory in 2015 and 2019 (Figure 17). Especially for Coriolis_Mass, a meter uncertainty reduction (u_{temp}) of up to 92 % was gained, if the meter error e was corrected by the described method. This clear improvement of u_{temp} over full flow scale can be explained by the distinctive temperature dependency of the Coriolis meter. Additionally, the low variations of u_{temp} between several evaluation years of 2013, 2015 and 2019 (Figure 17) underlines the long term stability of the investigated model parameters, presented in Table 13.

The calculation of u_{TS} itself is based on the following procedure and assumptions. The temperature range of reported laboratory data T_{fluid} does not exceed the investigated range of 20°C +/- 10 °C during characterisation measurements at pilot laboratory (Figure 13). As already discussed, within this range both meters showed a characteristic temperature sensitivity of meter error (Figure 14). The sensitivities of original meter error e and corrected meter error e_{cor} can also be expressed as specific model residuals $e_{residual}$ to mean values over all temperatures (Equation 26 and Figure 16). Maximum and minimum values of $e_{residual}$ were used to calculate u_{temp} with an assumption of a rectangular probability distribution (Equation 27).

The described procedure was practiced, separately for each flowrate and calibration period in 2013, 2015 and 2019. Based on corrected meter errors, the maximum uncertainties of the years 2013, 2015 and 2019 were used as final values for u_{temp} (Table 14).

For calculation of E_N values, all reported meter errors (e_v and e_m) of participating laboratories were corrected by the described method (Equation 22 until Equation 25).

$$e_{residual} = e - e_{mean} \quad (26)$$

where $e_{residual}$ - Model residuals (%)
 e_{mean} - Mean values of meter error at one flowrate over all temperatures (%)

$$u_{temp} = \frac{\max(e_{residual}) - \min(e_{residual})}{2\sqrt{3}} \quad (27)$$

where u_{temp} - Meter uncertainty caused by temperature effects (%)

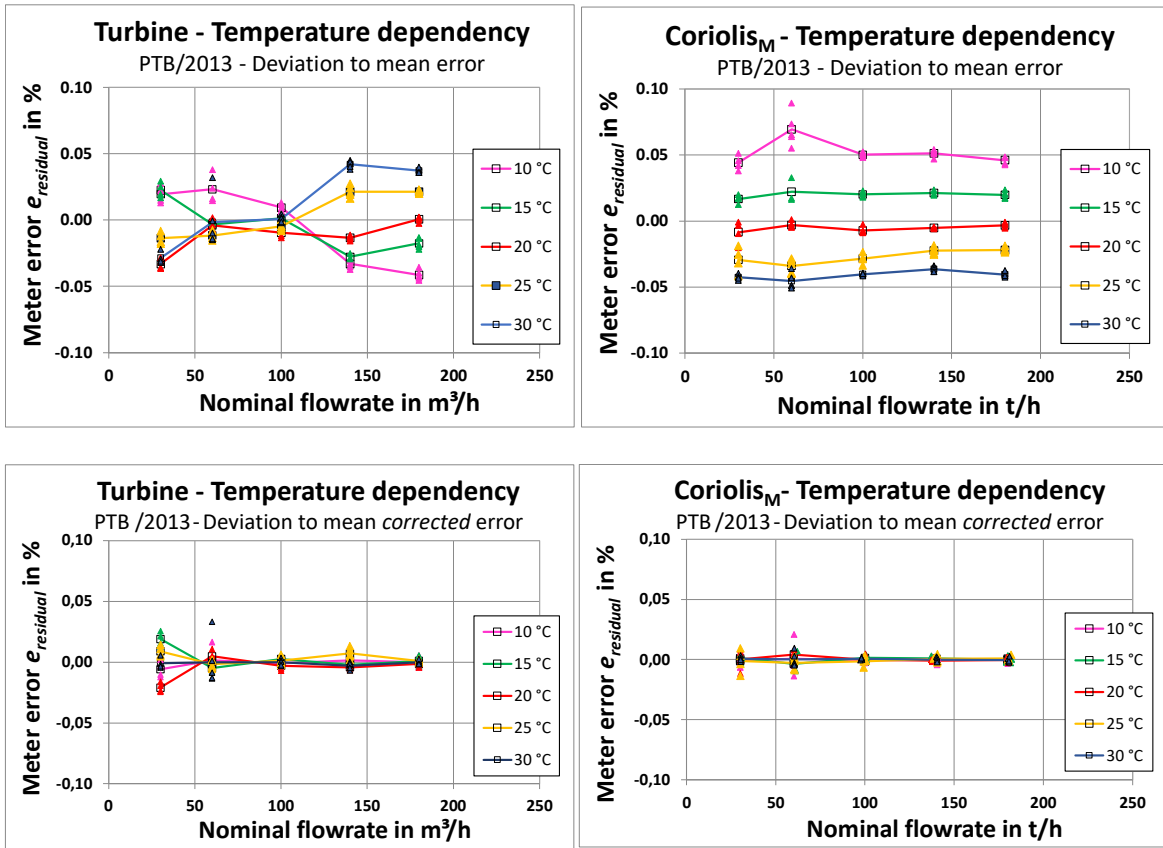


Figure 16: Temperature dependencies of Turbine meter and Coriolis_Mass - Residuals to mean values of Equation (26) for original meter error e and corrected meter error e_{cor}

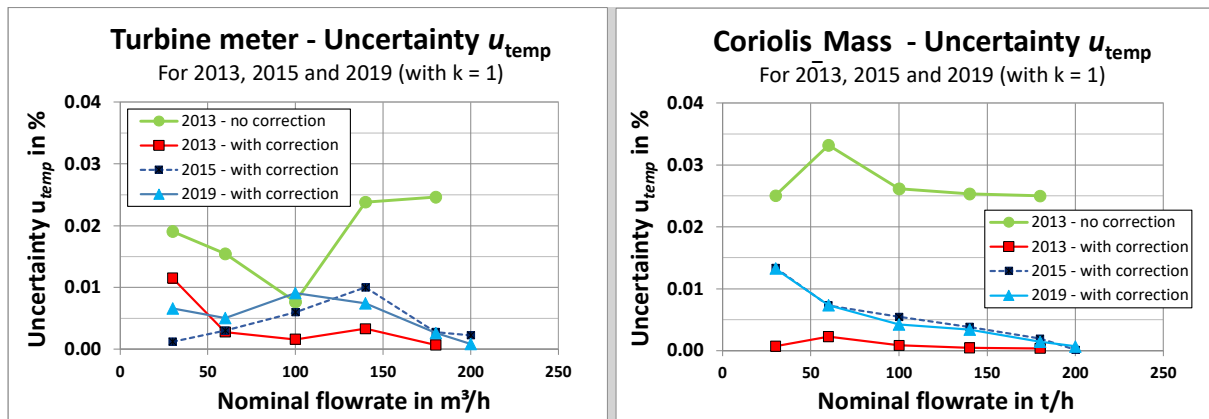


Figure 17: Meter uncertainties u_{temp} for turbine meter and Coriolis_Mass - based on non corrected meter error e for 2013, respectively, on corrected meter error e_{cor} for 2013, 2015 and 2019 by using Equation (22) until Equation (27).

Table 14: Final uncertainties of meter temperature sensitivity u_{temp}

Nominal flowrate in m^3/h	Uncertainty u_{temp} ($k = 1$)	
	Turbine meter in %	Coriolis_Mass in %
30	0.012	0.013
60	0.005	0.007
100	0.009	0.005
140	0.010	0.004
180	0.003	0.002
200	0.002	0.001

6.4 Pressure dependency - uncertainty u_{pres}

Laboratory conditions

The span of line pressure in participating laboratories p_{fluid} ranged between 0.33 bar and 3.29 bar (positive pressure after calibration setup), whereas 29 % of calibrations were made at line pressure between 2 bar and 1.5 bar and 11 % at line pressure < 1.5 bar (Figure 18).

Table 15: Line pressure p_{fluid} (bar) in participating laboratories during calibration

NMI	VSL	RISE	PTB 4	UME	NIST
Max	2.56	3.16	3.00	0.98	2.59
Min	1.65	2.98	2.99	0.33	1.64
Max - Min	0.91	0.18	0.01	0.65	0.95
Mean	2.05	3.07	3.00	0.56	1.98

NMI	CENAM	ITRI	NIM	NMIJ	KRISS
Max	3.00	4.47	2.30	2.36	2.83
Min	2.94	2.39	1.70	0.82	2.04
Max - Min	0.06	2.08	0.60	1.54	0.79
Mean	2.98	3.07	1.93	1.68	2.27

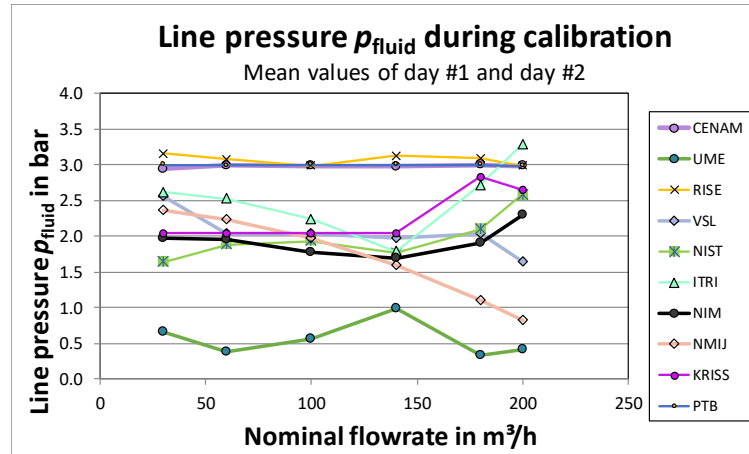


Figure 18: Line pressure during calibrations in participating laboratories - Mean values at each flowrate of calibration day #1 and day #2

Meter characteristics

Pressure dependencies of transfer meters were analyzed at pilot laboratory during characterisation measurements in 2013 and 2018 (Table 7). Due to technical restrictions, calibrations were only possible at line pressure between 2 bar and 4 bar. For data analysis, mean values over all pressure rates were calculated, separately for each calibration period and flowrate. Both meters showed a very low sensitivity to changes in line pressure (Figure 19 and Figure 20).

The deviations of meter error to mean values, expressed as residuals, were calculated separately for each calibration period. For a final analysis, these residuals were averaged over both calibration periods for each pressure rate (Figure 21). For pressure differences of +/- 1 bar, the sensitivity of meter error does not exceed +/- 0.02 % for turbine meter and +/- 0.01 % for Coriolis_{mass}.

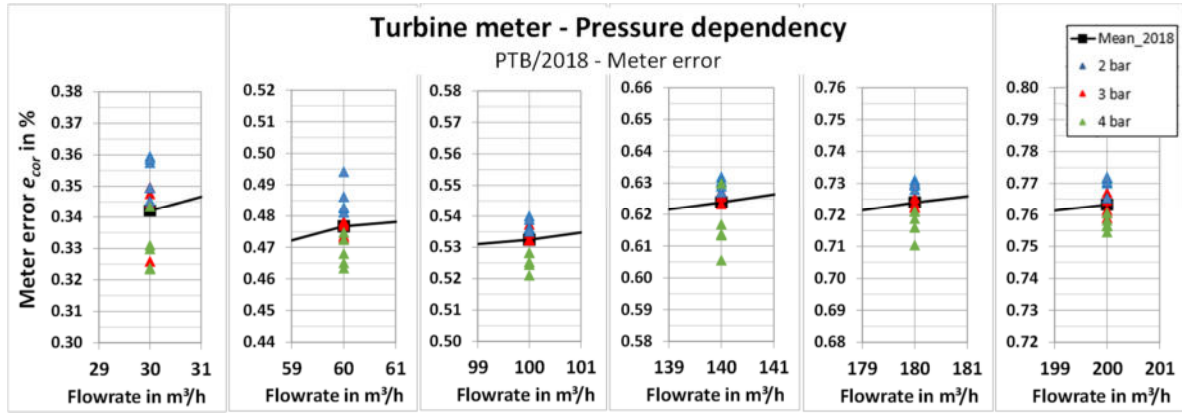


Figure 19: Pressure dependencies of turbine meter - Calibration results and mean values of characterization measurements at pilot laboratory in 2018

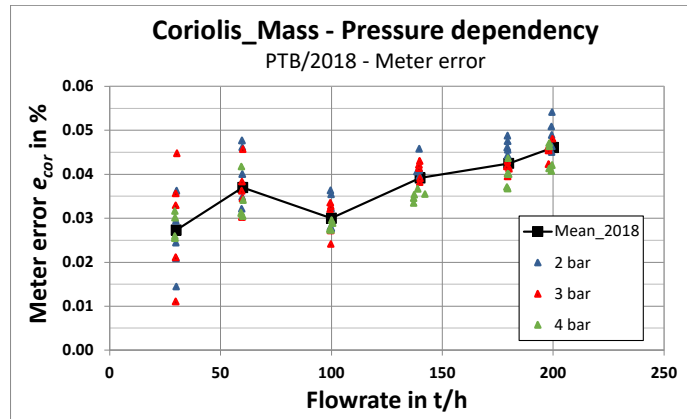


Figure 20: Pressure dependencies of Coriolis_Mass during characterisation measurements at pilot laboratory in 2018 - temperature corrected meter error and mean values

Meter uncertainty u_{pres}

For uncertainty calculation of u_{pres} it was assumed that the following conservative estimation of meter sensitivities do include the pressure range between 0.33 bar and 2 bar of reported data (Figure 18). The pressure sensitivities were treated as uncertainty contribution for turbine meter by $u_{pres} = 0.020 \% / \sqrt{3}$ and for Coriolis by $u_{pres} = 0.010 \% / \sqrt{3}$, based on a rectangular probability distribution. The described method gave constant values for turbine meter ($u_{pres} = 0.012 \%$) and Coriolis ($u_{pres} = 0.006 \%$), which were used for full investigated flow scale. For final calculation of E_N values, no pressure corrections were made to the data submitted by participating laboratories.

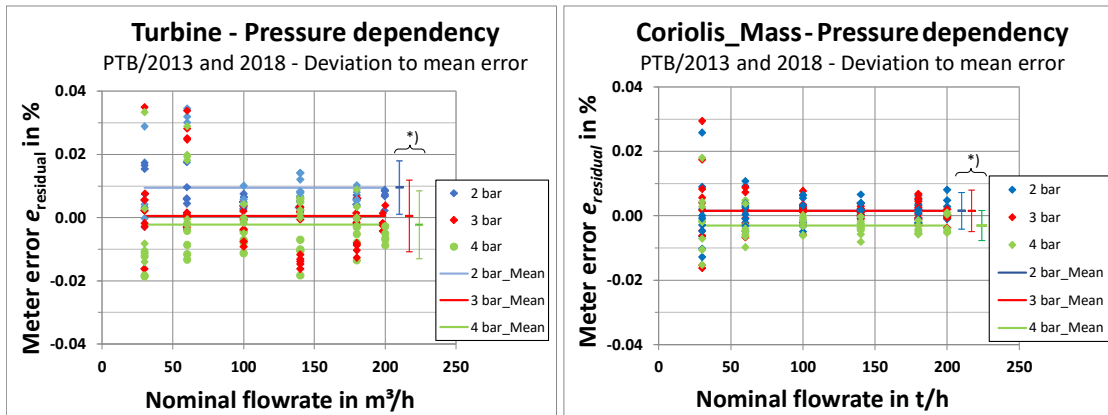


Figure 21: Pressure dependencies of turbine meter and Coriolis_Mass - residuals to mean values of temperature corrected meter error e_{cor} . *) represents the standard deviation of e_{cor} for each pressure rate

6.5 Dependency on flow stability - uncertainty u_{flow}

Laboratory conditions

For data analysis of flow stability, the deviations of reference flow between pilot laboratory and participating laboratories were used. The mean values of these differences did not exceed +/-3 % of flowrate at pilot laboratory (Figure 22).

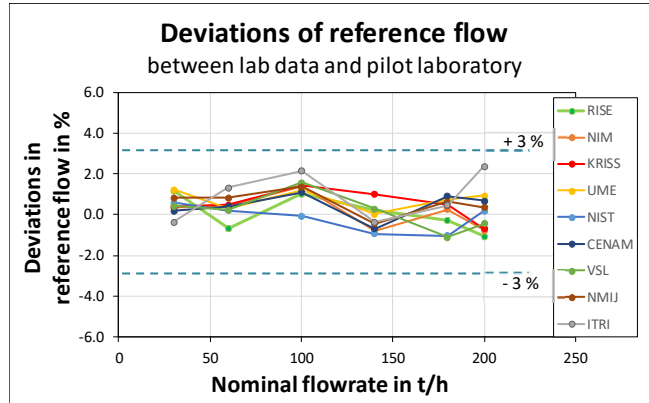


Figure 22: Flow stability \dot{m} (t/h), expressed as deviations in reference flow between pilot laboratory (07/2015) and reported values of participating laboratories

Meter characteristics

For analyzing meter error sensitivity to changes in flowrate, calibration results at reference laboratory were evaluated. Between single calibration points, the meter error of a standard calibration ($T_{fluid} = 20\text{ }^{\circ}\text{C}$, $p_{fluid} = 3\text{ bar}$) was linear interpolated. Within this model, the sensitivities of meter error were estimated by varying flowrates to maximum values of +/- 5.0 % with a resolution of 0.5 % (Figure 23). Based on the previously discussed maximum limits in flowrate stability of +/- 3 % (Figure 22), the turbine meter showed a maximum sensitivity in meter error of +/- 0.005 %. The Coriolis was much less sensitive, with values lower than +/- 0.001 % (Figure 23).

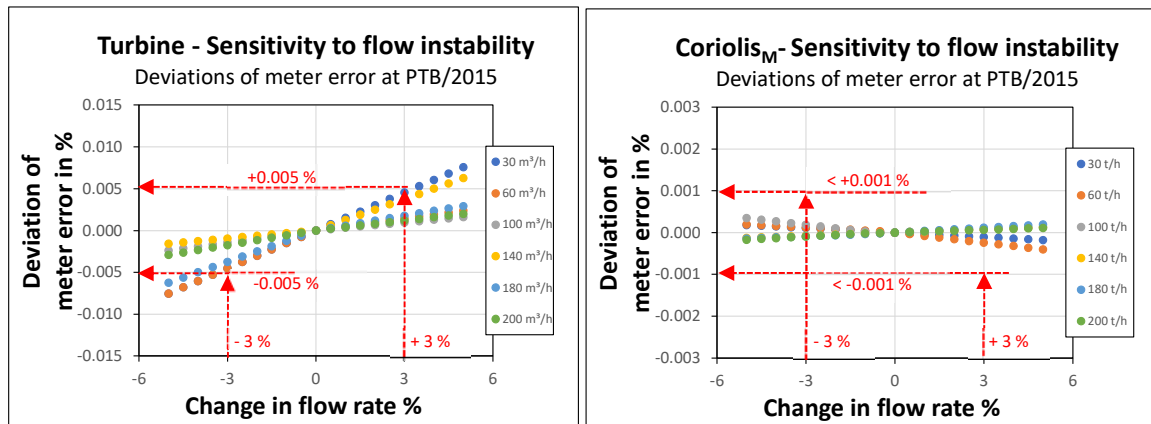


Figure 23: Sensitivity of transfer meters to flow instability - based on PTB data set 07/2015

Meter uncertainty u_{flow}

The estimated maximum values of flow meter sensitivity were used for calculation of u_{flow} . The flow stability sensitivities were treated as a rectangular uncertainty contribution, for turbine meter with $u_{flow} = 0.005\% / \sqrt{3}$ and for Coriolis by $u_{flow} = 0.001\% / \sqrt{3}$, based on a rectangular distribution. It was assumed, that the results for turbine meter ($u_{flow} = 0.003\%$) and Coriolis ($u_{flow} = 0.001\%$) are valid for full investigated flow scale. For final calculation of E_N values, no flow stability corrections were made to the data submitted by participating laboratories.

6.6 Dependency of inflow conditions to Turbine meter - uncertainty u_{inflow}

Laboratory conditions

The span of undisturbed inflow length in participating laboratories ranged between 3.0 m and 15.0 m. Typical fittings like valves, tube bundle or elbows were installed at the inflow of calibration line (Table 16).

Table 16: Reported inflow lengths of undisturbed flow and pipe installation at the inflow of calibration line in participating laboratories

NMI	VSL	RISE	PTB	UME	NIST
Undisturbed inflow length	9 m	5.7 m	8.5 m	15 m	15 m
Pipe installation before inflow	valve	90° elbow, flow conditioner	tube bundle, line reducer	valve	valve, elbow

NMI	CENAM	ITRI	NIM	NMIJ	KRISS
Undisturbed inflow length	8 m	3 m	3.3 m	7 m	8 m
Pipe installation before inflow	line reducer, valve	tube bundle, line reducer	filter	line reducer	header, valve, tube bundle

Turbine meter characteristics

For analyzing meter error sensitivity to different inflow conditions, additional calibrations at pilot laboratory were evaluated (Chapter 4.3). All used flow disturber showed a clear influence to the meter error of turbine meter. In comparison to calibrations without any flow disturber, the maximum observed shift of meter error (Figure 24) in positive direction was +0.167 % (disturber type: swirl right oriented, inflow length: 2 m), in negative direction -0.092 % (disturber type: 2nd turbine meter, inflow length: 4 m). For a maximum investigated inflow length of 8 m, the highest shift in meter error was observed with a right oriented swirl (+0.085 %).

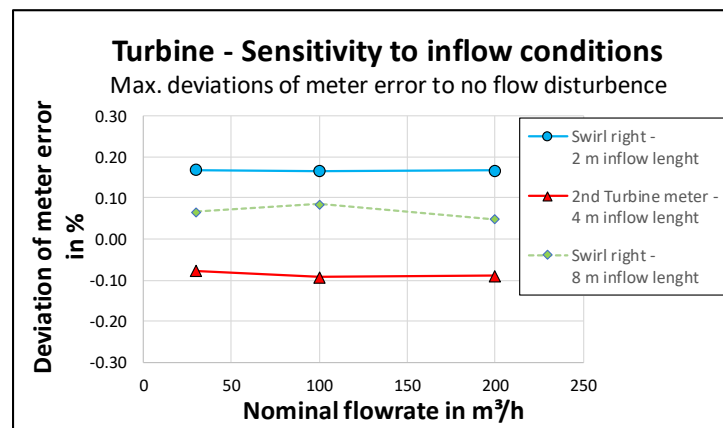


Figure 24: Maximum observed values of turbine meter sensitivity to different flow disturber and inflow length - based on PTB calibrations in 03/2019

Meter uncertainty u_{inflow}

The goal of this investigation was, to quantify the influence of different inflow conditions to calibration characteristics of the turbine meter. This research was necessary due to significant differences in turbine meter calibrations of participating laboratories. Whereas, the maximum span of Coriolis meter error between laboratories reached only 0.105 % (Figure 48), the results of turbine meter differed up to 0.395 % (Figure 26).

Such differences could not be explained by a standard estimation of meter uncertainties. Behind this background an additional uncertainty parameter (u_{inflow}) was introduced for the turbine meter.

With reference to the minimum reported inflow length of 3 m at participating laboratories (Table 16), the maximum observed meter error deviation at 2 m inflow length (Figure 24) was used for the estimation of turbine meter sensitivity u_{inflow} . The inflow sensitivity was treated as a rectangular uncertainty contribution with $u_{inflow} = 0.167\% / \sqrt{3} = 0.096\%$.

It was assumed, that the results of $u_{inflow} = 0.096\%$ are valid for full investigated flow scale. For final calculation of E_N values, no corrections for different inflow conditions were made to the submitted data of turbine meter.

6.7 Dependency of hysteresis effect - uncertainty u_{hyst}

Laboratory conditions

Depending on the working procedure of the participating laboratories, the transfer meter could be subjected to different warming up flowrates and periods. Within the technical protocol no specifications were given about warming up procedures before starting the standard calibration program of KC1.

Meter characteristics

For analyzing meter error sensitivities to hysteresis effect, calibration data of participating flow laboratory at NIM were used. During these tests, it was found that K_V of turbine meter drifted to smaller value after long time running at high flow rate (Test B of Table 17), but the value of K_V got back when the turbine was retested after zero flow rate for a while (Test A). At low flow rates between 30 m³/h and 100 m³/h, the drift reached values up to 0.128 %, which underlines the importance of this additional source of measurement uncertainty.

Table 17: Results of hysteresis effect calibrations under different types of warming up procedures (flow rates) - mean values of K_V and K_m were calibrated at flow laboratory of NIM in September 2017.

Nominal flowrate in m ³ /h	Turbine meter			Coriolis_Mass		
	Test A	Test B	ΔK_V Test A / Test B	Test A	Test B	ΔK_m Test A / Test B
	K_V in pulses/L	K_V in pulses/L	in %	K_m in pulses/kg	K_m in pulses/kg	in %
30	6.6505	6.6420	0.128	99.9981	99.9984	0.000
60	6.6596	6.6549	0.071	100.0045	99.9990	0.005
100	6.6659	6.6627	0.048	100.0133	100.0049	0.008
140	6.6725	6.6708	0.025	100.0110	100.0078	0.003
180	6.6777	6.6776	0.001	100.0107	100.0114	-0.001
200	6.6797	6.6812	-0.022	100.0128	100.0161	-0.003

Test A: After about 15min warming up at about 140 m³/h, with a test sequence **30 m³/h to 200 m³/h**.

Test B: After about 15min warming up at about 140 m³/h, with a test sequence **200 m³/h to 30 m³/h**.

Meter uncertainty u_{hyst}

For Coriolis meter, the differences ΔK_m of both testing modes (Table 17) were within the uncertainty ranges of u_{reprod} (Table 9) and were interpreted as negligible. But, there was an obviously change of K_V for Turbine meter, especially at low flow rates between 30 m³/h and 100 m³/h, by $\Delta K_V > 0.12\%$ (Table 17). Behind this background the additional uncertainty u_{hyst} for Turbine meter was introduced. Under the assumption of a rectangular distribution, the uncertainty u_{hyst} was estimated by using Equation (28). The results of u_{hyst} are presented in Table 18. For final calculation of E_N values, no correction for hysteresis effect were made to the data submitted by participating laboratories.

$$u_{\text{hyst}} = \frac{\Delta K_V}{\sqrt{3}} \quad (28)$$

where ΔK_V - Difference between testing modes A and B of Table 17 (%)

Table 18: Final uncertainties of turbine meter sensitivity to hysteresis effect u_{hyst}

Nominal flow rate	Uncertainty $u_{\text{hyst}} (k = 1)$
	Turbine meter
in m ³ /h	in %
30	0.074
60	0.041
100	0.028
140	0.015
180	0.001
200	0.013

7 Evaluation of comparison results

7.1 Ambient air temperature

Laboratory conditions

The span of air temperature in participating laboratories ranged between 18.24 °C and 32.31 °C. The maximum variation of air temperature within a participating lab, expressed as $\max(T_{\text{air}}) - \min(T_{\text{air}})$, was reported with 5.40 °C (Table 19, Figure 25).

Table 19: Air temperatures T_{air} (°C) in participating laboratories during calibrations on day#1 and day#2. *) only constant values were reported

	NMI	VSL	RISE	PTB 4	UME *)	NIST	CENAM	ITRI	NIM	NMIJ	KRISS
Max		20.97		23.24	22.60	24.50	22.60	32.31	27.10	20.89	23.90
Min		20.36		22.34	22.60	23.90	19.57	31.22	23.70	18.24	18.50
Max - Min		0.61		0.90		0.60	3.03	1.09	3.40	2.65	5.40
Mean		20.54		23.06	22.60	24.02	20.98	31.45	23.70	19.66	18.57

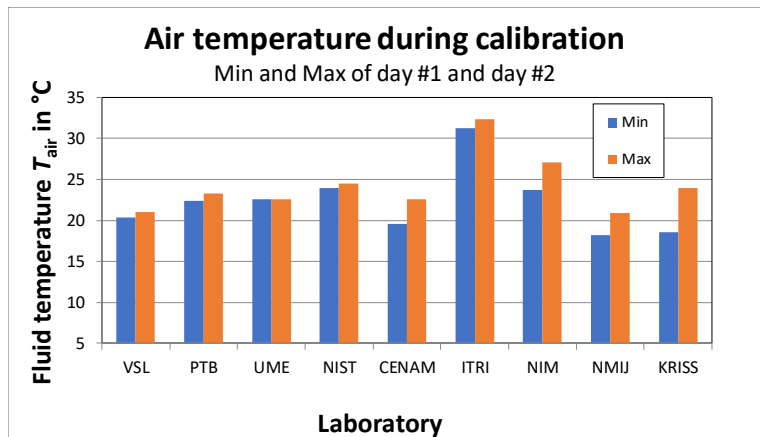


Figure 25: Air temperature T_{air} during calibrations in participating laboratories - maximum and minimum of calibration day #1 and day #2

7.2 Turbine transfer meter

7.2.1 Summarized results

Laboratory results

Table 20: Relative measurement error x_i (%) of turbine meter at participating laboratories - temperature corrected mean values of day #1 and day #2

Flowrate in m ³ /h	VSL	RISE	UME	PTB 4	NIST	CENAM	ITRI	NIM	NMIJ	KRISS
30	0.278	0.220	0.317	0.313		0.002	0.421	0.252	0.292	0.268
60	0.411	0.354	0.440	0.465		0.379	0.561	0.399	0.410	0.376
100	0.495	0.420	0.510	0.527		0.450	0.663	0.489	0.497	0.457
140	0.611	0.504	0.545	0.634		0.512	0.743	0.553	0.595	0.560
180	0.727	0.601	0.633	0.736		0.595	0.864	0.647	0.705	0.677
200	0.771	0.637	0.672	0.775		0.619	0.903	0.682	0.745	0.727

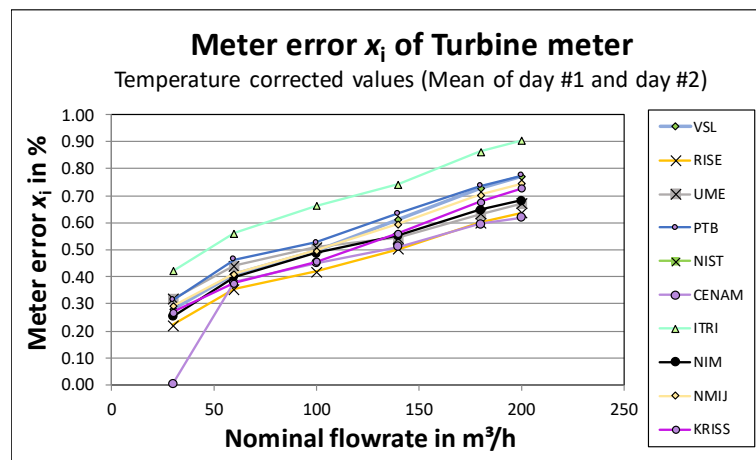


Figure 26: Relative measurement error x_i of turbine meter at participating laboratories - temperature corrected mean values of day #1 and day #2

KCRV, U(KCRV) and E_N -Value

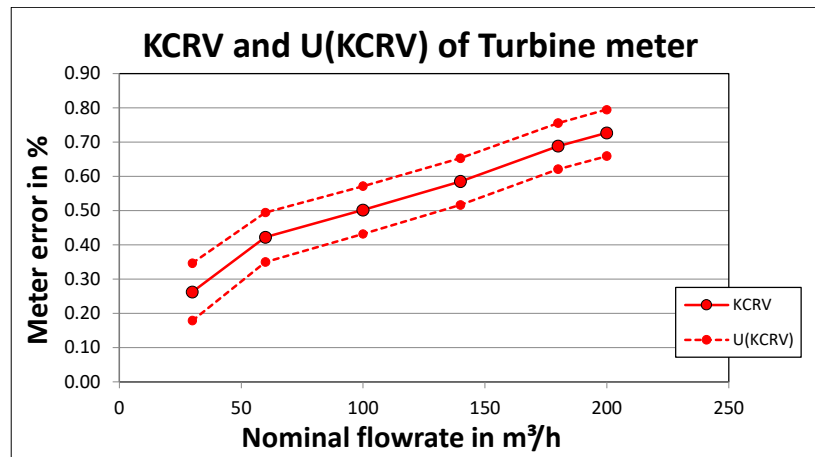
The weighted mean y and its uncertainty $u(y)$ was calculated based on all laboratory data of calibration day #1 and day #2. The results of $\frac{(x_i - y)^2}{u^2(x_i)}$ and consistency check as well as the $KCRV$ are summarized in Table 21 and Table 22.

Table 21: Results of $\frac{(x_i - y)^2}{u^2(x_i)}$ for each participating laboratory for turbine meter

Flowrate in m ³ /h	VSL	RISE	UME	PTB 4	NIST	CENAM	ITRI	NIM	NMIJ	KRISS
30	0.015	0.111	0.180	0.166		4.331	1.596	0.007	0.056	0.002
60	0.012	0.386	0.026	0.159		0.159	1.671	0.047	0.012	0.176
100	0.004	0.594	0.007	0.064		0.244	2.434	0.015	0.002	0.180
140	0.064	0.612	0.148	0.242		0.525	2.428	0.101	0.009	0.057
180	0.146	0.724	0.279	0.235		0.876	3.067	0.166	0.026	0.012
200	0.194	0.755	0.273	0.239		1.156	3.069	0.194	0.032	0.000

Table 22: Results of chi-squared test and *KCRV*-value for turbine meter

Flowrate	$\chi^2(\nu)$	χ^2_{obs}	Results of chi-squared test	<i>KCRV</i>	<i>U(KCRV)</i> (<i>k</i> = 2)
in m ³ /h				in %	in %
30	15.51	6.46	passed	0.263	0.084
60	15.51	2.65	passed	0.422	0.072
100	15.51	3.54	passed	0.502	0.070
140	15.51	4.19	passed	0.585	0.068
180	15.51	5.53	passed	0.688	0.067
200	15.51	5.91	passed	0.727	0.068

**Figure 27:** Key Comparison Reference value (*KCRV*) and its expanded uncertainty *U(KCRV)* for turbine meter, with *k* = 2

The degree of equivalence value E_N is a measure of result agreement of each participating laboratory to the *KCRV*. Expressed as the normalized differences of “lab to *KCRV*”, the final E_N values of turbine meter are summarized in Table 23 and Figure 28. All results of participating laboratories confirmed to the consistency check of chi-squared test (Table 22). No extractions of laboratory results were made. All laboratories complied with the E_N criteria of < 1.2.

Table 23: Summary of E_N -values for turbine meter of each participating laboratory

Flowrate in m ³ /h	VSL	RISE	UME	PTB 4	NIST	CENAM	ITRI	NIM	NMIJ	KRISS
30	0.07	0.18	0.22	0.22		1.10	0.67	0.04	0.13	0.02
60	0.06	0.33	0.08	0.21		0.21	0.69	0.11	0.06	0.22
100	0.04	0.41	0.04	0.13		0.26	0.83	0.07	0.02	0.22
140	0.13	0.41	0.20	0.26		0.38	0.83	0.17	0.05	0.13
180	0.20	0.45	0.28	0.26		0.50	0.93	0.22	0.09	0.06
200	0.23	0.46	0.28	0.26		0.57	0.93	0.23	0.09	0.00

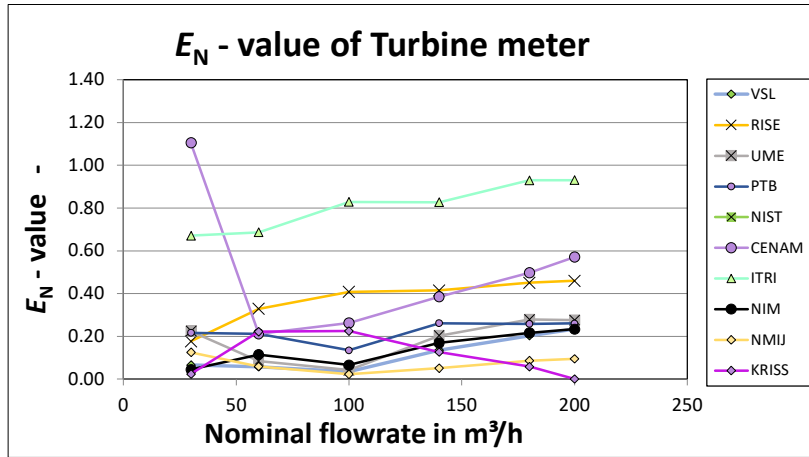


Figure 28: Summarized E_N -values of participating laboratories for turbine meter

Conclusive tests of comparison results $u_{comp}/u_{base,i}$

Based on [3], for a conclusive proof of participant results and an agreement with the *KCRV*, the comparison uncertainty ratio $u_{comp}/u_{base,i}$ should be < 2 .

Results from all participating laboratories couldn't comply with this limit (Table 24). For the purpose of KC1 the uncertainty u_{comp} of turbine meter was too high. A calibration of turbine meter gave for all laboratories inconclusive results. Finally, the meter was not suitable for a confirmation of the declared CMC values.

Table 24: Summarized results of conclusive proof $u_{comp}/u_{base,i}$ of each participating laboratory for turbine meter - * represents inconclusive data

Flowrate in m ³ /h	VSL	RISE	UME	PTB 4	NIST	CENAM	ITRI	NIM	NMIJ	KRISS
30	5.48 *	4.11 *	3.55 *	12.34 *		6.51 *	6.17 *	4.94 *	5.88 *	4.11 *
60	4.70 *	3.52 *	3.03 *	10.57 *		5.56 *	5.29 *	4.23 *	5.04 *	3.53 *
100	4.52 *	3.39 *	2.92 *	10.17 *		5.35 *	5.08 *	4.07 *	4.84 *	3.39 *
140	4.42 *	3.32 *	2.85 *	9.95 *		5.24 *	4.97 *	3.98 *	4.74 *	3.32 *
180	4.35 *	3.26 *	2.81 *	9.80 *		5.16 *	4.90 *	3.92 *	4.66 *	3.27 *
200	4.39 *	3.29 *	2.82 *	9.87 *		5.19 *	4.93 *	3.95 *	4.70 *	3.29 *

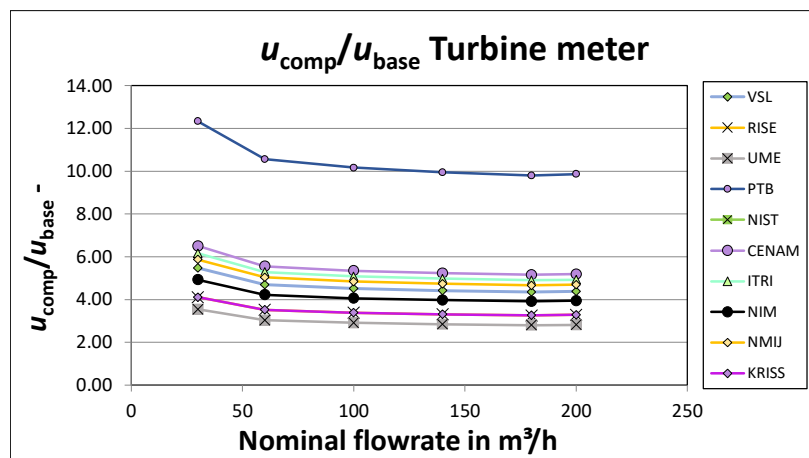


Figure 29: Summarized results of conclusive proof $u_{comp}/u_{base,i}$ of each participating laboratory for turbine meter

7.2.2 Final CMC-decision tables for participating laboratories

VSL - laboratory (Netherlands)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 25), because of inconclusive data - at all calibrated flowrates the ratio of u_{comp}/u_{base} was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

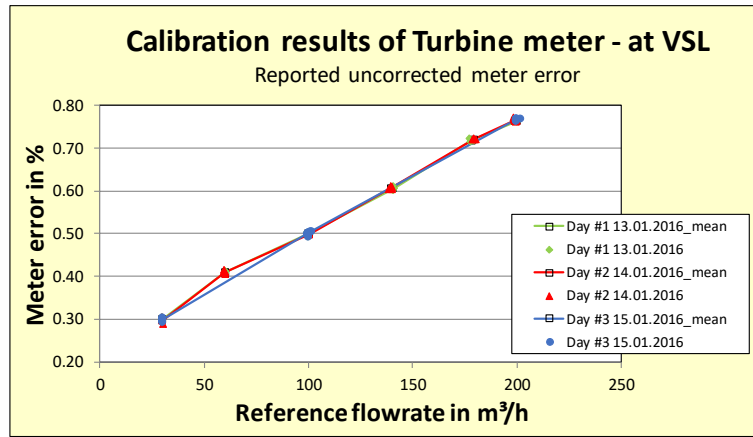


Figure 30: Calibration results of VSL laboratory for turbine meter - reported uncorrected meter error e_v

Table 25: Comparison decision table for VSL (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - * represents inconclusive data

VSL / Netherlands							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	$u_{comp}/u_{base,i}$	CMC decision status
	x_i	$U_{base,i}$ (k = 2)	$U(x_i)$ (k = 2)	d_i	$E_{N,i}$		
in m³/h	in %	in %	in %	-	-	-	
30	0.278	0.045	0.251	0.016	0.07	5.48 *	inconclusive
60	0.411	0.045	0.216	-0.012	0.06	4.70 *	inconclusive
100	0.495	0.045	0.208	-0.007	0.04	4.52 *	inconclusive
140	0.611	0.045	0.204	0.026	0.13	4.42 *	inconclusive
180	0.727	0.045	0.201	0.038	0.20	4.35 *	inconclusive
200	0.771	0.045	0.202	0.045	0.23	4.39 *	inconclusive

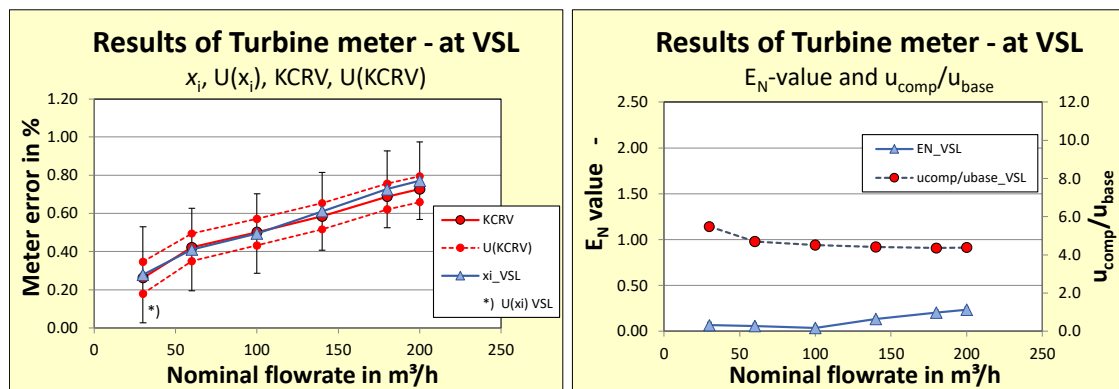


Figure 31: Comparison results of VSL laboratory for turbine meter

RISE - laboratory (Sweden)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 26), because of inconclusive data - at all calibrated flowrates the ratio of u_{comp}/u_{base} was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

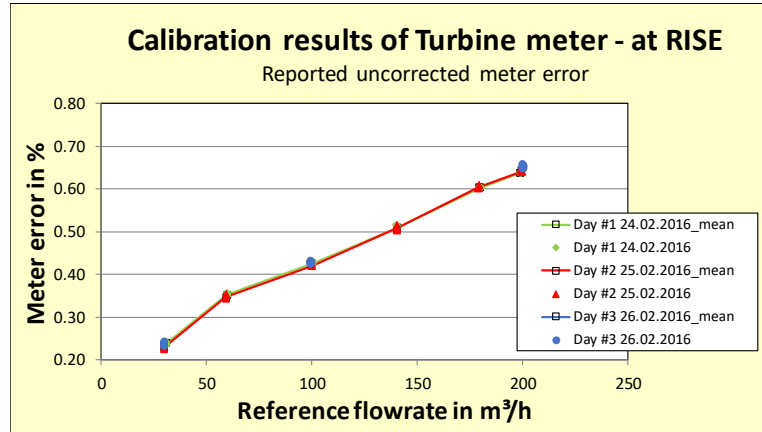


Figure 32: Calibration results of RISE laboratory for turbine meter - reported uncorrected meter error e_v

Table 26: Comparison decision table for RISE (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - * represents inconclusive data

RISE / Sweden							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
in m³/h	in %	in %	in %	-	-	-	
30	0.220	0.060	0.254	-0.042	0.18	4.11 *	inconclusive
60	0.354	0.060	0.220	-0.068	0.33	3.52 *	inconclusive
100	0.420	0.060	0.212	-0.082	0.41	3.39 *	inconclusive
140	0.504	0.060	0.208	-0.081	0.41	3.32 *	inconclusive
180	0.601	0.060	0.205	-0.087	0.45	3.26 *	inconclusive
200	0.637	0.060	0.206	-0.090	0.46	3.29 *	inconclusive

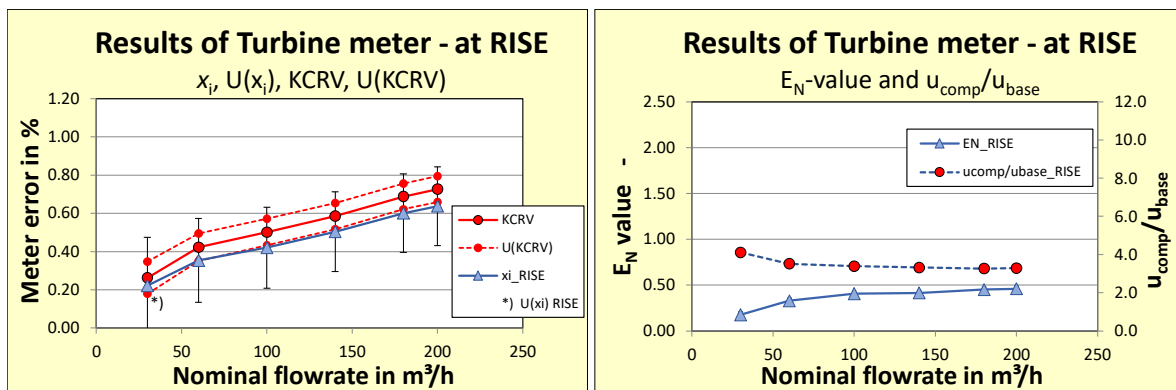


Figure 33: Comparison results of RISE laboratory for turbine meter

UME - laboratory (Turkey)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 27), because of inconclusive data - at all calibrated flowrates the ratio of u_{comp}/u_{base} was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

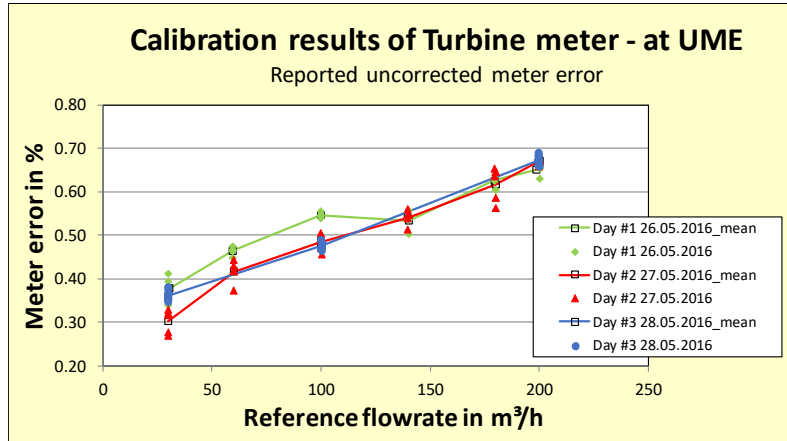


Figure 34: Calibration results of UME for turbine meter - reported uncorrected meter error e_v

Table 27: Comparison decision table for UME (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - * represents inconclusive data

UME / Turkey							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
in m^3/h	in %	in %	in %	-	-	-	
30	0.317	0.070	0.258	0.055	0.22	3.55 *	inconclusive
60	0.440	0.070	0.223	0.018	0.08	3.03 *	inconclusive
100	0.510	0.070	0.216	0.009	0.04	2.92 *	inconclusive
140	0.545	0.070	0.211	-0.041	0.20	2.85 *	inconclusive
180	0.633	0.070	0.209	-0.055	0.28	2.81 *	inconclusive
200	0.672	0.070	0.210	-0.055	0.28	2.82 *	inconclusive

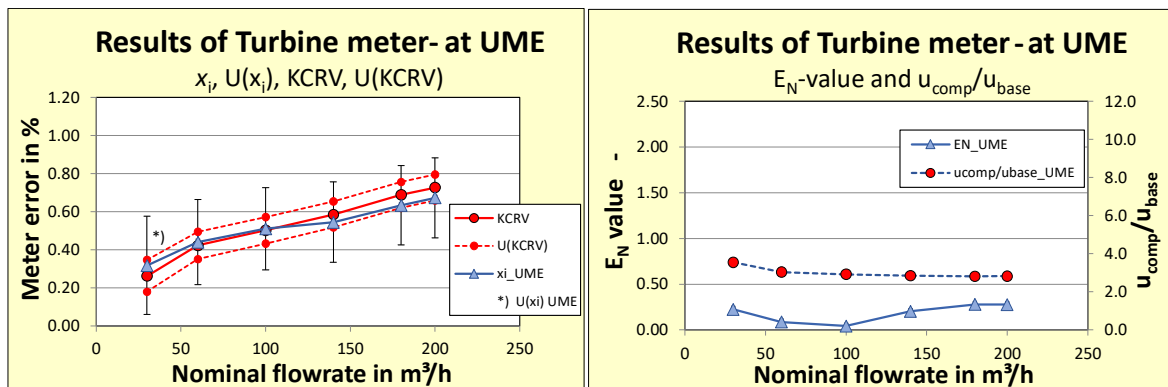


Figure 35: Comparison results of UME laboratory for turbine meter

PTB - laboratory (Germany)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 28), because of inconclusive data - at all calibrated flowrates the ratio of u_{comp}/u_{base} was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

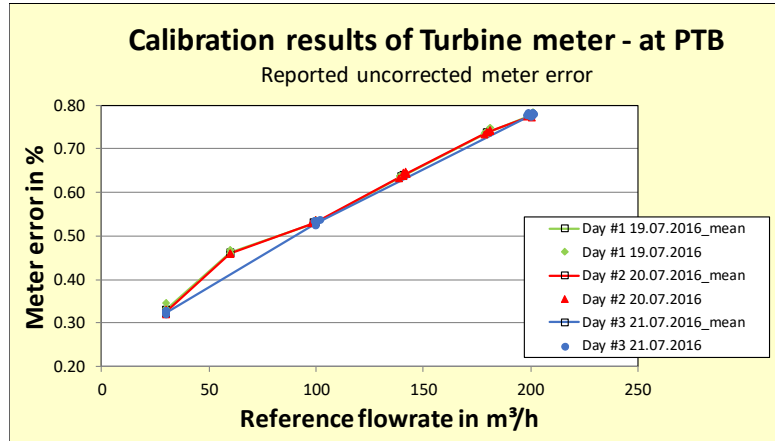


Figure 36: Calibration results of PTB for turbine meter - reported uncorrected meter error e_v

Table 28: Comparison decision table for PTB (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - * represents inconclusive data

PTB / Germany							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
in m^3/h	in %	in %	in %	-	-	-	
30	0.313	0.020	0.248	0.050	0.22	12.34 *	inconclusive
60	0.465	0.020	0.212	0.042	0.21	10.57 *	inconclusive
100	0.527	0.020	0.204	0.026	0.13	10.17 *	inconclusive
140	0.634	0.020	0.200	0.049	0.26	9.95 *	inconclusive
180	0.736	0.020	0.197	0.048	0.26	9.80 *	inconclusive
200	0.775	0.020	0.198	0.048	0.26	9.87 *	inconclusive

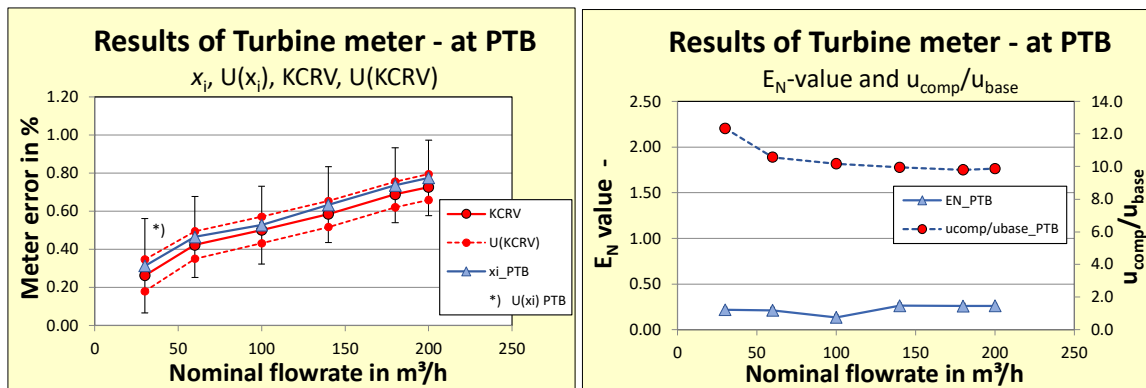


Figure 37: Comparison results of PTB laboratory for turbine meter

CENAM - laboratory (Mexico)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 29), because of inconclusive data - at all calibrated flowrates the ratio of u_{comp}/u_{base} was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

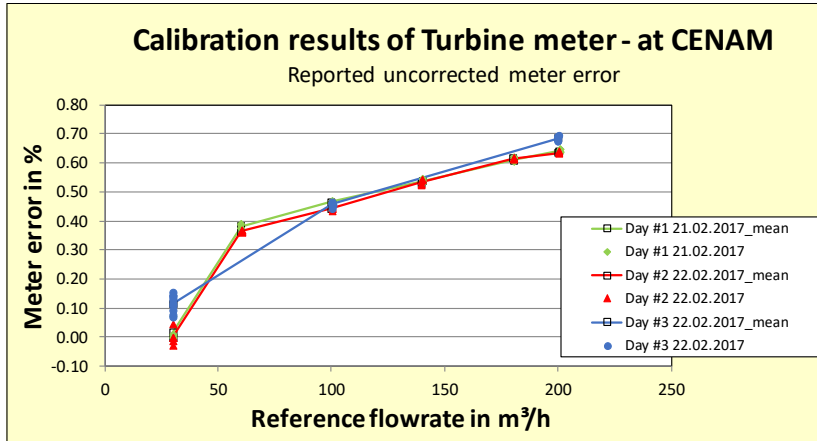


Figure 38: Calibration results of CENAM laboratory for turbine meter - reported uncorrected meter error e_v

Table 29: Comparison decision table for CENAM (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - * represents inconclusive data, ** represents data at warning level

CENAM / Mexico							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i} (k=2)$	$U(x_i) (k=2)$	d_i	$E_{N,i}$		
in m³/h	in %	in %	in %	-	-	-	
30	0.002	0.038	0.250	-0.260	1.10 **	6.51 *	inconclusive
60	0.379	0.038	0.215	-0.043	0.21	5.56 *	inconclusive
100	0.450	0.038	0.207	-0.051	0.26	5.35 *	inconclusive
140	0.512	0.038	0.203	-0.073	0.38	5.24 *	inconclusive
180	0.595	0.038	0.200	-0.093	0.50	5.16 *	inconclusive
200	0.619	0.038	0.201	-0.108	0.57	5.19 *	inconclusive

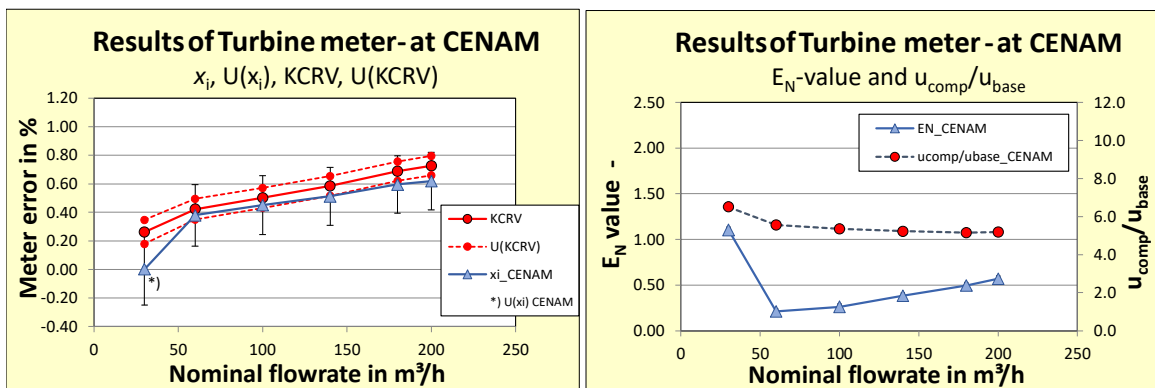


Figure 39: Comparison results of CENAM laboratory for turbine meter

ITRI - laboratory (Chinese Taipei)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 30), because of inconclusive data - at all calibrated flowrates the ratio of u_{comp}/u_{base} was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

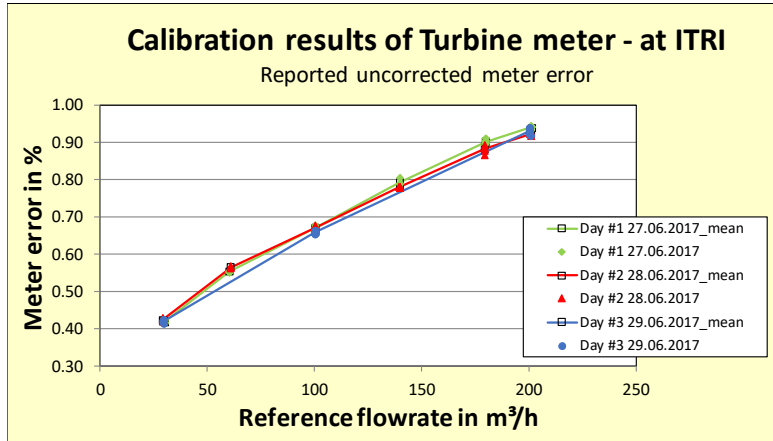


Figure 40: Calibration results of ITRI laboratory for turbine meter - reported uncorrected meter error e_v

Table 30: Comparison decision table for ITRI (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - * represents inconclusive data

Nominal flowrate	ITRI / Chinese Taipei						
	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i} (k=2)$	$U(x_i) (k=2)$	d_i	$E_{N,i}$		
in m³/h	in %	in %	in %	-	-	-	
30	0.421	0.040	0.250	0.158	0.67	6.17 *	inconclusive
60	0.561	0.040	0.215	0.139	0.69	5.29 *	inconclusive
100	0.663	0.040	0.207	0.162	0.83	5.08 *	inconclusive
140	0.743	0.040	0.203	0.158	0.83	4.97 *	inconclusive
180	0.864	0.040	0.200	0.175	0.93	4.90 *	inconclusive
200	0.903	0.040	0.201	0.176	0.93	4.93 *	inconclusive

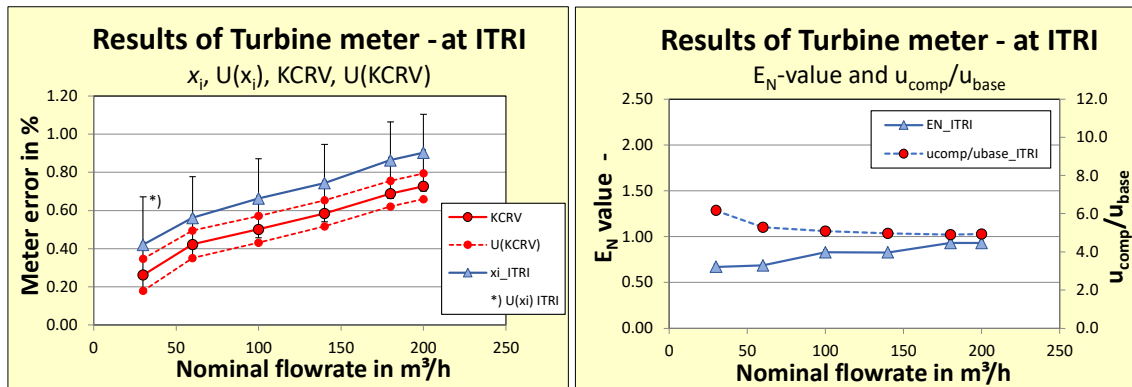


Figure 41: Comparison results of ITRI laboratory for turbine meter

NIM - laboratory (P.R. China)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 31), because of inconclusive data - at all calibrated flowrates the ratio of u_{comp}/u_{base} was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

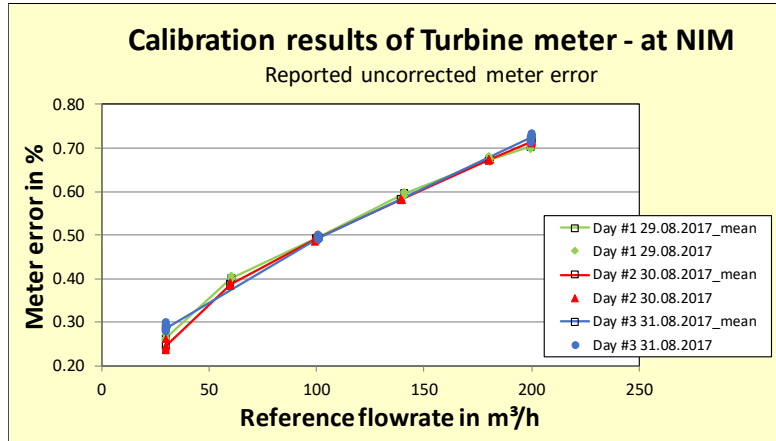


Figure 42: Calibration results of NIM laboratory for turbine meter - reported uncorrected meter error e_v

Table 31: Comparison decision table for NIM (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - * represents inconclusive data

NIM / P.R. China							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
in m³/h	in %	in %	in %	-	-	-	
30	0.252	0.050	0.252	-0.011	0.04	4.94 *	inconclusive
60	0.399	0.050	0.217	-0.024	0.11	4.23 *	inconclusive
100	0.489	0.050	0.209	-0.013	0.07	4.07 *	inconclusive
140	0.553	0.050	0.205	-0.033	0.17	3.98 *	inconclusive
180	0.647	0.050	0.202	-0.041	0.22	3.92 *	inconclusive
200	0.682	0.050	0.204	-0.045	0.23	3.95 *	inconclusive

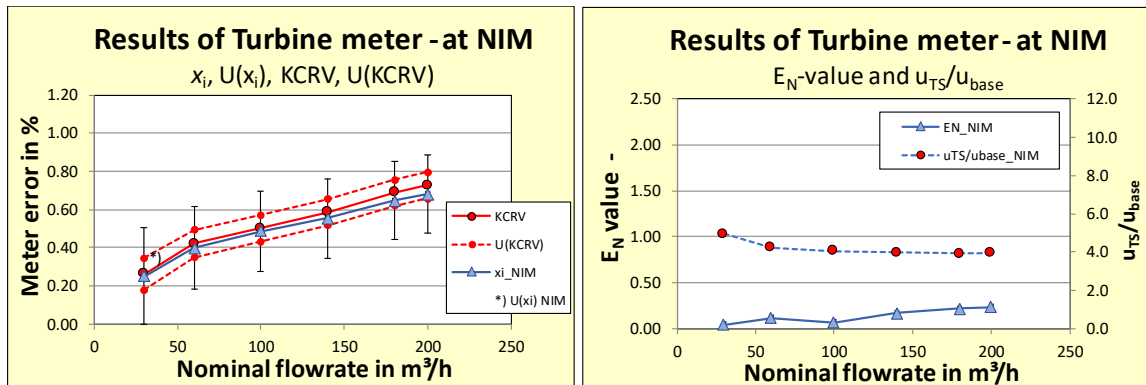


Figure 43: Comparison results of NIM laboratory for turbine meter

NMIJ - laboratory (Japan)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 32), because of inconclusive data - at all calibrated flowrates the ratio of u_{comp}/u_{base} was > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

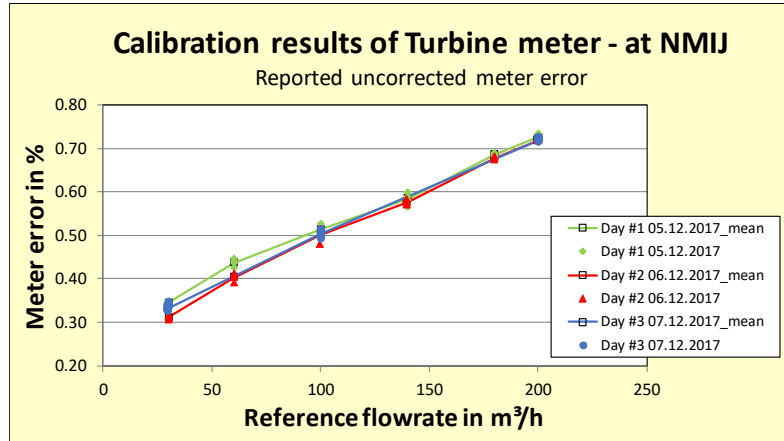


Figure 44: Calibration results of NMIJ for turbine meter - reported uncorrected meter error e_v

Table 32: Comparison decision table for NMIJ (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - * represents inconclusive data

NMIJ / Japan							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
in m ³ /h	in %	in %	in %	-	-	-	
30	0.292	0.042	0.250	0.030	0.13	5.88 *	inconclusive
60	0.410	0.042	0.216	-0.012	0.06	5.04 *	inconclusive
100	0.497	0.042	0.208	-0.004	0.02	4.84 *	inconclusive
140	0.595	0.042	0.203	0.010	0.05	4.74 *	inconclusive
180	0.705	0.042	0.200	0.016	0.09	4.66 *	inconclusive
200	0.745	0.042	0.202	0.018	0.09	4.70 *	inconclusive

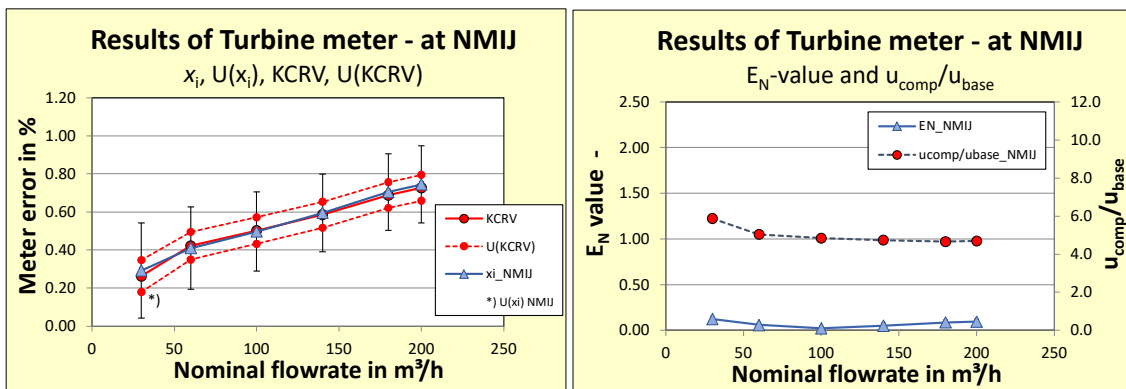


Figure 45: Comparison results of NMIJ laboratory for turbine meter

KRISS - laboratory (Korea)

For volume calibration this comparison couldn't support the declared base uncertainties of the participant (Table 33), because of inconclusive data - at all calibrated flowrates the ratio of u_{comp}/u_{base} is > 2 . The turbine meter was not suitable for a confirmation of the declared CMC values.

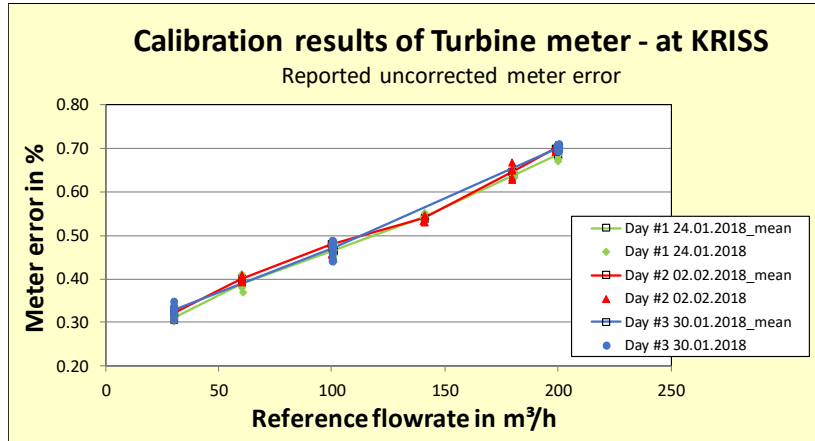


Figure 46: Comparison results of KRISS for turbine meter - reported uncorrected meter error e_v

Table 33: Comparison decision table for KRISS (turbine meter), where x_i is the temperature corrected meter error (mean of day #1 and day #2) - * represents inconclusive data

KRISS / Korea							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i} (k = 2)$	$U(x_i) (k = 2)$	d_i	$E_{N,i}$		
in m^3/h	in %	in %	in %	-	-	-	
30	0.268	0.060	0.254	0.006	0.02	4.11 *	inconclusive
60	0.376	0.060	0.220	-0.046	0.22	3.53 *	inconclusive
100	0.457	0.060	0.212	-0.045	0.22	3.39 *	inconclusive
140	0.560	0.060	0.208	-0.025	0.13	3.32 *	inconclusive
180	0.677	0.060	0.205	-0.011	0.06	3.27 *	inconclusive
200	0.727	0.060	0.206	0.000	0.00	3.29 *	inconclusive

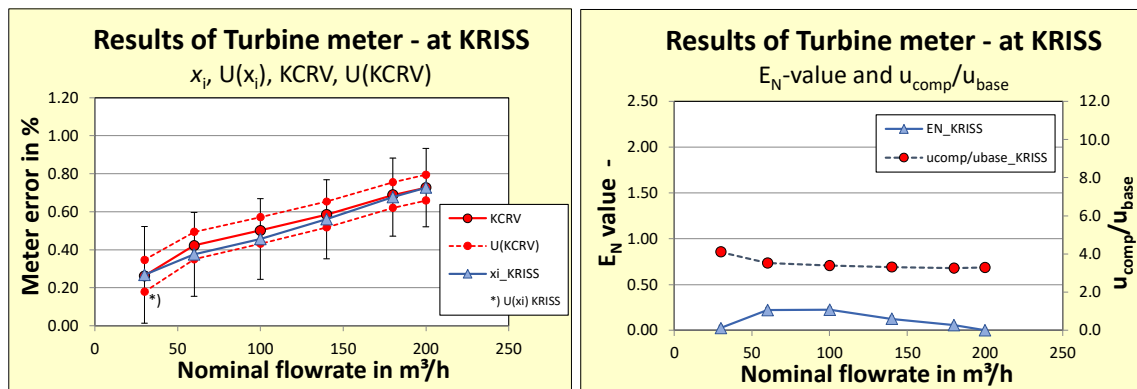


Figure 47: Comparison results of KRISS laboratory for turbine meter

7.3 Coriolis_Mass transfer meter

7.3.1 Summarized results

Laboratory results

Table 34: Relative measurement error x_i (%) of Coriolis_Mass at participating laboratories - temperature corrected mean values of day #1 and day #2

Flowrate in t/h	VSL	RISE	UME	PTB 4	NIST	CENAM	ITRI	NIM	NMIJ	KRISS
30	0.024	0.032	0.061	0.045	0.013	0.047	0.069	0.023	0.074	0.027
60	0.024	0.029	0.048	0.041	0.021	0.049	0.074	0.036	0.055	-0.002
100	0.023	0.020	0.039	0.032	0.014	0.045	0.079	0.037	0.058	-0.022
140	0.029	0.020	-0.015	0.034	0.017	0.030	0.073	0.034	0.060	-0.032
180	0.033	0.023	0.014	0.036	0.002	0.035	0.086	0.038	0.067	-0.017
200	0.037	0.022	-0.005	0.040	0.026	0.037	0.072	0.041	0.067	-0.005

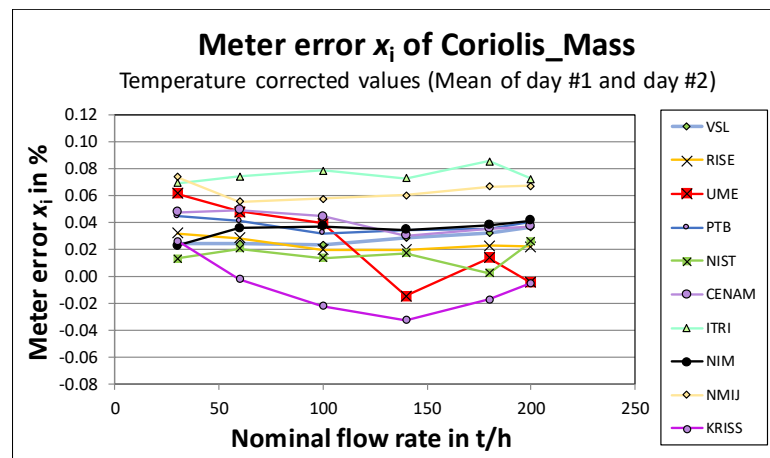


Figure 48: Relative measurement error x_i of Coriolis_Mass at participating laboratories - temperature corrected mean values of day #1 and day #2

KCRV, $U(KCRV)$ and E_N -Value

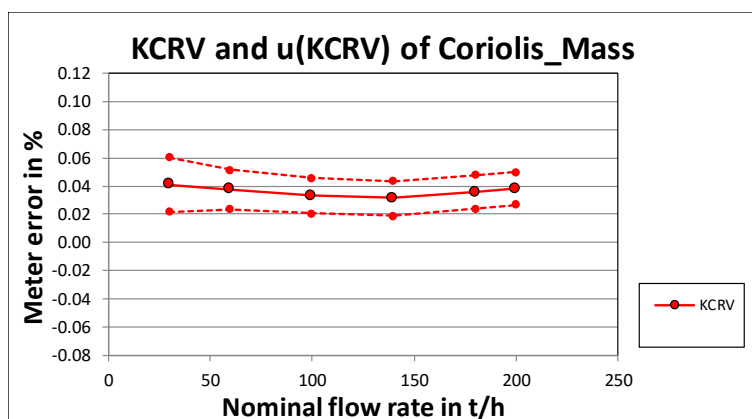
The weighted mean y and its uncertainty $u(y)$ was calculated based on all laboratory data of calibration day #1 and day #2. The results of $\frac{(x_i - y)^2}{u^2(x_i)}$ and consistency check as well as the $KCRV$ are summarized in Table 35 and Table 36.

Table 35: Results of $\frac{(x_i - y)^2}{u^2(x_i)}$ for each participating laboratory for Coriolis_Mass

Flowrate in t/h	VSL	RISE	UME	PTB 4	NIST	CENAM	ITRI	NIM	NMIJ	KRISS
30	0.408	0.041	0.232	0.022	1.028	0.055	0.908	0.302	1.103	0.155
60	0.836	0.045	0.072	0.050	0.673	0.355	2.441	0.004	0.529	1.465
100	0.609	0.105	0.028	0.007	1.018	0.417	4.132	0.023	1.101	2.926
140	0.039	0.078	1.457	0.043	0.542	0.002	3.618	0.014	1.592	4.116
180	0.088	0.099	0.362	0.000	2.148	0.001	5.356	0.008	1.929	2.877
200	0.018	0.160	1.406	0.021	0.547	0.005	2.529	0.015	1.670	1.952

Table 36: Results of chi-squared test and *KCRV*-value for Coriolis_Mass transfer meter

Flowrate	$\chi^2(\nu)$	χ^2_{obs}	Results of chi-squared test	<i>KCRV</i>	<i>U(KCRV)</i> (<i>k</i> = 2)
in t/h				in %	in %
30	16.92	4.25	passed	0.041	0.019
60	16.92	6.47	passed	0.038	0.014
100	16.92	10.37	passed	0.033	0.013
140	16.92	11.50	passed	0.031	0.012
180	16.92	12.87	passed	0.036	0.012
200	16.92	8.32	passed	0.038	0.011

**Figure 49:** Key Comparison Reference value (*KCRV*) and its expanded uncertainty *U(KCRV)* for Coriolis_Mass, with *k* = 2

The degree of equivalence value E_N is a measure of result agreement of each participating laboratory to the *KCRV*. Expressed as the normalized differences of “lab to *KCRV*”, the final E_N values are summarized in Table 37 and Figure 50. All results of participating laboratories confirmed to the consistency check of chi-squared test (Table 36). No extractions of laboratory results were made. All laboratories complied with the E_N criteria of < 1.2.

Table 37: Summary of E_N -values of participating laboratories for Coriolis_Mass transfer meter - * represents values at warning level

Flowrate in t/h	VSL	RISE	UME	PTB 4	NIST	CENAM	ITRI	NIM	NMIJ	KRISS
30	0.34	0.10	0.25	0.08	0.54	0.13	0.50	0.29	0.55	0.20
60	0.52	0.11	0.14	0.12	0.44	0.32	0.82	0.03	0.38	0.62
100	0.45	0.16	0.09	0.05	0.53	0.35	1.06 *	0.08	0.55	0.87
140	0.12	0.14	0.61	0.12	0.39	0.03	0.99	0.06	0.65	1.03 *
180	0.18	0.16	0.31	0.01	0.76	0.01	1.20 *	0.05	0.72	0.86
200	0.08	0.20	0.60	0.08	0.39	0.04	0.83	0.06	0.67	0.71

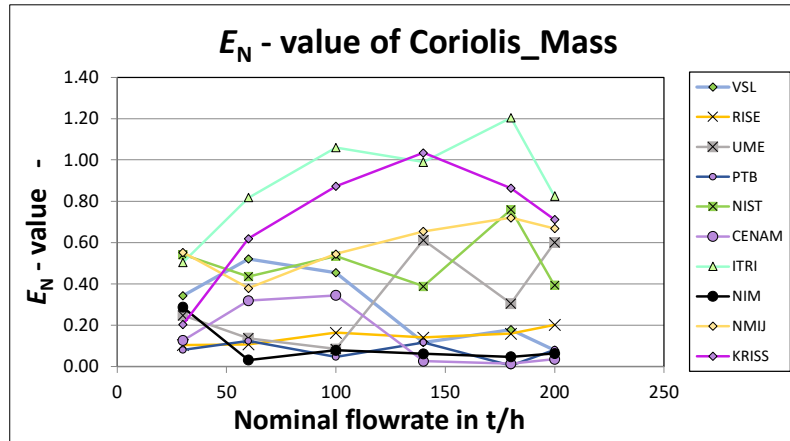


Figure 50: Summarized E_N -values of participating laboratories for Coriolis_Mass transfer meter

Conclusive tests of comparison results u_{comp}/u_{base}

Based on [3], for a conclusive proof of participant results and an agreement with the *KCRV*, the comparison uncertainty ratio u_{comp}/u_{base} should be < 2 . The results for participating laboratories are summarized in Table 38 and Figure 51.

Beside one calibration, all results complied with this limit. For the final purpose of KC1 the uncertainties u_{comp} of Coriolis_Mass were sufficiently low enough. Finally, the meter was suitable for a confirmation of the declared CMC values.

Table 38: Summarized results of conclusive proof u_{comp}/u_{base} of participating laboratories for Coriolis_Mass transfer meter - * represents values with inconclusive data

	NMI	VSL	RISE	UME	PTB 4	NIST	CENAM	ITRI	NIM	NMIJ	KRISS
Flowrate in t/h											
30		1.46	0.55	0.66	2.19 *	1.53	1.47	1.10	0.88	1.08	0.74
60		1.65	0.31	0.44	1.24	0.92	0.82	0.62	0.50	0.61	0.43
100		1.32	0.25	0.31	0.99	0.82	0.66	0.50	0.40	0.49	0.38
140		1.17	0.22	0.42	0.88	0.77	0.59	0.45	0.35	0.43	0.30
180		1.03	0.19	0.27	0.78	1.15	0.52	0.40	0.31	0.37	0.28
200		1.00	0.19	0.25	0.75	0.52	0.50	0.38	0.30	0.37	0.26

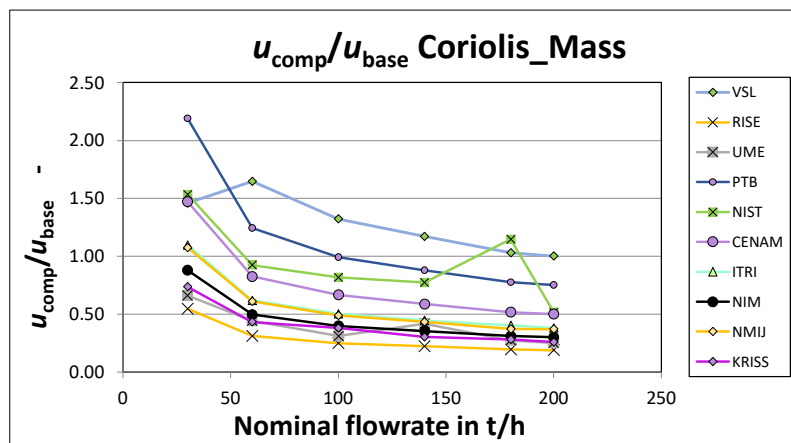


Figure 51: Summarized results of conclusive proof u_{comp}/u_{base} of participating laboratories for Coriolis_Mass transfer meter

7.3.2 Final CMC-decision tables for participating laboratories

VSL - laboratory (Netherlands)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 39).

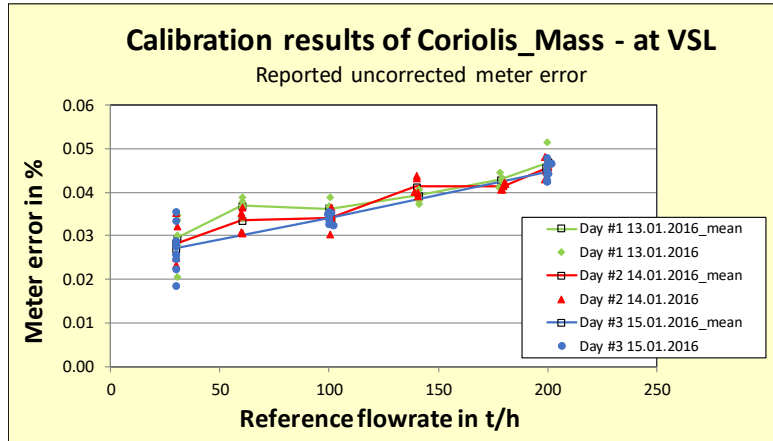


Figure 52: Calibration results of VSL for Coriolis_Mass transfer meter - reported uncorrected meter error e_m

Table 39: Comparison decision table for VSL (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2)

VSL / Netherlands							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
in t/h	in %	in %	in %	-	-	-	
30	0.024	0.030	0.053	-0.017	0.34	1.46	acceptable
60	0.024	0.015	0.029	-0.013	0.52	1.65	acceptable
100	0.023	0.015	0.025	-0.010	0.45	1.32	acceptable
140	0.029	0.015	0.023	-0.002	0.12	1.17	acceptable
180	0.033	0.015	0.022	-0.003	0.18	1.03	acceptable
200	0.037	0.015	0.021	-0.001	0.08	1.00	acceptable

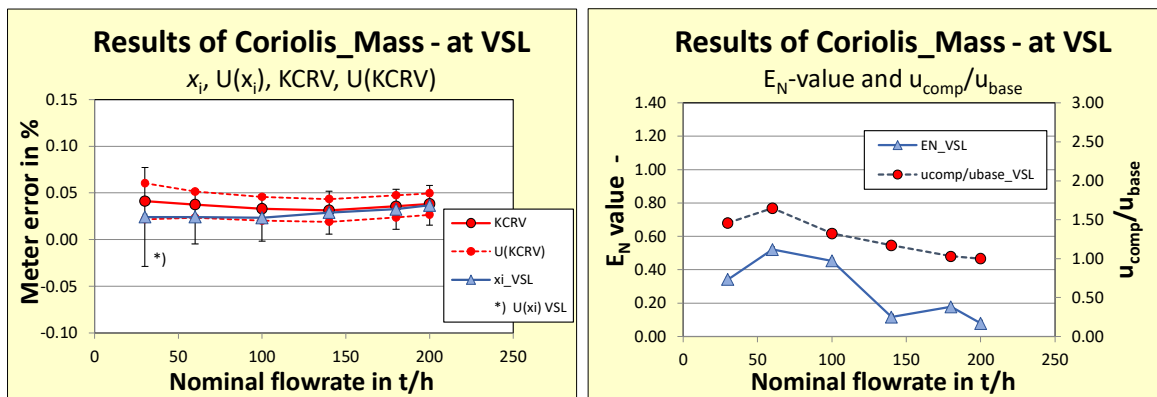


Figure 53: Comparison results of VSL laboratory for Coriolis_Mass transfer meter

RISE - laboratory (Sweden)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 40).

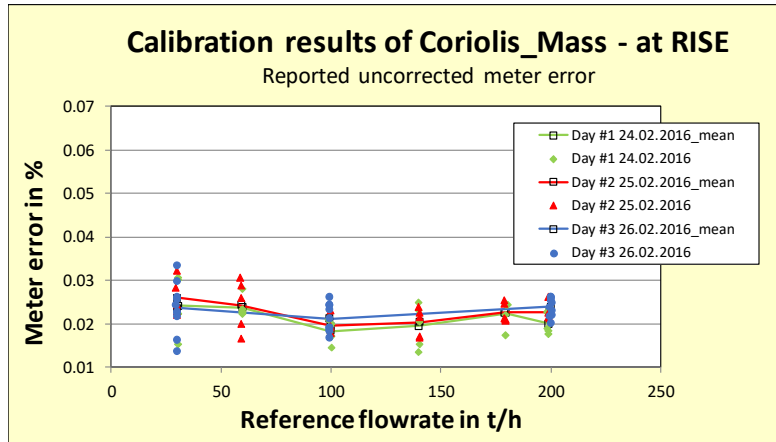


Figure 54: Calibration results of RISE for Coriolis_Mass transfer meter – reported uncorrected meter error e_m

Table 40: Comparison decision table for RISE laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2)

RISE / Sweden							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
in t/h	in %	in %	in %	-	-	-	
30	0.032	0.080	0.091	-0.009	0.10	0.55	acceptable
60	0.029	0.080	0.084	-0.009	0.11	0.31	acceptable
100	0.020	0.080	0.082	-0.013	0.16	0.25	acceptable
140	0.020	0.080	0.082	-0.011	0.14	0.22	acceptable
180	0.023	0.080	0.081	-0.013	0.16	0.19	acceptable
200	0.022	0.080	0.081	-0.016	0.20	0.19	acceptable

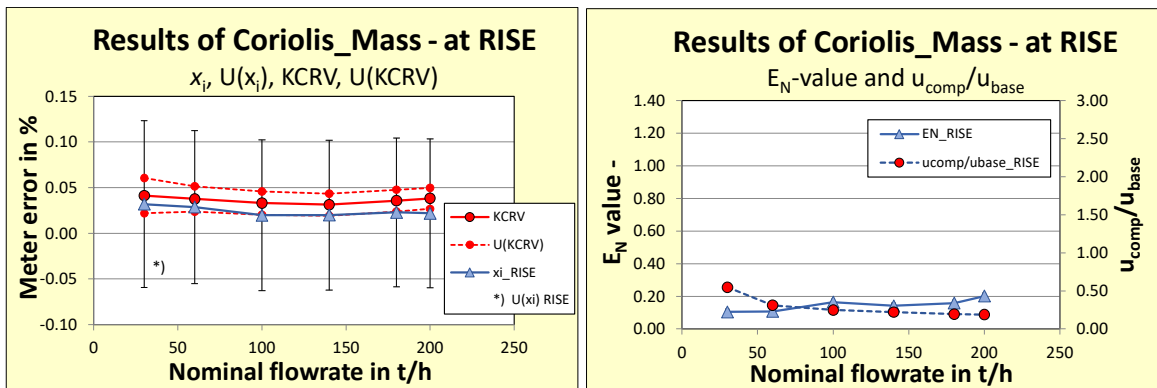


Figure 55: Comparison results of RISE laboratory for Coriolis_Mass transfer meter

UME - laboratory (Turkey)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 41).

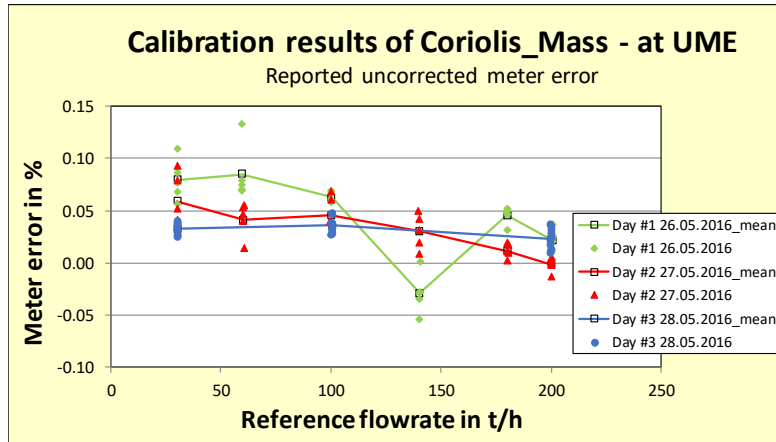


Figure 56: Calibration results of UME for Coriolis_Mass transfer meter – reported uncorrected meter error e_m

Table 41: Comparison decision table for UME laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2)

UME / Turkey							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i} (k=2)$	$U(x_i) (k=2)$	d_i	$E_{N,i}$		
in t/h	in %	in %	in %	-	-	-	
30	0.061	0.070	0.084	0.020	0.25	0.66	acceptable
60	0.048	0.070	0.077	0.010	0.14	0.44	acceptable
100	0.039	0.070	0.073	0.006	0.09	0.31	acceptable
140	-0.015	0.070	0.076	-0.046	0.61	0.42	acceptable
180	0.014	0.070	0.073	-0.022	0.31	0.27	acceptable
200	-0.005	0.070	0.072	-0.043	0.60	0.25	acceptable

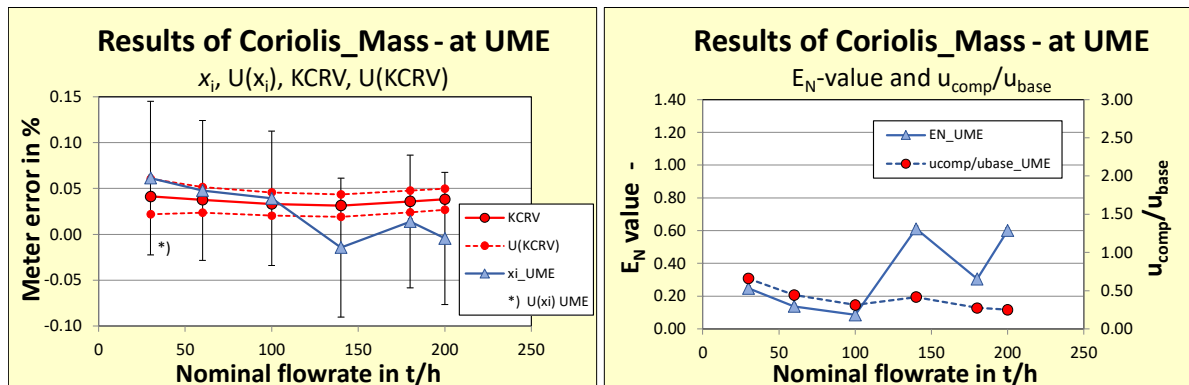


Figure 57: Comparison results of UME laboratory for Coriolis_Mass transfer meter

PTB - laboratory (Germany)

For mass calibration between flowrates of 60 t/h and 200 t/h this comparison supported the declared base uncertainties of the participant (Table 42). Only at the flowrate of 30 t/h the results were inconclusive - ratio of u_{comp}/u_{base} was > 2 . The Coriolis meter was not suitable for a confirmation of the declared CMC value at this flowrate.

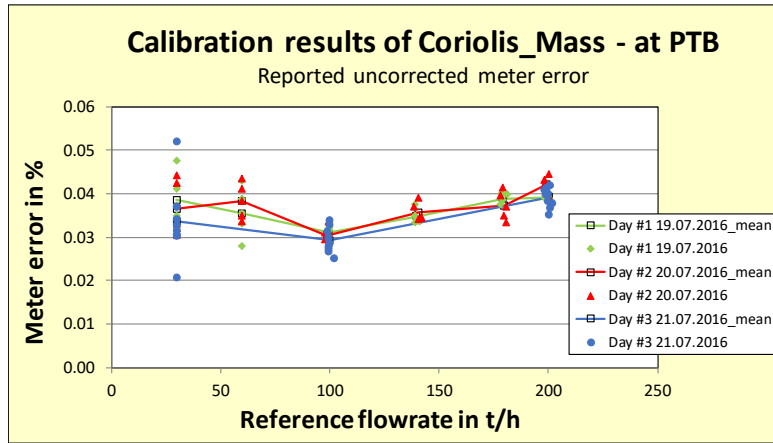


Figure 58: Calibration results of PTB for Coriolis_Mass transfer meter – reported uncorrected meter error e_m

Table 42: Comparison decision table for PTB laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2) - * represents inconclusive data

PTB / Germany							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i} (k=2)$	$U(x_i) (k=2)$	d_i	$E_{N,i}$		
in t/h	in %	in %	in %	-	-	-	
30	0.045	0.020	0.048	0.004	0.08	2.19 *	inconclusive
60	0.041	0.020	0.032	0.004	0.12	1.24	acceptable
100	0.032	0.020	0.028	-0.001	0.05	0.99	acceptable
140	0.034	0.020	0.027	0.003	0.12	0.88	acceptable
180	0.036	0.020	0.025	0.000	0.01	0.78	acceptable
200	0.040	0.020	0.025	0.002	0.08	0.75	acceptable

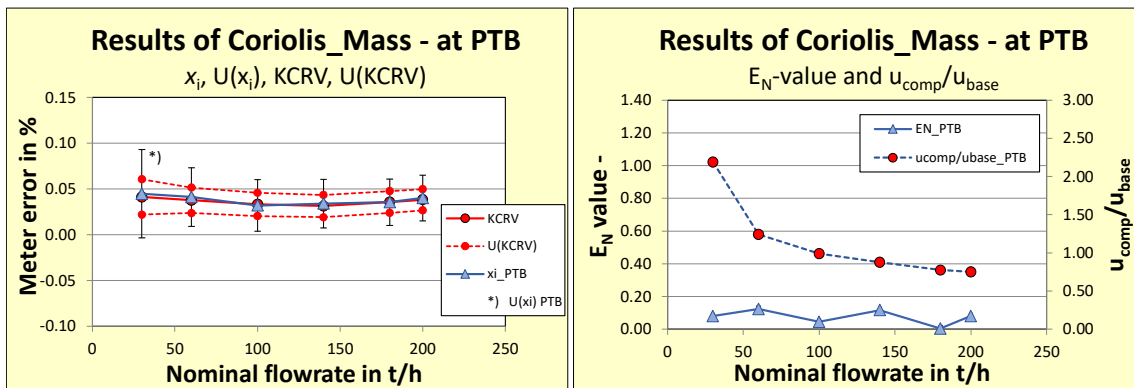


Figure 59: Comparison results of PTB laboratory for Coriolis_Mass transfer meter

NIST - laboratory (USA)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 43).

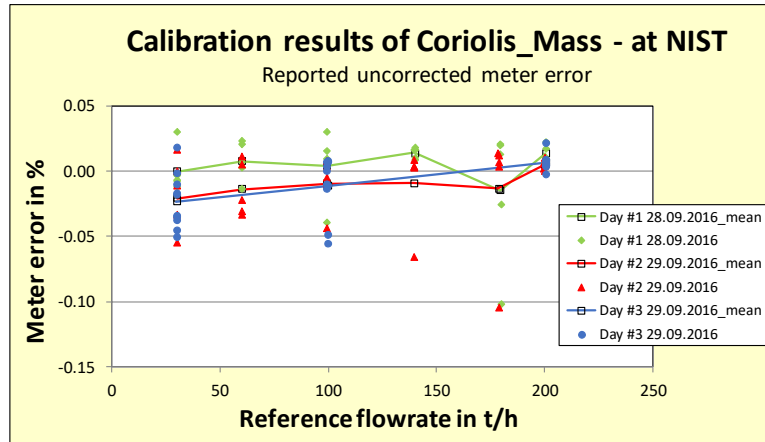


Figure 60: Comparison results of NIST for Coriolis_Mass transfer meter - reported uncorrected meter error e_m

Table 43: Comparison decision table for NIST laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2)

NIST / USA							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i} (k=2)$	$U(x_i) (k=2)$	d_i	$E_{N,i}$		
in t/h	in %	in %	in %	-	-	-	
30	0.013	0.030	0.055	-0.028	0.54	1.53	acceptable
60	0.021	0.030	0.041	-0.017	0.44	0.92	acceptable
100	0.014	0.030	0.039	-0.020	0.53	0.82	acceptable
140	0.017	0.030	0.038	-0.014	0.39	0.77	acceptable
180	0.002	0.030	0.046	-0.033	0.76	1.15	acceptable
200	0.026	0.030	0.034	-0.012	0.39	0.52	acceptable

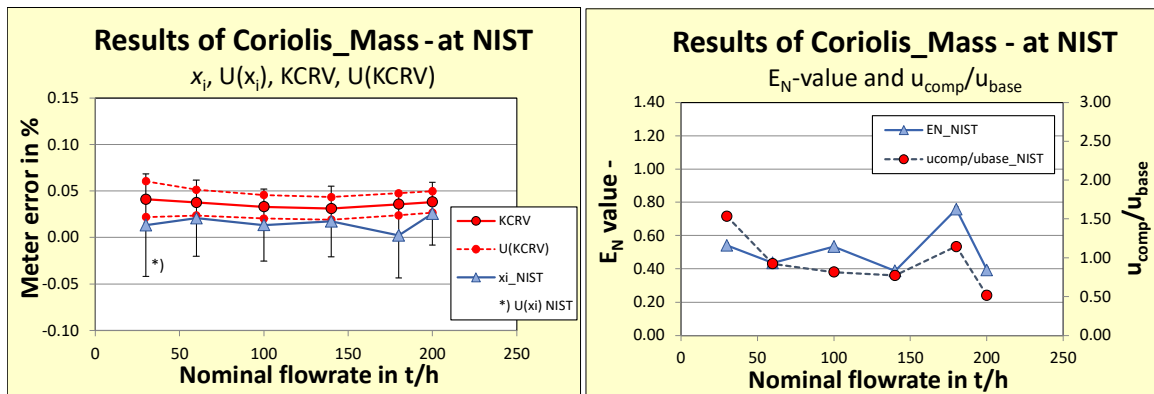


Figure 61: Comparison results of NIST laboratory for Coriolis_Mass transfer meter

CENAM - laboratory (Mexico)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 44).

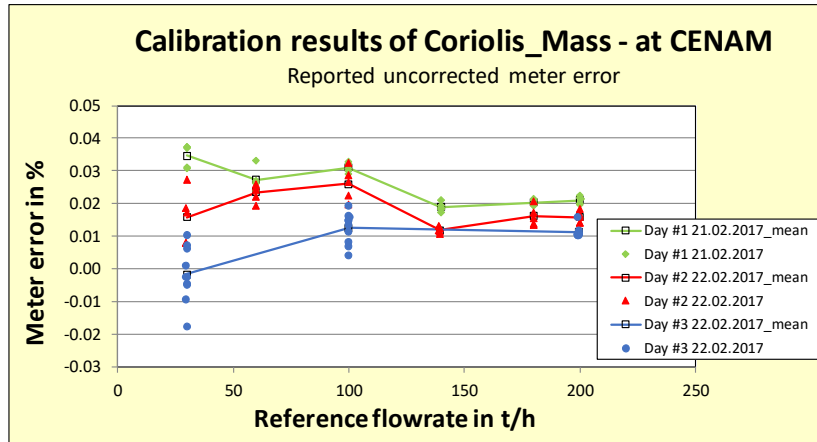


Figure 62: Comparison results of CENAM for Coriolis_Mass transfer meter - reported uncorrected meter error e_m

Table 44: Comparison decision table for CENAM laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2)

CENAM / Mexico							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
in t/h	in %	in %	in %	-	-	-	
30	0.047	0.030	0.053	0.006	0.13	1.47	acceptable
60	0.049	0.030	0.039	0.012	0.32	0.82	acceptable
100	0.045	0.030	0.036	0.012	0.35	0.66	acceptable
140	0.030	0.030	0.035	-0.001	0.03	0.59	acceptable
180	0.035	0.030	0.034	0.000	0.01	0.52	acceptable
200	0.037	0.030	0.034	-0.001	0.04	0.50	acceptable

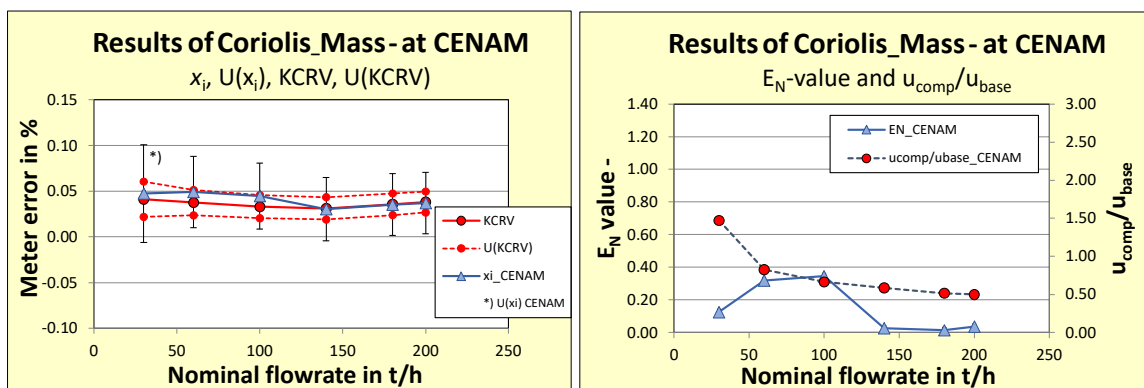


Figure 63: Comparison results of CENAM laboratory for Coriolis_Mass transfer meter

ITRI - laboratory (Chinese Taipei)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 45).

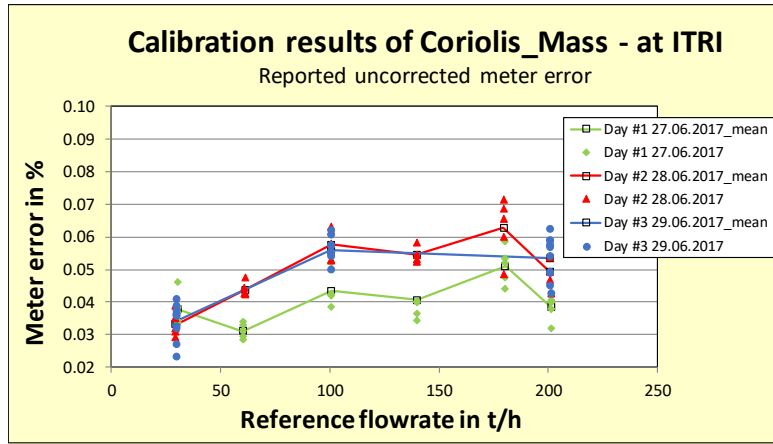


Figure 64: Comparison results of ITRI for Coriolis_Mass transfer meter - reported uncorrected meter error e_m

Table 45: Comparison decision table for ITRI laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2) - * represents E_N values at warning level

ITRI / Chinese Taipei							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i} (k=2)$	$U(x_i) (k=2)$	d_i	$E_{N,i}$		
in t/h	in %	in %	in %	-	-	-	
30	0.069	0.040	0.059	0.028	0.50	1.10	acceptable
60	0.074	0.040	0.047	0.037	0.82	0.62	acceptable
100	0.079	0.040	0.045	0.045	1.06 *	0.50	warning level
140	0.073	0.040	0.044	0.042	0.99	0.45	acceptable
180	0.086	0.040	0.043	0.050	1.20 *	0.40	warning level
200	0.072	0.040	0.043	0.034	0.83	0.38	acceptable

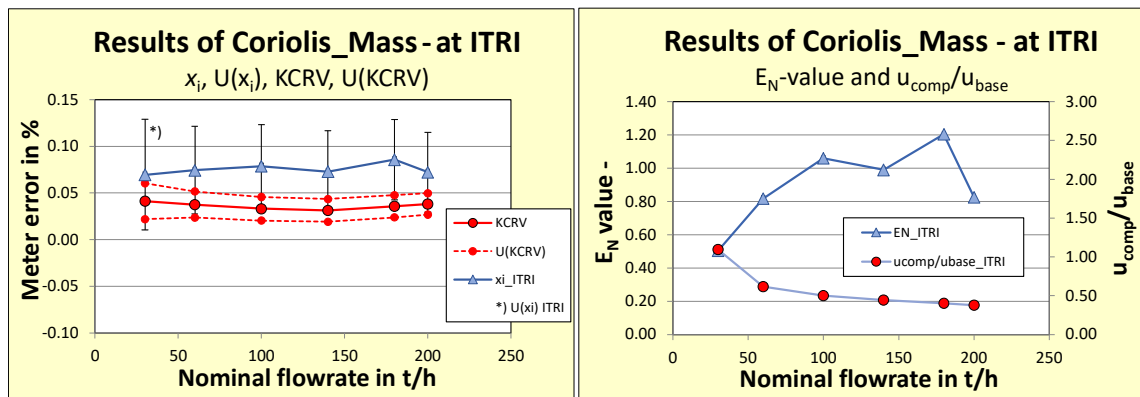


Figure 65: Comparison results of ITRI Chinese Taipei laboratory for Coriolis_Mass transfer meter

NIM - laboratory (P.R. China)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 46).

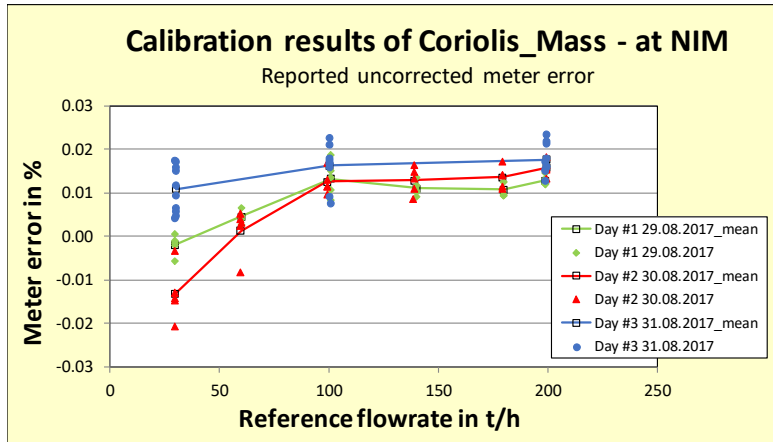


Figure 66: Calibration results of NIM for Coriolis_Mass transfer meter – reported uncorrected meter error e_m

Table 46: Comparison decision table for NIM laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2)

NIM / P.R. China							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i}$ ($k = 2$)	$U(x_i)$ ($k = 2$)	d_i	$E_{N,i}$		
in t/h	in %	in %	in %	-	-	-	
30	0.023	0.050	0.067	-0.018	0.29	0.88	acceptable
60	0.036	0.050	0.056	-0.002	0.03	0.50	acceptable
100	0.037	0.050	0.054	0.004	0.08	0.40	acceptable
140	0.034	0.050	0.053	0.003	0.06	0.35	acceptable
180	0.038	0.050	0.052	0.002	0.05	0.31	acceptable
200	0.041	0.050	0.052	0.003	0.06	0.30	acceptable

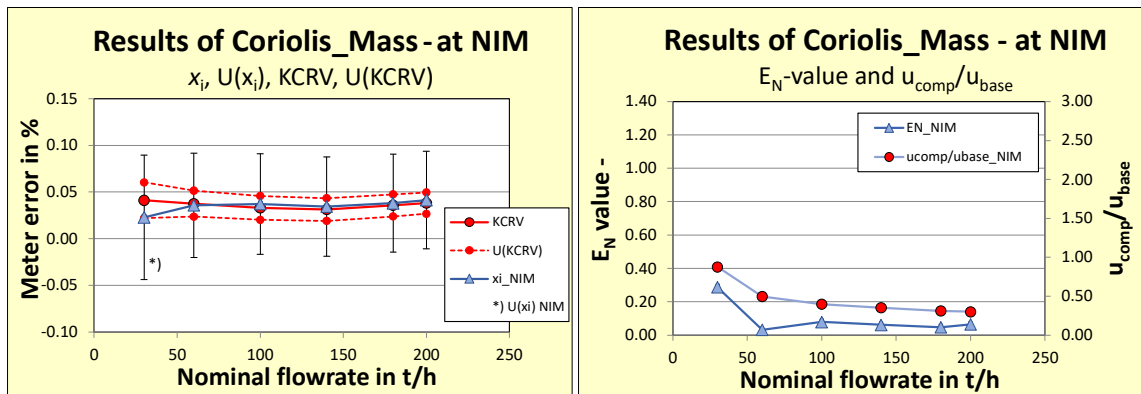


Figure 67: Comparison results of NIM/P.R. China laboratory for Coriolis_Mass transfer meter

NMIJ - laboratory (Japan)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 47).

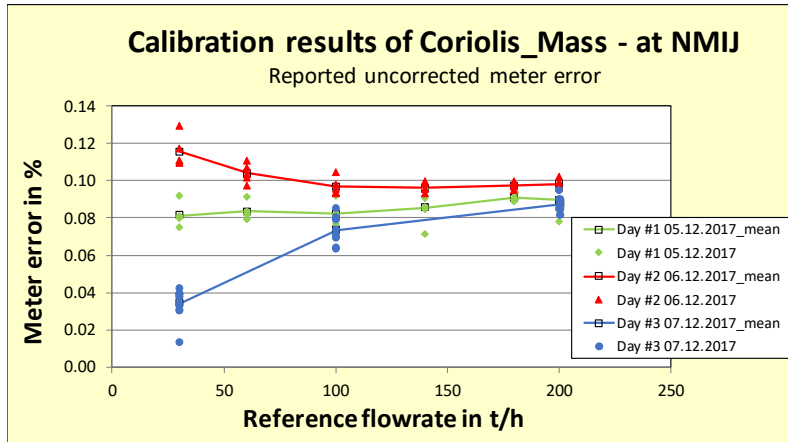


Figure 68: Comparison results of NMIJ for Coriolis_Mass transfer meter – reported uncorrected meter error e_m

Table 47: Comparison decision table for NMIJ laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2)

NMIJ / Japan							
Nominal flowrate	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{comp}/u_{base}	CMC decision status
	x_i	$U_{base,i} (k=2)$	$U(x_i) (k=2)$	d_i	$E_{N,i}$		
in t/h	in %	in %	in %	-	-	-	
30	0.074	0.042	0.062	0.032	0.55	1.08	acceptable
60	0.055	0.042	0.049	0.018	0.38	0.61	acceptable
100	0.058	0.042	0.047	0.025	0.55	0.49	acceptable
140	0.060	0.042	0.046	0.029	0.65	0.43	acceptable
180	0.067	0.042	0.045	0.031	0.72	0.37	acceptable
200	0.067	0.042	0.045	0.029	0.67	0.37	acceptable

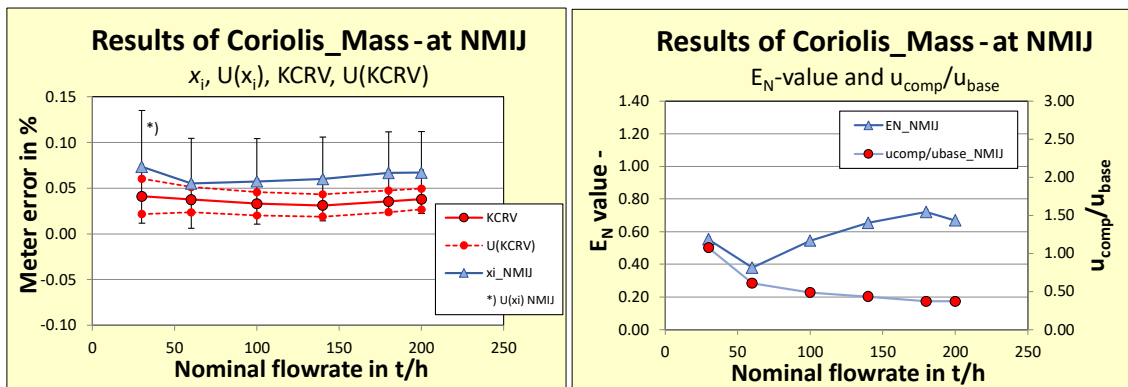


Figure 69: Comparison results of NMIJ/Japan laboratory for Coriolis_Mass transfer meter

KRISS-laboratory (Korea)

For mass calibration this comparison supported the declared base uncertainties of the participant (Table 48).

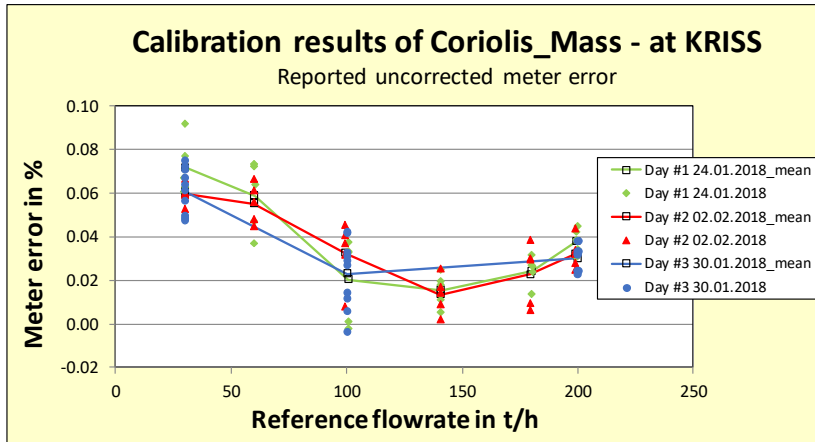


Figure 70: Comparison results of KRISS for Coriolis_Mass transfer meter - reported uncorrected meter error e_m

Table 48: Comparison decision table for KRISS laboratory (Coriolis_Mass transfer meter), where x_i is the temperature corrected meter error (mean of day #1 and day#2) - * represents E_N values at warning level

Nominal flowrate	KRISS / Korea						
	Relative measurement error	Expanded laboratory uncertainty	Expanded measurement uncertainty	Degree of equivalence	Normalized degree of equivalence	u_{TS}/u_{base}	CMC decision status
	x_i	$U_{base,i} (k=2)$	$U(x_i) (k=2)$	d_i	$E_{N,i}$		
in t/h	in %	in %	in %	-	-	-	
30	0.027	0.060	0.074	-0.015	0.20	0.74	acceptable
60	-0.002	0.060	0.065	-0.040	0.62	0.43	acceptable
100	-0.022	0.060	0.064	-0.055	0.87	0.38	acceptable
140	-0.032	0.060	0.063	-0.064	1.03 *	0.30	warning level
180	-0.017	0.060	0.062	-0.053	0.86	0.28	acceptable
200	-0.005	0.060	0.062	-0.043	0.71	0.26	acceptable

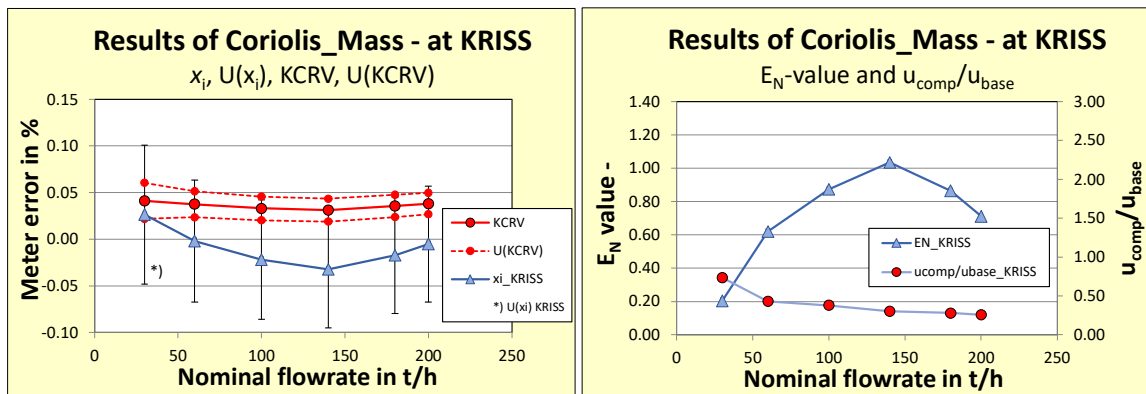


Figure 71: Comparison results of KRISS laboratory for Coriolis_Mass transfer meter

8 Nomenclature and unit symbols

Terms and abbreviations

APMP	Asia Pacific Metrology Programme
BIPM	Bureau International des Poids et Mesures
CCM	Consultative Committee for Mass and Related Quantities
CIPM	International Committee for Weights and Measures
CMC	Calibration and Measurement Capabilities
DI	Designated Institute
DN	Inner pipe diameter (mm)
DoE	Degree of Equivalence
EURAMET	The European Association of National Metrology Institutes
GUM	Guide to the Expression of Uncertainty in Measurement
FF	Fluid flow
KC1	Key comparison CCM.FF-K1.2015
KCRV	Key comparison reference value
MRA	(CIPM) Mutual Recognition Arrangement
NMI	National Metrology Institute
RMO	Regional Metrology Organisation
SIM	Interamerican Metrology System
TP	Technical Protocol
WGFF	(CCM) Working Group on Fluid Flow

Symbols and units

d_i	Degree of equivalence (DoE) for each laboratory i (%)
Δe_{nom}	Difference of meter error (%)
e	Meter error at current temperature conditions (%)
e_{cor}	Temperature corrected meter error (%)
Δe_{cor}	Correction value of meter error (%)
e_{mean}	Mean values of meter error at one flow rate over all temperatures (%)
$E_{N,i}$	Normalized Degree of Equivalence (-)
e_{nom}	Meter error at nominal temperature of 20 °C (%)
e_m	Relative measurement error of Coriolis meter (%)
$e_{m,cor}$	Temperature corrected measurement error of Coriolis meter (%)
$e_{residual}$	Model residuals (%)
e_v	Relative measurement error of turbine meter (%)
$e_{v,cor}$	Temperature corrected measurement error of turbine meter (%)
i	Laboratory index
k	Coverage factor (-)
K_m	meter K -factor - mass-related output (Coriolis meter) (pulses/kg)
$K_{m,nom}$	Nominal K -factor of Coriolis mass (pulses/kg)
K_v	meter K -factor - volume-related output (turbine meter) (pulses/L)
ΔK_v	Difference in meter K -factor of turbine meter (%)

$K_{V,nom}$	Nominal K -factor of turbine meter (pulses/L)
m_{ref}	Mass, measured by the reference standard (kg)
n	Number of calibrations (-)
N	Counted number of pulses of the transfer meter (pulses)
n_i	number of evaluated laboratories (-)
p_{fluid}	Line pressure (bar)
s	Standard deviation of the mean of measurements at one flowrate point (%)
T_{air}	Air temperature (°C)
T_{fluid}	Current fluid temperature (°C)
ΔT_{fluid}	Difference of current fluid temperature to nominal temperature of 20 °C (°C)
T_{nom}	Nominal temperature of 20°C
$u_{base,i}$	Standard uncertainty of laboratory refence (%)
u_{comp}	Standard uncertainty of transfer meter measurements (%)
u_{TS}	Standard uncertainty of transfer meter (%)
u_{drift}	Standard uncertainty due to drift of transfer meter (%)
u_{reprod}	Standard uncertainty due to reproducibility characteristics of transfer meter (%)
u_{temp}	Standard uncertainty caused by temperature characteristics of transfer meter (%)
u_{pres}	Standard uncertainty caused by pressure characteristics of transfer meter (%)
u_{flow}	Standard uncertainty due to sensitivity of transfer meter to instable flow conditions (%)
u_{inflow}	Standard uncertainty due to sensitivity of turbine meter to different inflow conditions (%)
u_{hyst}	Standard uncertainty due to hysteresis effect (%)
$U(KCRV)$	Expanded uncertainty of Key comparison reference value (%)
u_y	Standard uncertainty of y (%)
$U(y)$	Expanded uncertainty of y (%)
$u_{x,i}$	Standard uncertainty of reported and temperature corrected meter error (%)
V_{ref}	Volume, measured by the reference standard (m ³)
y	Reference value of the comparison (%)
x_i	Temperature corrected meter error for E_N -value evaluation
X_{KCRV}	Key Comparison Reference value (%)
ν	Degrees of freedom
X_{obs}^2	Observed chi-squared value
X_{ν}^2	Chi-squerred test value

9 References

- [1] *Technical Protocol for Key Comparison CCM.FF-K1.2015*. Draft 5/3. Unpublished. 23.01.2017
- [2] GUM - *Guide to the Expression of Uncertainty in Measurement*, JCGM 100:2008.
- [3] BIPM: *WGFF Guidelines for CMC Uncertainty and Calibration Report Uncertainty*. 21.10.2013, <http://www.bipm.org/utis/en/pdf/ccm-wgff-guidelines.pdf>
- [4] WRIGHT, J. et al. (2016): *Transfer standard uncertainty can cause inconclusive inter-laboratory comparisons*. Metrologia 53 (2016) 1243 - 1258
- [5] Cox M. G.: *Evaluation of key comparison data*, Metrologia 39 (2002) 589 - 595
- [6] Cox M. G.: *The evaluation of key comparison data: determining the largest consistent subset*, Metrologia 44 (2007) 187 - 200

10 Appendices

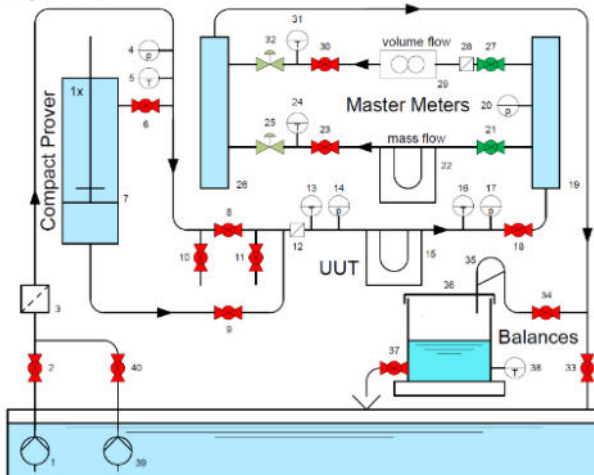
10.1 Information about participating laboratories

NMI/DI	Country	RMO	Contact	Address
NEL	UK	EURAMET	Christopher Mills Chris.Mills@ tuvsud.com	TÜV SÜD National Engineering Laboratory Scottish Enterprise Technology Park, East Kilbride Glasgow G75 0QF, United Kingdom
VSL	Netherlands	EURAMET	F. M. Smits fsmits@ vsl.nl	VSL - Dutch Metrology Institute Thijssesweg 11 2629 JA Delft, Netherlands
RISE	Sweden	EURAMET	Oliver Büker oliver.buker@ ri.se	RISE - Research Institutes of Sweden Measurement Science and Technology Brinellgatan 4 SE-504 62 Borås, Sweden
PTB	Germany	EURAMET	Enrico Frahm enrico.frahm@ ptb.de	PTB - Physikalisch-Technische Bundesanstalt Department 1.5 Liquid Flow Bundesallee 100 38116 Braunschweig, Germany
UME	Turkey	EURAMET	Başak Akselli basak.akselli@ tubitak.gov.tr	UME - Ulusal Metroloji Enstitüsü, TUBITAK UME Akiskanlar Laboratuvarlari Baris Mah. Dr. Zeki Acar cad. No: 1 41470 Gebze / Kocaeli, Turkey
NIST	USA	SIM/ Noramet	Iosif Shinder iosif.shinder@ nist.gov	NIST - National Institute of Standards and Technology 100 Bureau Dr Gaithersburg, MD 20899, USA
CENAM	Mexico	SIM/ Noramet	Roberto Arias Romero rarias@ cenam.mx	CENAM - Centro Nacional de Metrología km 4.5 carretera a los Cués, El Marqués, Qro. México, CP 76246
ITRI	Chinese Taipei	APMP	Cheng-Tsair Yang ctyang@ itri.org.tw	ITRI - Industrial Technology Research Institute Center for Measurement Standards Bldg. 16, No. 321, Sec. 2, Kuang-Fu Rd. Hsinchu, Chinese Taipei 30044
NIM	P.R. China	APMP	Tao Meng mengt@ nim.ac.cn	NIM - National Institute of Metrology Division of Thermometry and Material Evaluation No.18 Bei San Huan Dong Lu, Chaoyang District Beijing, 100029, P.R. China
NMIJ/AIST	Japan	APMP	Noriyuki Furuichi furuichi.noriyuki@ aist.go.jp	NMIJ/AIST - National Institute of Advanced Industrial Science and Technology National Metrology Institute of Japan Fluid Flow Division AIST Tsukuba Central 3, 1-1-1 Umezono Tsukuba 305-8563, Japan
KRISS	Korea	APMP	Sejong Chun sjchun@ kriss.re.kr	KRISS - Korea Research Institute of Standards and Science Thermometry and Fluid Flow Metrology Group Division of Physical Metrology 205A-dong 101-ho, Gajeong-ro 267, Yuseong-gu Daejeon 34113, South Korea

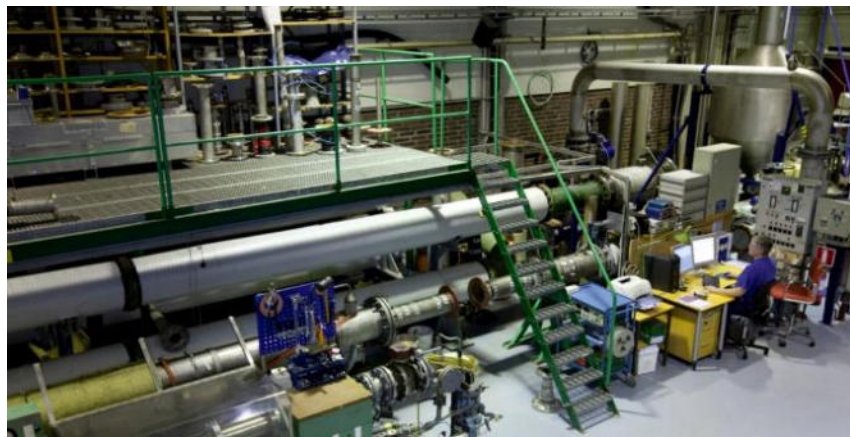
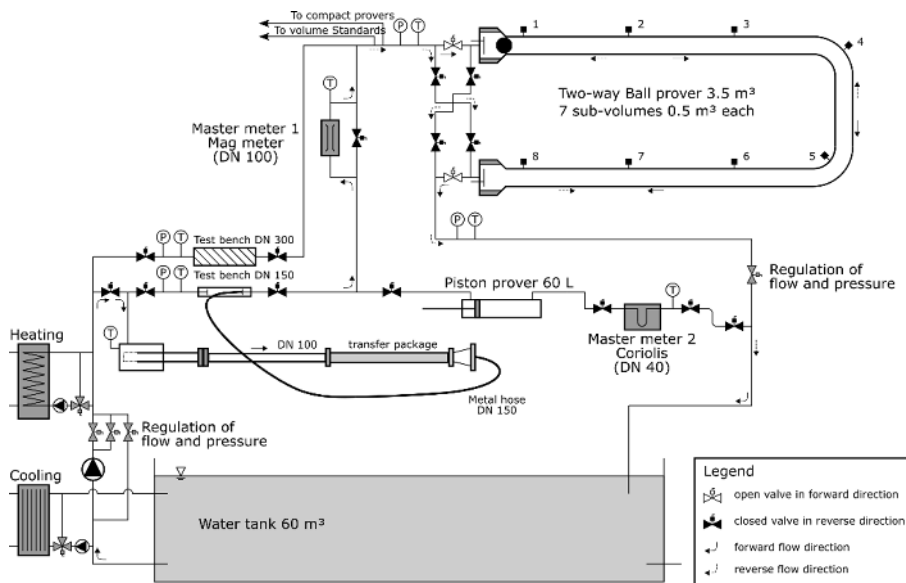
Characteristic information of primary standard used during KC		Working procedure																
VSL – Netherlands <table border="1"> <tr> <td>Range of flowrate</td> <td>0.001 m³/h ... 400 m³/h</td> </tr> <tr> <td>Fluid temperature</td> <td>Ambient 15 °C ... 25 °C</td> </tr> <tr> <td>Line pressure</td> <td>1 bar(g) 5 bar(g)</td> </tr> <tr> <td>Uncertainty (k = 2)</td> <td>0.02% volume and mass for gravimetric and prover 0.04% master meter</td> </tr> <tr> <td>Reference</td> <td>Gravimetric, prover, master meters</td> </tr> <tr> <td>Operating method</td> <td>Dynamic for prover and master meter. Standing start-stop for gravimetric</td> </tr> <tr> <td>Calibration line diameter</td> <td>3 mm ... 200 mm</td> </tr> <tr> <td>Test fluid</td> <td>water</td> </tr> </table>		Range of flowrate	0.001 m ³ /h ... 400 m ³ /h	Fluid temperature	Ambient 15 °C ... 25 °C	Line pressure	1 bar(g) 5 bar(g)	Uncertainty (k = 2)	0.02% volume and mass for gravimetric and prover 0.04% master meter	Reference	Gravimetric, prover, master meters	Operating method	Dynamic for prover and master meter. Standing start-stop for gravimetric	Calibration line diameter	3 mm ... 200 mm	Test fluid	water	<p>The VSL Water Flow facility (WF) represents the national standard of the Netherlands for the realization of the measurands volumetric and mass flow rate as well as the total volume and mass of flowing liquids (water). The gravimetric system utilized during the comparison has a standing start-stop method with five weighing scales and transfer points. Maximum loads of 10 t, 3.5 t, 600 kg, 70 kg and 6 kg. The dynamic system consists of a prover and seven master meters (three turbine meters and four Coriolis mass flow meters). For generating and stabilizing flow rates, the supply system consists of a 190 m³ storage tank, and two frequency-controlled pumps. The facility has two Meter Under Test sections at different locations in the facility. The maximum build in length is 9 meters. The fluid temperature is ambient with the concrete tank generating cooling from the surrounding soil to keep temperature stable during calibration runs.</p>
Range of flowrate	0.001 m ³ /h ... 400 m ³ /h																	
Fluid temperature	Ambient 15 °C ... 25 °C																	
Line pressure	1 bar(g) 5 bar(g)																	
Uncertainty (k = 2)	0.02% volume and mass for gravimetric and prover 0.04% master meter																	
Reference	Gravimetric, prover, master meters																	
Operating method	Dynamic for prover and master meter. Standing start-stop for gravimetric																	
Calibration line diameter	3 mm ... 200 mm																	
Test fluid	water																	



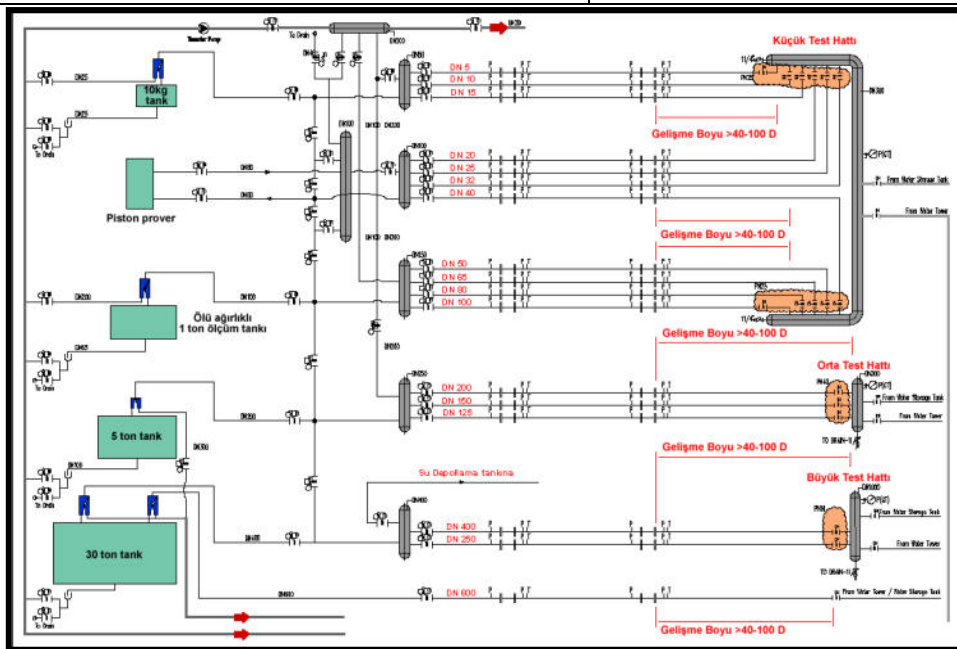
Simplified P&ID



Characteristic information of primary standard used during KC	Working procedure																
<p>RISE – Sweden</p> <table border="1"> <tr> <td data-bbox="204 353 491 387">Range of flowrate</td> <td data-bbox="491 353 778 387">6 m³/h to 720 m³/h</td> </tr> <tr> <td data-bbox="204 387 491 421">Fluid temperature</td> <td data-bbox="491 387 778 421">15 °C to 90 °C</td> </tr> <tr> <td data-bbox="204 421 491 454">Line pressure</td> <td data-bbox="491 421 778 454">up to 8 bar</td> </tr> <tr> <td data-bbox="204 454 491 521">Uncertainty (k = 2)</td> <td data-bbox="491 454 778 521">0.06% (volume flow) 0.08% (mass flow)</td> </tr> <tr> <td data-bbox="204 521 491 689">Reference</td> <td data-bbox="491 521 778 689">Ball prover 3.5 m³ Fixed volume standards with 1000 L or 3500 L BCP 12" (20 L and 60 L) BCP 24" (250 L)</td> </tr> <tr> <td data-bbox="204 689 491 790">Operating method</td> <td data-bbox="491 689 778 790">Direct pumping, Flying- / standing- start-and-stop</td> </tr> <tr> <td data-bbox="204 790 491 857">Calibration line diameter</td> <td data-bbox="491 790 778 857">DN 40 (1 1/2") to DN 300 (12")</td> </tr> <tr> <td data-bbox="204 857 491 891">Test fluid</td> <td data-bbox="491 857 778 891">water (and kerosene)</td> </tr> </table>	Range of flowrate	6 m ³ /h to 720 m ³ /h	Fluid temperature	15 °C to 90 °C	Line pressure	up to 8 bar	Uncertainty (k = 2)	0.06% (volume flow) 0.08% (mass flow)	Reference	Ball prover 3.5 m³ Fixed volume standards with 1000 L or 3500 L BCP 12" (20 L and 60 L) BCP 24" (250 L)	Operating method	Direct pumping, Flying- / standing- start-and-stop	Calibration line diameter	DN 40 (1 1/2") to DN 300 (12")	Test fluid	water (and kerosene)	<p>VM4 represents one of the national primary standards of Sweden for the realization of the measurands volumetric and mass flow rate as well as the total volume and mass of water and kerosene. Traceability at low flow is realized by means of a compact piston prover with volumes of 20 L and 60 L and at high flow rates with a ball prover with a volume of 0.5 m³ to 3.5 m³. In addition, VM4 offers the possibility for direct calibration against two (fixed) volume standards of 1000 L and 3500 L. The flow is generated from a 60 m³ storage tank by means of frequency-controlled pumps. For the measurements a >50 D straight inlet section was provided upstream the transfer package. The fluid temperature (stability better ±0.2 K) is adjusted and controlled by a heating and cooling system.</p>
Range of flowrate	6 m ³ /h to 720 m ³ /h																
Fluid temperature	15 °C to 90 °C																
Line pressure	up to 8 bar																
Uncertainty (k = 2)	0.06% (volume flow) 0.08% (mass flow)																
Reference	Ball prover 3.5 m³ Fixed volume standards with 1000 L or 3500 L BCP 12" (20 L and 60 L) BCP 24" (250 L)																
Operating method	Direct pumping, Flying- / standing- start-and-stop																
Calibration line diameter	DN 40 (1 1/2") to DN 300 (12")																
Test fluid	water (and kerosene)																



Characteristic information of primary standard used during KC		Working procedure
UME – Turkey		<p>The UME Water Flow Measurement Laboratory represents the national primary standard of Turkey for the realization of the measures volumetric and mass flow rate as well as the total volume and mass of flowing liquids (water).</p> <p>The gravimetric reference consists of four independent diverter and balance systems with max. loads of 30 t, 5 t, 1 t and 10 kg. For generating and stabilizing flow rates, the supply system consists of a 300 m³ storage tank, of a frequency controlled pumping system, a constant head tank (50 m³, 15 m³ and 5 m³, at a height of 35 m) and 16 calibration lines. For each diameter an upstream straight pipeline with a length of 50D and downstream of 20D is available.</p>
Range of flowrate	0.01 m ³ /h ... 2,000 m ³ /h	
Fluid temperature	10 °C ... 35 °C	
Line pressure	1 bar ... 6 bar	
Uncertainty (k = 2)	0.04 % volume, mass	
Reference	gravimetric	
Operating method	Direct pumping, constant head tank flying-/ standing-start-stop	
Calibration line diameter	5 mm ... 400 mm	
Test fluid	water	



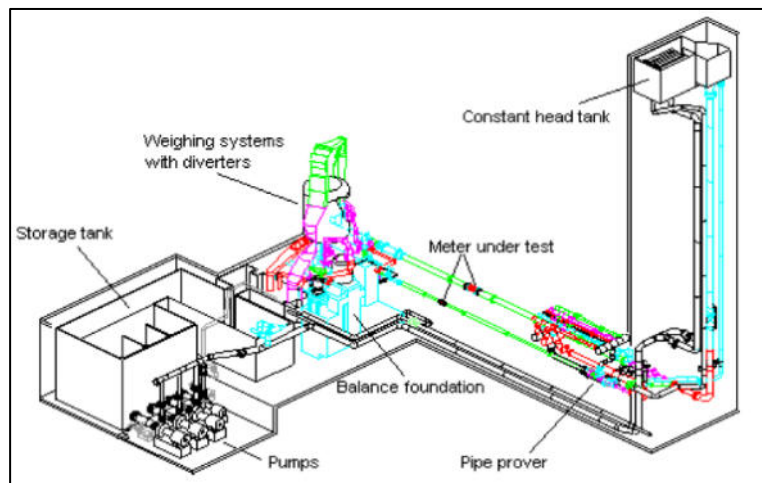
Characteristic information of primary standard used during KC		Working procedure																
PTB – Germany <table border="1"> <tr> <td>Range of flowrate</td> <td>0.3 m³/h ... 2,100 m³/h</td> </tr> <tr> <td>Fluid temperature</td> <td>10 °C ... 35 °C</td> </tr> <tr> <td>Line pressure</td> <td>2 bar ... 6 bar</td> </tr> <tr> <td>Uncertainty (k = 2)</td> <td>0.02 volume, mass</td> </tr> <tr> <td>Reference</td> <td>gravimetric</td> </tr> <tr> <td>Operating method</td> <td>Direct pumping , constant head tank flying-/ standing-start-stop</td> </tr> <tr> <td>Calibration line diameter</td> <td>25 mm ... 400 mm</td> </tr> <tr> <td>Test fluid</td> <td>water</td> </tr> </table>		Range of flowrate	0.3 m ³ /h ... 2,100 m ³ /h	Fluid temperature	10 °C ... 35 °C	Line pressure	2 bar ... 6 bar	Uncertainty (k = 2)	0.02 volume, mass	Reference	gravimetric	Operating method	Direct pumping , constant head tank flying-/ standing-start-stop	Calibration line diameter	25 mm ... 400 mm	Test fluid	water	<p>The PTB hydrodynamic test field (HDP) represents the national primary standard of Germany for the realization of the measurands volumetric and mass flow rate as well as the total volume and mass of flowing liquids (water).</p> <p>The gravimetric reference consists of three independent diverter and balance systems with max. loads of 30 t, 3 t and 300 kg. For generating and stabilizing flow rates, the supply system consists of a 400 m³ storage tank, of a frequency controlled pumping system, a constant head tank (30 m³, at a height of 30 m) and two calibration lines. For each diameter an upstream straight pipeline with a length of 50D and downstream of 20D is available. The fluid temperature is adjusted and controlled by two separate heat exchanger systems.</p>
Range of flowrate	0.3 m ³ /h ... 2,100 m ³ /h																	
Fluid temperature	10 °C ... 35 °C																	
Line pressure	2 bar ... 6 bar																	
Uncertainty (k = 2)	0.02 volume, mass																	
Reference	gravimetric																	
Operating method	Direct pumping , constant head tank flying-/ standing-start-stop																	
Calibration line diameter	25 mm ... 400 mm																	
Test fluid	water																	



Upstream view to calibration lines



3 t balance and diverter system



Principle drawing of the Hydrodynamic Test Field

Characteristic information of primary standard used during KC	Working procedure																
<p>NIST – USA</p> <table border="1"> <tr> <td data-bbox="204 353 464 387">Range of flowrate</td> <td data-bbox="464 353 699 387">0.7 kg/s-65 kg/s</td> </tr> <tr> <td data-bbox="204 387 464 421">Fluid temperature</td> <td data-bbox="464 387 699 421">20°C to 40°C</td> </tr> <tr> <td data-bbox="204 421 464 488">Line pressure</td> <td data-bbox="464 421 699 488">300 kPa to 700 kPa</td> </tr> <tr> <td data-bbox="204 488 464 521">Uncertainty ($k = 2$)</td> <td data-bbox="464 488 699 521">0.033%</td> </tr> <tr> <td data-bbox="204 521 464 555">Reference</td> <td data-bbox="464 521 699 555">Gravimetric</td> </tr> <tr> <td data-bbox="204 555 464 656">Operating method</td> <td data-bbox="464 555 699 656">Static, Flying start and stop Gravimetric</td> </tr> <tr> <td data-bbox="204 656 464 723">Calibration line diameter</td> <td data-bbox="464 656 699 723">100 mm</td> </tr> <tr> <td data-bbox="204 723 464 757">Test fluid</td> <td data-bbox="464 723 699 757">Water</td> </tr> </table>	Range of flowrate	0.7 kg/s-65 kg/s	Fluid temperature	20°C to 40°C	Line pressure	300 kPa to 700 kPa	Uncertainty ($k = 2$)	0.033%	Reference	Gravimetric	Operating method	Static, Flying start and stop Gravimetric	Calibration line diameter	100 mm	Test fluid	Water	<p>NIST Water Flow Measurement Standard (WFCF) has three parallel pipelines with diameters of 100, 200 and 400 mm and weighing system with capacity 3700 kg. Part of the WFCF which includes a 3700 kg collection tank and a 100 mm pipeline was used for key comparison. The WFCF uses two methods: (1) the static gravimetric method and an error-free uni-directional diverter with a collection/bypass unit to perform water flowmeter calibrations and (2) dynamic gravimetric method. Flow generation system comprised of storage tank, pumping system, and a flow control system which actuates the control valves. The flow generation system produces the water flow through the test section at the constant rate required for test point series necessary for a calibration.</p>
Range of flowrate	0.7 kg/s-65 kg/s																
Fluid temperature	20°C to 40°C																
Line pressure	300 kPa to 700 kPa																
Uncertainty ($k = 2$)	0.033%																
Reference	Gravimetric																
Operating method	Static, Flying start and stop Gravimetric																
Calibration line diameter	100 mm																
Test fluid	Water																



Characteristic information of primary standard used during KC	Working procedure																
<p>CENAM – Mexico</p> <table border="1"> <tr> <td data-bbox="204 353 427 387">Range of flow rate</td> <td data-bbox="427 353 778 387">(100... 12 000) kg/min</td> </tr> <tr> <td data-bbox="204 387 427 421">Fluid temperature</td> <td data-bbox="427 387 778 421">Ambient (not controlled) (15...27) °C</td> </tr> <tr> <td data-bbox="204 421 427 454">Line pressure</td> <td data-bbox="427 421 778 454">up to 10 bar</td> </tr> <tr> <td data-bbox="204 454 427 499">Uncertainty</td> <td data-bbox="427 454 778 499">$U(q_m)/\% = 0.030$ $U(q_v)/\% = 0.038$ $k = 2$</td> </tr> <tr> <td data-bbox="204 499 427 533">Reference</td> <td data-bbox="427 499 778 533">Gravimetric</td> </tr> <tr> <td data-bbox="204 533 427 566">Operating method</td> <td data-bbox="427 533 778 566">Flying start and stop</td> </tr> <tr> <td data-bbox="204 566 427 611">Calibration line diameter</td> <td data-bbox="427 566 778 611">100 mm 200 mm</td> </tr> <tr> <td data-bbox="204 611 427 645">Test fluid</td> <td data-bbox="427 611 778 645">Water</td> </tr> </table>	Range of flow rate	(100... 12 000) kg/min	Fluid temperature	Ambient (not controlled) (15...27) °C	Line pressure	up to 10 bar	Uncertainty	$U(q_m)/\% = 0.030$ $U(q_v)/\% = 0.038$ $k = 2$	Reference	Gravimetric	Operating method	Flying start and stop	Calibration line diameter	100 mm 200 mm	Test fluid	Water	<p>The Mexican Primary Measurement System for Water Flow is of the Static Weighing Design.</p> <p>The gravimetric reference consists of two independent diverter and weighing systems; which maximum load capacities are 1500 kg and 10 000 kg, respectively.</p> <p>Flow is controlled by means of frequency converter and throttling valves.</p> <p>More than $100D$ upstream pipe length is available for calibrations.</p> <p>No fluid temperature control available.</p>
Range of flow rate	(100... 12 000) kg/min																
Fluid temperature	Ambient (not controlled) (15...27) °C																
Line pressure	up to 10 bar																
Uncertainty	$U(q_m)/\% = 0.030$ $U(q_v)/\% = 0.038$ $k = 2$																
Reference	Gravimetric																
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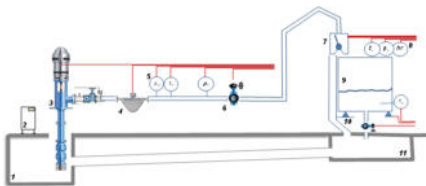


Fig. 1: Schematic diagram of CENAM water flow facility

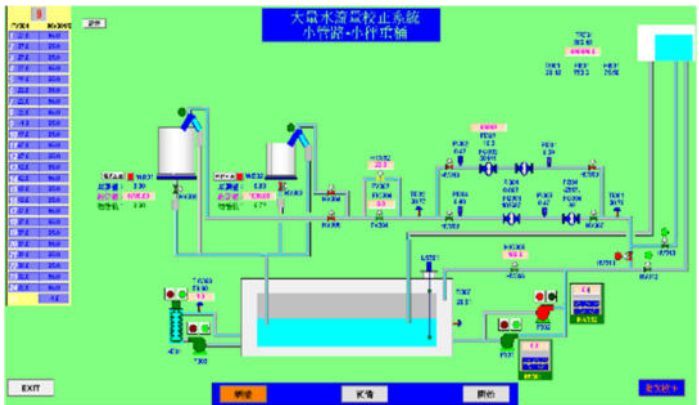
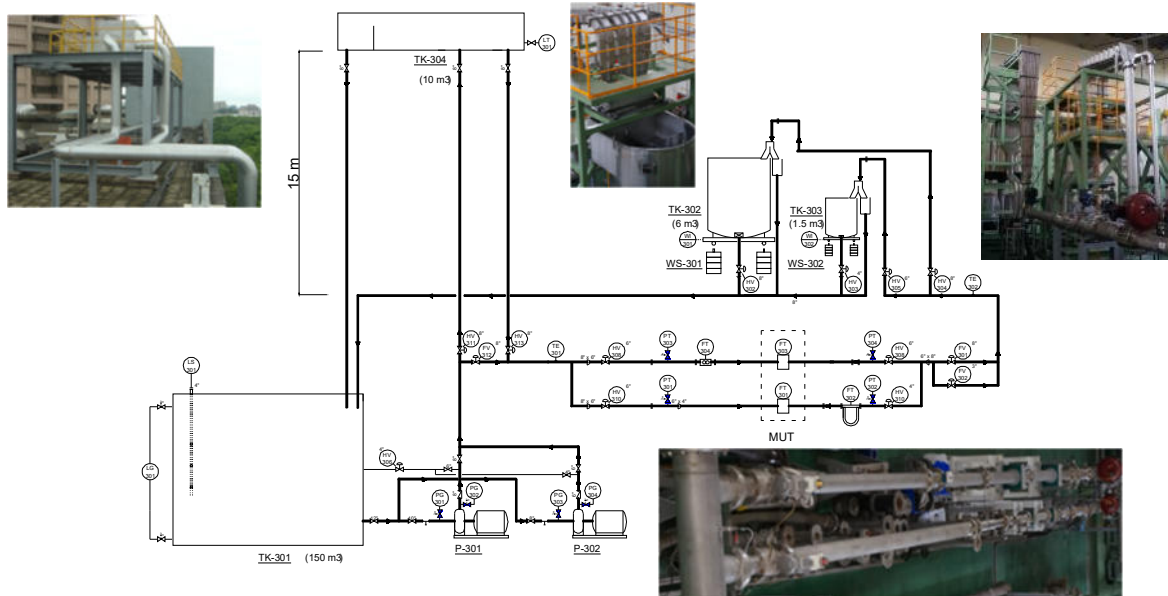


Fig. 2: A view of the load cell at the 10 000 kg tank



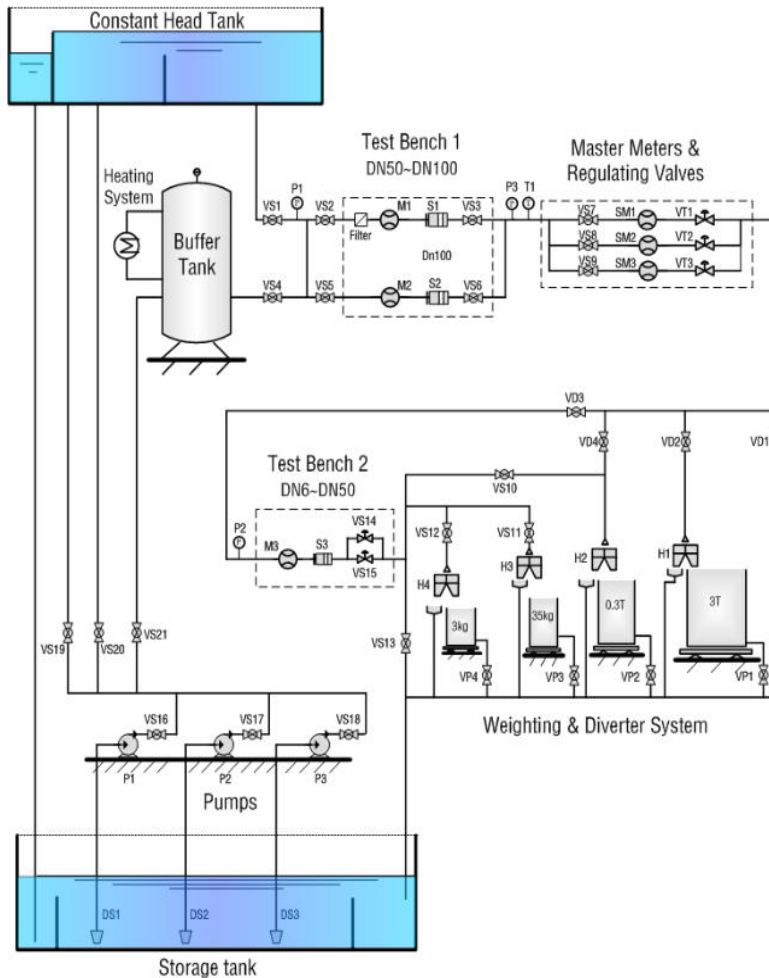
Fig. 3: Front view of the static weighing system at CENAM Primary System for Water Flow

Characteristic information of primary standard used during KC	Working procedure																
<p>ITRI – Chinese Taipei</p> <table border="1"> <tr> <td>Range of flowrate</td> <td>1.8 m³/h to 480 m³/h</td> </tr> <tr> <td>Fluid temperature</td> <td>15 °C to 35 °C</td> </tr> <tr> <td>Line pressure</td> <td>40 kPa to 500 kPa</td> </tr> <tr> <td>Uncertainty ($k = 2$)</td> <td>$U_{CMC,V} = 0.04 \%$</td> </tr> <tr> <td>Reference</td> <td>Weighing platform 6000 kg & 1500 kg</td> </tr> <tr> <td>Operating method</td> <td>Static weighing method with flying-start-and-finish Operating mode</td> </tr> <tr> <td>Calibration line diameter</td> <td>50 mm to 300 mm</td> </tr> <tr> <td>Test fluid</td> <td>Tap water</td> </tr> </table>	Range of flowrate	1.8 m ³ /h to 480 m ³ /h	Fluid temperature	15 °C to 35 °C	Line pressure	40 kPa to 500 kPa	Uncertainty ($k = 2$)	$U_{CMC,V} = 0.04 \%$	Reference	Weighing platform 6000 kg & 1500 kg	Operating method	Static weighing method with flying-start-and-finish Operating mode	Calibration line diameter	50 mm to 300 mm	Test fluid	Tap water	<p>The primary standard adapts static weighing method with flying-start-and-finish mode to calibrate either quantity-type flowmeters or rate-type flowmeters. The water is pumped from the reservoir in the base room by a frequency controlled pump. Then the water flow directly through the meter under test, or flow to the constant head tank and the meter under test sequentially. The diverter is used to manipulate flow along the bypass loop or towards the weighing tank. When the predetermined flow quantity or the time interval for single test is achieved, the quantity of water accumulated in the tank is compared with that measured by the meter under test. Two weighing tanks are used as the references depending on the flow rate. Both quantity-type and rate-type flowmeters could be calibrated by the primary standard. The output of flowmeters could be volume, mass, volume flowrate, or mass flowrate.</p>
Range of flowrate	1.8 m ³ /h to 480 m ³ /h																
Fluid temperature	15 °C to 35 °C																
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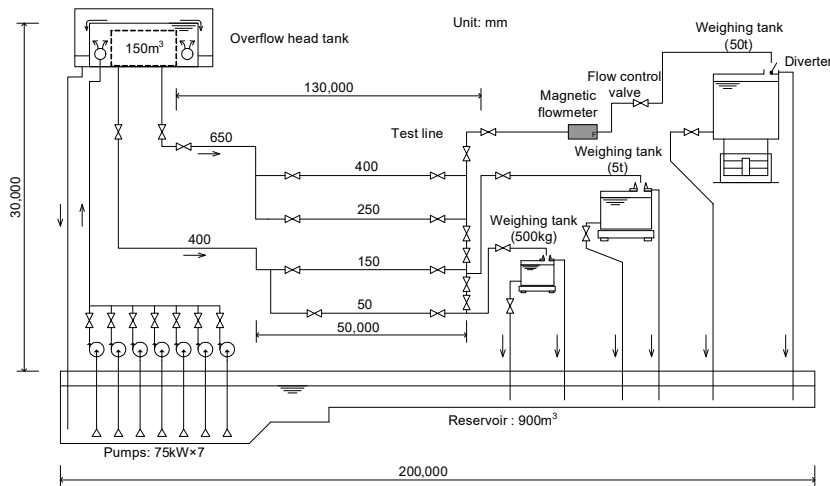
The water flow standard at ITRI

Characteristic information of primary standard used during KC	Working procedure																
<p>NIM – P.R. China</p> <table border="1"> <tr> <td data-bbox="204 353 491 387">Range of flowrate</td> <td data-bbox="491 353 778 387">10L/h ... 200m³/h</td> </tr> <tr> <td data-bbox="204 387 491 421">Fluid temperature</td> <td data-bbox="491 387 778 421">15°C ... 35°C</td> </tr> <tr> <td data-bbox="204 421 491 454">Line pressure</td> <td data-bbox="491 421 778 454">1bar ... 4bar</td> </tr> <tr> <td data-bbox="204 454 491 555">Uncertainty (k = 2)</td> <td data-bbox="491 454 778 555">0.05%</td> </tr> <tr> <td data-bbox="204 555 491 589">Reference</td> <td data-bbox="491 555 778 589">mass, volume</td> </tr> <tr> <td data-bbox="204 589 491 790">Operating method</td> <td data-bbox="491 589 778 790">gravimetric</td> </tr> <tr> <td data-bbox="204 790 491 857">Calibration line diameter</td> <td data-bbox="491 790 778 857">Direct pumping with buffer tank, constant head tank flying-start-stop</td> </tr> <tr> <td data-bbox="204 857 491 902">Test fluid</td> <td data-bbox="491 857 778 902">DN6 ... DN100 water</td> </tr> </table>	Range of flowrate	10L/h ... 200m ³ /h	Fluid temperature	15°C ... 35°C	Line pressure	1bar ... 4bar	Uncertainty (k = 2)	0.05%	Reference	mass, volume	Operating method	gravimetric	Calibration line diameter	Direct pumping with buffer tank, constant head tank flying-start-stop	Test fluid	DN6 ... DN100 water	<p>The cold-water flow facility of NIM is the Chinese national primary standard of water flow.</p> <p>It is a static gravimetric test facility. The gravimetric reference consists of four independent diverter-weighting systems with max. loads of 3t, 300 kg, 30kg and 3kg. For stabilizing flow rate, the supply system consists of three pumps, a head constant tank (about 18m high), a buffer tank and an underground water pool. Almost, the head constant tank is used when the flow below 160 m³/h, and the buffer tank can be used for the full flow range.</p>
Range of flowrate	10L/h ... 200m ³ /h																
Fluid temperature	15°C ... 35°C																
Line pressure	1bar ... 4bar																
Uncertainty (k = 2)	0.05%																
Reference	mass, volume																
Operating method	gravimetric																
Calibration line diameter	Direct pumping with buffer tank, constant head tank flying-start-stop																
Test fluid	DN6 ... DN100 water																



The water flow standard at NIM

Characteristic information of primary standard used during KC		Working procedure																
NMIJ/AIST – Japan <table border="1"> <tr> <td>Range of flowrate</td> <td>0.3 m³/h – 3,000 m³/h</td> </tr> <tr> <td>Fluid temperature</td> <td>Ambient (15 °C – 25 °C)</td> </tr> <tr> <td>Line pressure</td> <td>0.12 MPa – 0.24 MPa</td> </tr> <tr> <td>Uncertainty (k = 2)</td> <td>0.042% - 0.060% (mass, volume)</td> </tr> <tr> <td>Reference</td> <td>Gravimetric</td> </tr> <tr> <td>Operating method</td> <td>Overflow head tank, Weighing tank with double wing diverter</td> </tr> <tr> <td>Calibration line diameter</td> <td>25 mm - 400 mm</td> </tr> <tr> <td>Test fluid</td> <td>Water</td> </tr> </table>		Range of flowrate	0.3 m ³ /h – 3,000 m ³ /h	Fluid temperature	Ambient (15 °C – 25 °C)	Line pressure	0.12 MPa – 0.24 MPa	Uncertainty (k = 2)	0.042% - 0.060% (mass, volume)	Reference	Gravimetric	Operating method	Overflow head tank, Weighing tank with double wing diverter	Calibration line diameter	25 mm - 400 mm	Test fluid	Water	<p>The AIST water flow facility represents the national primary standard of Japan for the realization of the measurands volumetric and mass flow rate. The gravimetric reference consists of three independent diverter and balance systems with max. loads of 50 t, 5 t and 500 kg. For generating and stabilizing flow rates, the supply system consists of a 900 m³ storage tank, a overflow head tank (150 m³, at a height of 30 m) and four calibration lines. The straight pipe line lengths of each test line are 50 m. The fluid temperature is ambient but the stability of temperature is less than 1 °C during one day calibration.</p>
Range of flowrate	0.3 m ³ /h – 3,000 m ³ /h																	
Fluid temperature	Ambient (15 °C – 25 °C)																	
Line pressure	0.12 MPa – 0.24 MPa																	
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Reference	Gravimetric																	
Operating method	Overflow head tank, Weighing tank with double wing diverter																	
Calibration line diameter	25 mm - 400 mm																	
Test fluid	Water																	



Test line

The water flow standard at NMIJ



Weighing tank (5t)

Characteristic information of primary standard used during KC	Working procedure																
<p>KRISS – Korea</p> <table border="1"> <tr> <td>Range of flowrate</td> <td>10 L/h ... 2 000 m³/h</td> </tr> <tr> <td>Fluid temperature</td> <td>10 °C ... 40 °C</td> </tr> <tr> <td>Line pressure</td> <td>3 bar (typically, at 230 kPa)</td> </tr> <tr> <td>Uncertainty (<i>k</i> = 2)</td> <td>0.06 % (previously, 0.08 %) Volume flow, Mass flow</td> </tr> <tr> <td>Reference</td> <td>Gravimetric</td> </tr> <tr> <td>Operating method</td> <td>Constant head tank, Direct pumping, Flying-start-and-finish (Standing-start-and-finish possible, but not used)</td> </tr> <tr> <td>Calibration line diameter</td> <td>10 mm ... 400 mm</td> </tr> <tr> <td>Test fluid</td> <td>water</td> </tr> </table>	Range of flowrate	10 L/h ... 2 000 m ³ /h	Fluid temperature	10 °C ... 40 °C	Line pressure	3 bar (typically, at 230 kPa)	Uncertainty (<i>k</i> = 2)	0.06 % (previously, 0.08 %) Volume flow, Mass flow	Reference	Gravimetric	Operating method	Constant head tank, Direct pumping, Flying-start-and-finish (Standing-start-and-finish possible, but not used)	Calibration line diameter	10 mm ... 400 mm	Test fluid	water	<p>The water flow standard system at KRISS consists of a constant-level head tank, five weighing tanks, a reservoir, four pumps, six flow control units, six flow diverters, six weighbridges, ten test pipelines, and ten reference flow meters. The constant-level head tank is located at 20 m high from the ground level. Its height is 3 m. Thus, water pressure can be maintained at 230 kPa. The weight-bridges can collect water into the weighing tanks depending on the weighing capacity of 25 000 kg, 5 000, 1 000 kg, 100 kg, 64 kg and 6 kg. The straight pipelines have diameters from 10 mm to 400 mm. The biggest pipeline (400 mm) is directly connected from the head tank. A header is connected to the other pipelines (10 mm to 250 mm) to supply water from the head tank to the pipelines. The flow diverters are operated by the flying-start-and-finish method according to ISO 4185:1980.</p>
Range of flowrate	10 L/h ... 2 000 m ³ /h																
Fluid temperature	10 °C ... 40 °C																
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Calibration line diameter	10 mm ... 400 mm																
Test fluid	water																



The water flow standard system at KRISS

RISE Laboratory – Day#1

Table with columns: Date, Nominal flowrate, Measurement time, Laboratory reference (Standard mass flowrate, Standard volume flowrate, Mass, Volume), Fluid (Water density, Line pressure, Water temp, Air temp, Air pressure), Turbine meter (Kv, Pulse count, Meter error), Coriolis_Mass (Kv, Pulse count, Meter error), Coriolis_Vol (Kv, Pulse count, Meter error), Temperature correction of meter error (T_nom, Corrected meter error).

RISE Laboratory – Day#2

Date	Nominal flowrate V_{nom} [m ³ /h]	Laboratory reference						Fluid			Ambient conditions			Turbine meter			Coriolis_Mass			Coriolis_Vol			Temperature correction of meter error		
		Measur- ement time t	Standard mass flowrate m_{ref}^* [kg/h]	Standard volume flowrate V_{ref}^* [m ³ /h]	Mass m_{ref} [kg]	Volume V_{ref} [m ³]	Water density ρ_{fluid} [kg/m ³]	Line pressure P_{fluid} [bar]	Water temp. T_{fluid} [°C]	Air temp. T_{air} [°C]	Air pressure P_{air} [bar]	Pulse count N	K-factor K _v [Pulses/liter]	Meter error e _v [%]	Pulse count N	K-factor K _m [Pulses/kg]	Meter error e _m [%]	K _{nom} 63.2560 Pulses/ Liter	Pulse count N	K-factor K _v [Pulses/Liter]	Meter error e _v [%]	(T _{fluid} - T _{nom}) ΔT_{fluid} [°C]	Turbine meter e _{Vcor} [%]	Corrected meter error	Coriolis_Mass e _{Mass} [%]
25.02.2016	30	421.885	29.915	29.966	3500.808	3.507	998.298	3.06	19.94	19.94	23312.853	6.6479	0.225	23316.659	6.6479	0.225	350929.0287	100.0716	0.072	-0.060	0.210	0.031	0.031		
25.02.2016	30	421.306	29.972	29.972	3501.685	3.508	998.297	3.06	19.94	19.94	23319.183	6.6481	0.228	23319.979	6.6481	0.228	351099.9749	100.0716	0.072	-0.060	0.213	0.029	0.029		
25.02.2016	30	421.389	29.908	29.959	3500.830	3.507	998.296	3.06	19.95	19.95	23313.3276	6.6481	0.228	23313.3276	6.6481	0.228	351099.9749	100.0716	0.072	-0.060	0.216	0.039	0.039		
25.02.2016	30	422.577	29.831	29.882	3501.684	3.508	998.295	3.06	19.95	19.95	23319.9500	6.6483	0.231	23319.9500	6.6483	0.231	351029.9425	100.0753	0.075	-0.050	0.215	0.035	0.035		
25.02.2016	30	421.809	29.878	29.929	3500.804	3.507	998.294	3.06	19.97	19.97	23316.6542	6.6490	0.241	23316.6542	6.6490	0.241	350921.6138	100.0694	0.069	-0.030	0.227	0.029	0.029		
25.02.2016	60	213.317	59.081	59.182	3500.816	3.507	998.295	3.11	19.95	19.95	23340.9920	6.6558	0.344	23340.9920	6.6558	0.344	350947.3464	100.0768	0.077	-0.050	0.249	0.035	0.035		
25.02.2016	60	213.003	59.182	59.284	3501.663	3.508	998.296	3.11	19.95	19.95	23346.1226	6.6558	0.344	23346.1226	6.6558	0.344	350947.3464	100.0768	0.077	-0.050	0.249	0.035	0.035		
25.02.2016	60	213.065	59.150	59.230	3500.800	3.507	998.297	3.12	19.94	19.94	23342.2508	6.6558	0.351	23342.2508	6.6558	0.351	350979.8705	100.0719	0.072	-0.060	0.256	0.030	0.030		
25.02.2016	60	212.831	59.230	59.332	3501.673	3.508	998.296	3.11	19.96	19.96	23346.3144	6.6558	0.344	23346.3144	6.6558	0.344	350997.7648	100.0663	0.066	-0.040	0.249	0.024	0.024		
25.02.2016	60	212.986	59.172	59.273	3500.780	3.507	998.292	3.12	19.97	19.97	23342.5805	6.6564	0.353	23342.5805	6.6564	0.353	350941.2756	100.0750	0.075	-0.030	0.258	0.033	0.033		
25.02.2016	100	126.303	99.779	99.953	3500.677	3.507	998.282	3.04	20.11	20.11	23357.6458	6.6607	0.418	23357.6458	6.6607	0.418	350879.5584	100.0625	0.063	0.110	0.415	0.020	0.020		
25.02.2016	100	126.001	100.044	100.218	3501.568	3.508	998.264	3.04	20.11	20.11	23363.7491	6.6608	0.419	23363.7491	6.6608	0.419	350979.8538	100.0611	0.061	0.110	0.416	0.018	0.018		
25.02.2016	100	125.979	100.037	100.211	3500.704	3.507	998.262	3.05	20.12	20.12	23357.7172	6.6607	0.418	23357.7172	6.6607	0.418	350892.4955	100.0625	0.063	0.120	0.415	0.018	0.018		
25.02.2016	100	126.105	99.961	100.135	3501.537	3.508	998.256	3.04	20.15	20.15	23363.4465	6.6607	0.418	23363.4465	6.6607	0.418	350985.1137	100.0663	0.063	0.150	0.415	0.020	0.020		
25.02.2016	100	126.260	99.813	99.988	3500.664	3.507	998.257	3.04	20.13	20.13	23358.9200	6.6611	0.424	23358.9200	6.6611	0.424	350911.2232	100.0664	0.066	0.130	0.421	0.024	0.024		
25.02.2016	140	89.938	140.123	140.367	3500.657	3.507	998.259	3.01	20.13	20.13	23379.7619	6.6671	0.514	23379.7619	6.6671	0.514	350879.3614	100.0681	0.068	0.130	0.510	0.024	0.024		
25.02.2016	140	89.786	140.395	140.639	3501.534	3.508	998.261	3.00	20.12	20.12	23383.1341	6.6664	0.504	23383.1341	6.6664	0.504	350960.4633	100.0562	0.056	0.120	0.499	0.016	0.016		
25.02.2016	140	89.818	140.311	140.555	3500.686	3.507	998.262	3.01	20.11	20.11	23379.0461	6.6668	0.510	23379.0461	6.6668	0.510	350892.1413	100.0625	0.062	0.110	0.505	0.022	0.022		
25.02.2016	140	89.774	140.414	140.659	3501.545	3.508	998.264	3.00	20.11	20.11	23382.7985	6.6663	0.502	23382.7985	6.6663	0.502	350960.3187	100.0562	0.056	0.110	0.498	0.017	0.017		
25.02.2016	140	89.770	140.386	140.630	3500.686	3.507	998.265	3.02	20.10	20.10	23379.2141	6.6669	0.511	23379.2141	6.6669	0.511	350889.9674	100.0610	0.061	0.100	0.507	0.021	0.021		
25.02.2016	180	70.342	179.196	179.470	3500.617	3.507	998.255	3.06	20.16	20.16	23401.5258	6.6733	0.608	23401.5258	6.6733	0.608	350870.7644	100.0560	0.056	0.160	0.606	0.025	0.025		
25.02.2016	180	70.288	179.390	179.705	3501.501	3.508	998.252	3.03	20.17	20.17	23407.2206	6.6733	0.608	23407.2206	6.6733	0.608	350945.6819	100.0525	0.052	0.170	0.606	0.021	0.021		
25.02.2016	180	70.296	179.318	179.633	3501.479	3.508	998.248	3.05	20.19	20.19	23405.6528	6.6728	0.602	23405.6528	6.6728	0.602	350944.3486	100.0531	0.053	0.200	0.598	0.021	0.021		
25.02.2016	180	70.412	178.977	179.292	3500.591	3.507	998.244	3.04	20.20	20.20	23400.3187	6.6729	0.602	23400.3187	6.6729	0.602	350873.6505	100.0567	0.057	0.200	0.599	0.026	0.026		
25.02.2016	200	63.254	199.229	199.580	3500.561	3.507	998.239	3.02	20.22	20.22	23409.1604	6.6755	0.641	23409.1604	6.6755	0.641	350931.4753	100.0215	0.022	0.220	0.638	0.022	0.022		
25.02.2016	200	63.176	199.525	199.877	3501.446	3.508	998.241	2.99	20.22	20.22	23414.7321	6.6754	0.639	23414.7321	6.6754	0.639	350925.4530	100.0225	0.022	0.220	0.637	0.023	0.023		
25.02.2016	200	63.311	199.049	199.400	3500.550	3.507	998.241	3.01	20.22	20.22	23409.8322	6.6757	0.644	23409.8322	6.6757	0.644	350862.9525	100.0539	0.054	0.220	0.641	0.027	0.027		
25.02.2016	200	63.084	199.814	200.167	3501.414	3.508	998.240	3.00	20.22	20.22	23415.1022	6.6755	0.641	23415.1022	6.6755	0.641	350931.9620	100.0488	0.049	0.220	0.638	0.022	0.022		
25.02.2016	200	63.296	199.223	199.574	3500.576	3.507	998.240	3.02	20.22	20.22	23405.4151	6.6756	0.642	23405.4151	6.6756	0.642	350935.0125	100.0500	0.050	0.220	0.640	0.023	0.023		

*Original data set

Data report RISE: Day#2

RISE Laboratory – Day#3

Table with columns for Date, Nominal flowrate, Meas-urement time, Laboratory reference (Standard mass flowrate, Volume, Water density, Fluid Line pressure, Water temp., Ambient conditions), Turbine meter (K, N, Kv, error), Coriolis_Mass (K, N, Kv, error), Coriolis_Vol (K, N, Kv, error), and Temperature correction of meter error (T_nom, T, e_turbine, e_coriolis).

UME Laboratory – Day#1

Data report UME: Day#1					Original data set		Laboratory reference								Ambient conditions				Turbine meter		Coriolis_Mass				Coriolis_Vol				Temperature correction of meter error					
Date	Nominal flowrate	Measurment time	Standard mass flowrate	Standard volume flowrate	Mass	Volume	Water density	Water temp.	Line pressure	Fluid	Air temp.	Air pressure	Water temp.	Line pressure	Fluid	Nominal flowrate	Measurment time	Standard mass flowrate	Standard volume flowrate	Mass	Volume	Water density	Water temp.	Line pressure	Fluid	Air temp.	Air pressure	Water temp.	Line pressure	Fluid	T _{nom}	Temperature correction of meter error		
	[m³/h]	[s]	[m³/h]	[m³/h]	[kg]	[m³]	[kg/m³]	[°C]	[bar]	[m³/h]	[°C]	[bar]	[°C]	[bar]	[m³/h]	[m³/h]	[s]	[m³/h]	[m³/h]	[kg]	[m³]	[kg/m³]	[°C]	[bar]	[m³/h]	[°C]	[bar]	[°C]	[bar]	[m³/h]	[m³/h]	[°C]	Temperature correction of meter error	
26.05.2016	30	60.438	30.395	30.425	510.281	0.511	999.021	0.48	16.50	22.60	0.99	3402	6.6604	0.413	51084	100.1095	0.110	51165	100.1701	0.170	3500	0.388	0.100											
26.05.2016	30	60.642	30.392	30.421	511.943	0.512	999.021	0.48	16.50	22.60	0.99	3412	6.6583	0.381	51229	100.0677	0.088	51310	100.1278	0.128	-3500	0.356	0.058											
26.05.2016	30	60.558	30.370	30.407	508.419	0.509	999.021	0.48	16.50	22.60	0.99	3389	6.6592	0.396	50886	100.0867	0.087	50966	100.1459	0.146	-3500	0.371	0.077											
26.05.2016	30	60.234	30.386	30.415	508.399	0.509	999.021	0.48	16.50	22.60	0.99	3387	6.6556	0.340	50879	100.0769	0.077	50959	100.1361	0.136	-3500	0.316	0.067											
26.05.2016	60	46.162	59.787	59.846	766.648	0.767	999.021	0.34	16.50	22.60	0.99	5114	6.6641	0.468	76767	100.1333	0.133	76880	100.1825	0.182	-3500	0.467	0.115											
26.05.2016	60	46.298	59.788	59.846	768.911	0.770	999.021	0.34	16.50	22.60	0.99	5129	6.6589	0.467	76945	100.0701	0.070	77064	100.1268	0.127	-3500	0.465	0.052											
26.05.2016	60	46.472	59.768	59.826	771.544	0.772	999.021	0.34	16.50	22.60	0.99	5147	6.6645	0.475	77212	100.0747	0.075	77331	100.1308	0.131	-3500	0.474	0.057											
26.05.2016	60	46.318	59.750	59.808	768.751	0.770	999.021	0.34	16.50	22.60	0.99	5127	6.6627	0.448	76978	100.0689	0.069	77047	100.1255	0.126	-3500	0.447	0.051											
26.05.2016	60	46.468	59.768	59.826	771.474	0.772	999.021	0.34	16.50	22.60	0.99	5146	6.6638	0.465	77208	100.0786	0.079	77326	100.1334	0.133	-3500	0.463	0.051											
26.05.2016	100	31.853	100.264	100.364	887.148	0.888	999.004	0.80	16.60	22.60	0.99	9223	6.6698	0.555	88775	100.0679	0.068	88930	100.1202	0.120	-3400	0.549	0.051											
26.05.2016	100	31.129	100.191	100.291	921.998	0.923	999.004	0.80	16.60	22.60	0.99	6155	6.6691	0.544	92284	100.0588	0.059	92384	100.1108	0.111	-3400	0.538	0.042											
26.05.2016	100	32.857	100.072	100.172	913.348	0.914	999.004	0.80	16.60	22.60	0.99	6097	6.6688	0.540	91398	100.0692	0.069	91537	100.1215	0.122	-3400	0.534	0.052											
26.05.2016	100	33.179	99.990	100.090	921.538	0.922	999.004	0.80	16.60	22.60	0.99	6152	6.6692	0.545	92207	100.0578	0.058	92346	100.1088	0.109	-3400	0.539	0.041											
26.05.2016	100	32.873	99.916	100.016	912.367	0.913	999.004	0.80	16.60	22.60	0.99	6091	6.6694	0.549	91292	100.0606	0.061	91431	100.1132	0.113	-3400	0.543	0.044											
26.05.2016	140	54.357	140.175	140.318	2116.548	2.119	999.987	1.70	16.70	22.60	0.99	14124	6.6664	0.503	211539	99.9453	-0.055	211859	99.9951	-0.005	-3300	0.511	-0.071											
26.05.2016	140	52.230	140.217	140.361	2034.377	2.036	998.970	1.70	16.80	22.60	0.99	13580	6.6686	0.536	20362	99.9652	-0.055	203670	100.0135	0.014	-3200	0.543	-0.051											
26.05.2016	140	111.707	140.125	140.270	4348.038	4.353	998.970	1.70	16.80	22.60	0.99	29025	6.6685	0.536	434680	99.9715	-0.028	435345	100.0213	0.021	-3200	0.543	-0.045											
26.05.2016	140	64.752	140.430	140.575	2525.854	2.528	998.970	1.70	16.80	22.60	0.99	18865	6.6701	0.559	252589	100.0014	0.001	252980	100.0531	0.053	-3200	0.566	-0.015											
26.05.2016	140	64.196	140.577	140.722	2506.805	2.509	998.970	1.70	16.80	22.60	0.99	16784	6.6686	0.536	250609	99.9715	-0.029	250997	100.0231	0.023	-3200	0.543	-0.045											
26.05.2016	180	50.997	180.007	180.184	2549.955	2.552	999.021	0.36	16.50	22.60	0.99	17033	6.6722	0.606	255075	100.0312	0.031	255393	100.0578	0.058	-3500	0.619	0.015											
26.05.2016	180	51.846	179.902	180.078	2590.902	2.593	999.021	0.36	16.50	22.60	0.99	17310	6.6745	0.626	259209	100.0459	0.046	259538	100.0748	0.075	-3500	0.639	0.030											
26.05.2016	180	51.237	179.855	180.031	2559.766	2.562	999.021	0.36	16.50	22.60	0.99	17104	6.6753	0.638	256109	100.0517	0.052	256434	100.0806	0.081	-3500	0.651	0.036											
26.05.2016	180	51.883	179.859	180.035	2592.103	2.595	999.021	0.36	16.50	22.60	0.99	17319	6.6749	0.632	259338	100.0493	0.049	259665	100.0773	0.077	-3500	0.644	0.033											
26.05.2016	180	51.728	179.768	179.944	2583.093	2.586	999.021	0.36	16.50	22.60	0.99	17258	6.6746	0.627	258436	100.0490	0.049	258765	100.0783	0.078	-3500	0.640	0.033											
26.05.2016	200	54.785	200.631	200.828	3055.238	3.056	999.021	0.45	16.50	22.60	0.99	20405	6.6765	0.656	305385	100.0200	0.020	305796	100.0566	0.057	-3500	0.669	0.004											
26.05.2016	200	55.806	200.438	200.635	3107.100	3.110	999.021	0.45	16.50	22.60	0.99	20766	6.6769	0.661	310823	100.0364	0.036	311242	100.0732	0.073	-3500	0.674	0.020											
26.05.2016	200	54.736	200.510	200.707	3048.632	3.052	999.021	0.45	16.50	22.60	0.99	20374	6.6765	0.655	304935	100.0236	0.024	305349	100.0613	0.061	-3500	0.668	0.007											
26.05.2016	200	55.128	200.601	200.798	3071.859	3.075	999.021	0.45	16.50	22.60	0.99	20524	6.6748	0.630	307196	100.0033	0.003	307613	100.0410	0.041	-3500	0.642	-0.013											
26.05.2016	200	54.806	200.511	200.707	3052.537	3.056	999.021	0.45	16.50	22.60	0.99	20400	6.6764	0.655	305331	100.0253	0.025	305748	100.0639	0.064	-3500	0.667	0.009											

UME Laboratory – Day#2

Data report UME: Day#2												*Original data set																			
Laboratory reference											Turbine meter					Coriolis_Mass					Coriolis_Vol					Temperature correction of meter error					
Date	Nominal flowrate	Meas-urement time	Standard mass flowrate	Volume	Water density	Line pressure	Water temp.	Air temp.	Air pressure	Ambient conditions			K _{vol,nom}		Pulses/Liter		K _{mass,nom}		Pulses/kg		K _{vol,nom}		Pulses/Liter		T _{room}	°C					
										ρ _{fluid}	ρ _{air}	T _{air}	p _{air}	N	K _v	ε _v	N	K _m	ε _m	N	K _v	ε _v	N	K _m			ε _m	N	K _v	ε _v	ΔT _{fluid}
[mm/h]	[mm/h]	[s]	[lbh]	[m ³]	[kg/m ³]	[bar]	[°C]	[°C]	[bar]	[kg/m ³]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]					
27.05.2016	30	88.105	30.159	738.091	0.739	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	
27.05.2016	30	90.844	30.157	760.997	0.762	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	
27.05.2016	30	89.451	30.192	750.194	0.751	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	
27.05.2016	30	93.491	30.185	783.908	0.785	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	
27.05.2016	30	92.710	30.195	777.601	0.778	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	998.883	0.86	17.30	22.60	0.99	
27.05.2016	60	73.646	60.317	60.384	1233.930	1.235	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99
27.05.2016	60	72.609	60.301	60.367	1216.209	1.218	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99
27.05.2016	60	73.234	60.322	60.389	1227.122	1.228	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99
27.05.2016	60	72.355	60.288	60.335	1211.304	1.213	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99	998.900	0.42	17.20	22.60	0.99
27.05.2016	100	66.387	100.361	100.473	1859.744	1.853	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99
27.05.2016	100	66.811	100.178	100.290	1859.154	1.861	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99
27.05.2016	100	66.525	99.960	100.072	1847.178	1.849	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99
27.05.2016	100	64.806	99.809	99.921	1796.725	1.799	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99
27.05.2016	100	66.335	99.720	99.831	1837.478	1.840	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99	998.883	0.33	17.30	22.60	0.99
27.05.2016	140	63.042	140.267	140.422	2456.436	2.459	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99
27.05.2016	140	51.928	140.105	140.260	2070.945	2.073	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99
27.05.2016	140	53.216	140.067	140.221	2070.949	2.073	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99
27.05.2016	140	53.100	139.721	139.875	2060.888	2.063	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99
27.05.2016	180	52.914	139.886	140.040	2056.081	2.058	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99	998.900	0.27	17.20	22.60	0.99
27.05.2016	180	51.999	180.493	180.688	2576.986	2.580	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99
27.05.2016	180	50.871	180.404	180.600	2549.254	2.552	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99
27.05.2016	180	51.685	180.284	180.479	2588.239	2.591	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99
27.05.2016	180	52.217	179.972	180.167	2610.425	2.613	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99
27.05.2016	180	51.095	179.916	180.111	2553.559	2.556	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99	998.918	0.30	17.10	22.60	0.99
27.05.2016	200	56.409	200.305	200.526	3138.637	3.142	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99
27.05.2016	200	55.442	200.245	200.465	3083.873	3.087	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99
27.05.2016	200	55.681	200.083	200.303	3094.686	3.098	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99	998.900	0.37	17.20	22.60	0.99
27.05.2016	200	55.799	200.061	200.278	3100.893	3.104	998.918	0.37	17.10	22.60	0.99	998.918	0.37	17.10	22.60	0.99	998.918	0.37	17.10	22.60	0.99	998.918	0.37	17.10	22.60	0.99	998.918	0.37	17.10	22.60	0.99
27.05.2016	200	55.663	199.934	200.151	3091.382	3.095	998.918	0.37	17.10	22.60	0.99	998.918	0.37	17.10	22.60	0.99	998.918	0.37	17.10	22.60	0.99	998.918	0.37	17.10	22.60	0.99	998.918	0.37	17.10	22.60	0.99

UME Laboratory – Day#3

Data report UME: Day#3												*Original data set								Temperature correction of meter error													
Date	Nominal flowrate V _{nom} [m³/h]	Measurment time t [s]	Laboratory reference							Fluid				Ambient conditions				Turbine meter				Coriolis_Mass				Coriolis_Vol				Corrected meter error			
			Standard mass flowrate V _{st} [m³/h]	Standard volume flowrate V _{st} [m³/h]	Mass m _{st} [kg]	Volume V _{st} [m³]	Water density ρ _{water} [kg/m³]	Line pressure P _{line} [bar]	Water temp. T _{fluid} [°C]	Air temp. T _{air} [°C]	Air pressure P _{air} [bar]	Pulse count N	K-factor [Pulses/Liter]	Meter error ev [%]	K _m [Pulses/Liter]	Pulse count N	K-factor [Pulses/Liter]	Meter error ev [%]	Pulse count N	K-factor [Pulses/Liter]	Meter error ev [%]	(T _{fluid} -T _{nom}) [°C]	ΔT _{met} [°C]	Turbine meter e _{vac} [%]	Coriolis_Mass e _{vac} [%]	K _{v,nom}	Pulse count N	K-factor [Pulses/Liter]	Meter error ev [%]	(T _{fluid} -T _{nom}) [°C]	ΔT _{met} [°C]	Turbine meter e _{vac} [%]	Coriolis_Vol e _{vac} [%]
28.05.2016	30	89709	30.322	30.360	755.596	0.757	998.756	0.42	18.00	23.15	1.00	5036	6.6567	0.357	100.0310	0.086	75719	100.0864	0.086	-2.000	-2.000	0.337	0.029	100.0000	100.0000	100.0000	0.086	-2.000	-2.000	0.337	0.029	20	
28.05.2016	30	137898	30.314	30.351	1161.165	1.163	998.756	0.41	18.00	23.15	1.00	7739	6.6566	0.355	100.0323	0.086	116154	100.0310	0.086	-2.000	-2.000	0.335	0.030	100.0000	100.0000	100.0000	0.086	-2.000	-2.000	0.335	0.030	20	
28.05.2016	30	89893	30.293	30.332	756.474	0.757	998.756	0.41	18.00	23.15	1.00	5043	6.6583	0.381	100.0351	0.091	75674	100.0351	0.091	-2.000	-2.000	0.361	0.032	100.0000	100.0000	100.0000	0.091	-2.000	-2.000	0.361	0.032	20	
28.05.2016	30	87935	30.293	30.331	739.962	0.741	998.756	0.41	18.00	23.15	1.00	4932	6.6569	0.361	100.0376	0.091	74156	100.0376	0.091	-2.000	-2.000	0.341	0.035	100.0000	100.0000	100.0000	0.091	-2.000	-2.000	0.341	0.035	20	
28.05.2016	30	89603	30.301	30.338	754.172	0.755	998.756	0.41	18.00	23.15	1.00	5027	6.6573	0.366	100.0355	0.095	75444	100.0355	0.095	-2.000	-2.000	0.346	0.033	100.0000	100.0000	100.0000	0.095	-2.000	-2.000	0.346	0.033	20	
28.05.2016	30	87239	30.304	30.341	734.351	0.735	998.756	0.41	18.00	23.15	1.00	4894	6.6561	0.348	100.0244	0.077	73453	100.0244	0.077	-2.000	-2.000	0.328	0.022	100.0000	100.0000	100.0000	0.077	-2.000	-2.000	0.328	0.022	20	
28.05.2016	30	88757	30.308	30.346	747.242	0.748	998.756	0.41	18.00	23.15	1.00	4980	6.6562	0.350	100.0346	0.088	74750	100.0346	0.088	-2.000	-2.000	0.330	0.032	100.0000	100.0000	100.0000	0.088	-2.000	-2.000	0.330	0.032	20	
28.05.2016	30	90177	30.299	30.336	758.952	0.760	998.756	0.41	18.00	23.15	1.00	5058	6.6562	0.349	100.0314	0.081	75919	100.0314	0.081	-2.000	-2.000	0.329	0.029	100.0000	100.0000	100.0000	0.081	-2.000	-2.000	0.329	0.029	20	
28.05.2016	30	89033	30.298	30.336	749.145	0.750	998.756	0.41	18.00	23.15	1.00	4994	6.6580	0.377	100.0394	0.099	74944	100.0394	0.099	-2.000	-2.000	0.357	0.037	100.0000	100.0000	100.0000	0.099	-2.000	-2.000	0.357	0.037	20	
28.05.2016	30	91745	30.282	30.319	771.723	0.773	998.756	0.41	18.00	23.15	1.00	5144	6.6573	0.367	100.0256	0.078	77192	100.0256	0.078	-2.000	-2.000	0.347	0.023	100.0000	100.0000	100.0000	0.078	-2.000	-2.000	0.347	0.023	20	
28.05.2016	100	73601	100.195	100.320	2048.450	2.051	998.756	0.23	18.00	23.15	1.00	13671	6.6655	0.490	100.0381	0.038	204923	100.0381	0.038	-2.000	-2.000	0.486	0.028	100.0000	100.0000	100.0000	0.038	-2.000	-2.000	0.486	0.028	20	
28.05.2016	100	74248	100.393	100.518	2070.557	2.073	998.756	0.22	18.00	23.15	1.00	13818	6.6653	0.486	100.0460	0.046	207151	100.0460	0.046	-2.000	-2.000	0.482	0.036	100.0000	100.0000	100.0000	0.046	-2.000	-2.000	0.482	0.036	20	
28.05.2016	100	71607	100.348	100.471	1996.014	1.998	998.756	0.22	18.00	23.15	1.00	13319	6.6646	0.477	100.0270	0.032	199665	100.0270	0.032	-2.000	-2.000	0.472	0.022	100.0000	100.0000	100.0000	0.032	-2.000	-2.000	0.472	0.022	20	
28.05.2016	100	72567	100.386	100.510	2023.538	2.026	998.756	0.23	18.00	23.15	1.00	13902	6.6643	0.472	100.0293	0.029	202376	100.0293	0.029	-2.000	-2.000	0.470	0.024	100.0000	100.0000	100.0000	0.029	-2.000	-2.000	0.470	0.024	20	
28.05.2016	100	73381	100.456	100.580	2047.849	2.050	998.756	0.23	18.00	23.15	1.00	13664	6.6648	0.480	100.0381	0.038	204843	100.0381	0.038	-2.000	-2.000	0.476	0.028	100.0000	100.0000	100.0000	0.038	-2.000	-2.000	0.476	0.028	20	
28.05.2016	100	72489	100.544	100.669	2024.534	2.027	998.756	0.23	18.00	23.15	1.00	13508	6.6639	0.465	100.0285	0.028	202511	100.0285	0.028	-2.000	-2.000	0.461	0.019	100.0000	100.0000	100.0000	0.028	-2.000	-2.000	0.461	0.019	20	
28.05.2016	100	73856	100.463	100.588	2061.064	2.064	998.756	0.23	18.00	23.15	1.00	13754	6.6650	0.474	100.0371	0.037	206205	100.0371	0.037	-2.000	-2.000	0.470	0.027	100.0000	100.0000	100.0000	0.037	-2.000	-2.000	0.470	0.027	20	
28.05.2016	100	73028	100.384	100.509	2036.946	2.039	998.756	0.22	18.00	23.15	1.00	13888	6.6644	0.474	100.0371	0.037	204057	100.0371	0.037	-2.000	-2.000	0.470	0.027	100.0000	100.0000	100.0000	0.037	-2.000	-2.000	0.470	0.027	20	
28.05.2016	100	71483	100.361	100.486	1992.413	1.995	998.756	0.22	18.00	23.15	1.00	13297	6.6642	0.470	100.0335	0.033	199348	100.0335	0.033	-2.000	-2.000	0.466	0.024	100.0000	100.0000	100.0000	0.033	-2.000	-2.000	0.466	0.024	20	
28.05.2016	200	54857	200.012	200.261	3047.813	3.052	998.756	0.42	18.00	23.15	1.00	20381	6.6788	0.650	100.0347	0.035	304887	100.0347	0.035	-2.000	-2.000	0.657	0.025	100.0000	100.0000	100.0000	0.035	-2.000	-2.000	0.657	0.025	20	
28.05.2016	200	55300	199.892	200.141	3070.530	3.074	998.756	0.42	18.00	23.15	1.00	20530	6.6778	0.676	100.0247	0.025	307129	100.0247	0.025	-2.000	-2.000	0.671	0.016	100.0000	100.0000	100.0000	0.025	-2.000	-2.000	0.671	0.016	20	
28.05.2016	200	55368	199.795	200.044	3072.832	3.077	998.756	0.42	18.00	23.15	1.00	20545	6.6777	0.674	100.0367	0.037	307396	100.0367	0.037	-2.000	-2.000	0.680	0.027	100.0000	100.0000	100.0000	0.037	-2.000	-2.000	0.680	0.027	20	
28.05.2016	200	55245	199.871	200.180	3068.135	3.072	998.756	0.42	18.00	23.15	1.00	20516	6.6785	0.686	100.0275	0.028	306988	100.0275	0.028	-2.000	-2.000	0.680	0.018	100.0000	100.0000	100.0000	0.028	-2.000	-2.000	0.680	0.018	20	
28.05.2016	200	55779	199.871	200.124	3096.860	3.101	998.738	0.42	18.10	23.15	1.00	20708	6.6783	0.683	100.0310	0.031	310269	100.0310	0.031	-1.900	-1.900	0.690	0.022	100.0000	100.0000	100.0000	0.031	-1.900	-1.900	0.690	0.022	20	
28.05.2016	200	56281	199.753	200.002	3122.882	3.127	998.756	0.42	18.00	23.15	1.00	20878	6.6772	0.666	100.0169	0.017	312841	100.0169	0.017	-2.000	-2.000	0.673	0.008	100.0000	100.0000	100.0000	0.017	-2.000	-2.000	0.673	0.008	20	
28.05.2016	200	55547	199.847	200.100	3083.594	3.087	998.738	0.42	18.10	23.15	1.00	20617	6.6776	0.672	100.0219	0.022	308427	100.0219	0.022	-1.900	-1.900	0.678	0.013	100.0000	100.0000	100.0000	0.022	-1.900	-1.900	0.678	0.013	20	
28.05.2016	200	55165	199.836	200.085	3062.530	3.066	998.756	0.42	18.00	23.15	1.00	20471	6.6767	0.659	100.0101	0.010	306254	100.0101	0.010	-2.000	-2.000	0.665	0.001	100.0000	100.0000	100.0000	0.010	-2.000	-2.000	0.665	0.001	20	
28.05.2016	200	55334	200.188	200.437	3076.997	3.081	998.756	0.42	18.00	23.15	1.00	20570	6.6768	0.660	100.0121	0.012	307337	100.0121	0.012	-2.000	-2.000	0.667	0.003	100.0000	100.0000	100.0000	0.012	-2.000	-2.000	0.667	0.003	20	
28.05.2016	200	55129	200.149	200.402	3065.033	3.069	998.738	0.42	18.10	23.15	1.00	20491	6.6770	0.663	100.0130	0.013	306543	100.0130	0.013	-1.900	-1.900	0.669	0.004	100.0000	100.0000	100.0000	0.013	-1.900	-1.900	0.669	0.004	20	

PTB Laboratory – Day#1

Date	Nominal flowrate V _{nom} [m³/h]	Data report PTB: Day#1														Temperature correction of meter error										
		Measur-ment time t [s]	Standard mass flowrate m ^{ref} [kg/h]	Standard volume flowrate V ^{ref} [m³/h]	Laboratory reference					Air temp. T _{air} [°C]	Air pressure p _{air} [bar]	Turbine meter		Coriolis_Mass		Coriolis_Vol										
					Mass m ^{ref} [kg]	Volume V ^{ref} [m³]	Water density ρ _{fluid} [kg/m³]	Line pressure p _{fluid} [bar]	Water temp. T _{fluid} [°C]			K _{v,turn}	Pulse count	K-factor [Pulses/Liter]	Meter error e _v [%]	K _{m,nom}	Pulse count	K-factor [Pulses/kg]	Meter error e _m [%]	K _{v,vol}	Pulse count	K-factor [Pulses/Liter]	Meter error e _v [%]			
19.07.2016	30	324,140	29,905	29,956	2692,653	2,697	998,325	3,00	20,27	23,13	1,01	17952	6,65529	0,345	269393	100,0474	0,047	269898	100,0670	0,067	269898	100,0670	0,067	0,265	0,331	0,055
19.07.2016	30	324,119	29,946	29,995	2696,089	2,701	998,355	2,99	20,12	23,12	1,01	17972	6,65540	0,331	269700	100,0371	0,037	269700	100,0371	0,037	269700	100,0371	0,037	0,123	0,318	0,044
19.07.2016	30	324,114	29,902	29,951	2692,163	2,697	998,363	3,01	20,08	23,10	1,01	17945	6,65540	0,328	269310	100,0348	0,035	269799	100,0524	0,052	269799	100,0524	0,052	0,082	0,314	0,042
19.07.2016	30	324,133	29,899	29,948	2692,111	2,696	998,365	3,00	20,08	23,07	1,01	17943	6,65444	0,322	269288	100,0323	0,032	269775	100,0493	0,049	269775	100,0493	0,049	0,076	0,308	0,039
19.07.2016	30	324,090	29,924	29,973	2693,953	2,698	998,367	3,00	20,07	23,07	1,01	17956	6,65444	0,323	269506	100,0411	0,041	269994	100,0585	0,059	269994	100,0585	0,059	0,066	0,309	0,048
19.07.2016	60	162,117	59,881	59,881	59,881	2,697	998,391	3,00	19,95	23,08	1,01	17988	6,6638	0,465	269595	100,0353	0,035	270076	100,0522	0,052	270076	100,0522	0,052	-0,038	0,470	0,099
19.07.2016	60	162,128	59,889	59,886	2697,150	2,701	998,393	3,00	19,94	23,08	1,01	18001	6,6634	0,458	269819	100,0386	0,039	270302	100,0566	0,057	270302	100,0566	0,057	-0,061	0,463	0,043
19.07.2016	60	162,109	59,830	59,926	2694,163	2,698	998,393	3,00	19,94	23,09	1,01	17981	6,6633	0,457	269491	100,0277	0,028	269975	100,0463	0,046	269975	100,0463	0,046	-0,060	0,462	0,032
19.07.2016	60	162,106	59,887	59,887	2696,662	2,701	998,392	3,00	19,94	23,09	1,01	17998	6,6634	0,459	269755	100,0319	0,033	270241	100,0520	0,052	270241	100,0520	0,052	-0,057	0,464	0,037
19.07.2016	100	97,338	99,653	99,814	2694,458	2,699	998,388	3,00	19,96	23,11	1,01	17995	6,6678	0,524	269531	100,0316	0,032	270011	100,0483	0,048	270011	100,0483	0,048	-0,038	0,521	0,031
19.07.2016	100	97,324	99,758	99,918	2696,890	2,701	998,392	3,00	19,94	23,13	1,01	18013	6,6684	0,534	269774	100,0315	0,032	270254	100,0484	0,048	270254	100,0484	0,048	-0,057	0,531	0,031
19.07.2016	100	97,342	99,719	99,879	2695,843	2,700	998,395	3,00	19,93	23,12	1,01	18005	6,6681	0,529	269658	100,0274	0,027	270139	100,0450	0,045	270139	100,0450	0,045	-0,072	0,526	0,027
19.07.2016	100	97,342	99,766	99,927	2697,621	2,702	998,390	3,00	19,96	23,10	1,01	18017	6,6681	0,529	269849	100,0322	0,032	270331	100,0495	0,050	270331	100,0495	0,050	-0,044	0,526	0,032
19.07.2016	100	97,322	99,659	99,819	2694,156	2,698	998,393	3,00	19,94	23,08	1,01	17995	6,6685	0,536	269502	100,0321	0,032	269984	100,0499	0,050	269984	100,0499	0,050	-0,059	0,533	0,032
19.07.2016	140	69,523	140,947	141,174	2721,967	2,726	998,394	2,98	19,94	23,08	1,01	18200	6,6756	0,642	272288	100,0335	0,034	272764	100,0475	0,047	272764	100,0475	0,047	-0,065	0,638	0,032
19.07.2016	140	69,522	139,309	139,533	2690,292	2,695	998,394	3,01	19,93	23,07	1,01	17987	6,6752	0,636	269122	100,0345	0,035	269553	100,0486	0,049	269553	100,0486	0,049	-0,066	0,632	0,033
19.07.2016	140	69,543	139,235	139,460	2688,897	2,693	998,392	3,01	19,94	23,07	1,01	17977	6,6749	0,632	268983	100,0347	0,035	269455	100,0492	0,049	269455	100,0492	0,049	-0,058	0,628	0,034
19.07.2016	140	69,543	139,235	139,460	2689,681	2,694	998,389	3,01	19,96	23,08	1,01	17983	6,6752	0,636	269069	100,0375	0,038	269542	100,0520	0,052	269542	100,0520	0,052	-0,043	0,632	0,036
19.07.2016	140	69,568	139,188	139,412	2689,733	2,694	998,394	3,01	19,94	23,08	1,01	17948	6,6621	0,636	269063	100,0334	0,033	269537	100,0486	0,049	269537	100,0486	0,049	-0,063	0,630	0,032
19.07.2016	180	54,104	178,876	179,164	2688,296	2,693	998,392	3,02	19,95	23,03	1,01	17948	6,6817	0,734	268282	100,0373	0,037	268738	100,0462	0,046	268738	100,0462	0,046	-0,053	0,733	0,037
19.07.2016	180	54,105	178,793	179,081	2687,098	2,691	998,392	3,01	19,94	23,06	1,01	17991	6,6816	0,732	268936	100,0396	0,040	269394	100,0488	0,049	269394	100,0488	0,049	-0,058	0,731	0,039
19.07.2016	180	54,150	181,242	181,534	2726,170	2,731	998,392	2,97	19,94	23,07	1,01	18247	6,6825	0,746	272725	100,0396	0,040	273188	100,0483	0,048	273188	100,0483	0,048	-0,055	0,745	0,039
19.07.2016	180	54,105	179,358	179,648	2695,597	2,700	998,388	3,00	19,96	23,08	1,01	18040	6,6816	0,733	269663	100,0383	0,038	270123	100,0475	0,047	270123	100,0475	0,047	-0,038	0,732	0,038
19.07.2016	200	48,742	201,036	201,360	2721,898	2,726	998,390	2,97	19,95	23,06	1,01	18225	6,6849	0,783	272293	100,0379	0,038	272747	100,0434	0,043	272747	100,0434	0,043	-0,047	0,782	0,037
19.07.2016	200	48,699	200,222	200,546	2708,478	2,713	998,385	2,98	19,98	23,06	1,01	18134	6,6845	0,776	270960	100,0414	0,041	271412	100,0465	0,046	271412	100,0465	0,046	-0,023	0,775	0,041
19.07.2016	200	48,747	200,146	200,469	2710,127	2,715	998,389	2,99	19,96	23,07	1,01	18145	6,6845	0,776	271118	100,0389	0,039	271571	100,0445	0,045	271571	100,0445	0,045	-0,040	0,775	0,038
19.07.2016	200	48,727	198,156	198,476	2682,068	2,686	998,386	3,02	19,97	23,06	1,01	17957	6,6844	0,775	268311	100,0388	0,039	268763	100,0456	0,046	268763	100,0456	0,046	-0,027	0,774	0,038
19.07.2016	200	48,726	201,041	201,366	2721,086	2,725	998,386	2,97	19,97	23,08	1,01	18219	6,6847	0,779	272213	100,0384	0,038	272688	100,0439	0,044	272688	100,0439	0,044	-0,028	0,778	0,038

PTB Laboratory – Day#2

Table with columns: Date, Nominal flowrate, Measu- rament time, Laboratory reference (Standard mass flowrate, Standard volume flowrate, Mass, Volume), Fluid (Line pressure, Water density, Water temp., Air temp., Air pressure), Turbine meter (Pulse count, K-factor, Meter error), Coriolis_Mass (Pulse count, K-factor, Meter error), Coriolis_Vol (Pulse count, K-factor, Meter error), and Temperature correction of meter error (T_nom, Corrected meter error).

NIST Laboratory – Day#1

Data report NIST: Day#1				Laboratory reference								Turbine meter			Coriolis_Mass			Coriolis_Vol			Temperature correction of meter error																						
Date	Nominal flowrate	Measurment time	t	Standard mass flowrate	Standard volume flowrate	Mass	Volume	Water density	Line pressure	Water temp.	Air temp.	Air pressure	Pulse count	K-factor	e _v	K _{v, nom}	Pulses/Liter	Pulse count	K _{v, nom}	Pulses/kg	Meter output frequency	e _m	N	K _v	Pulses/ Liter	Meter output frequency	e _v	K _{v, nom}	Pulses/Liter	Meter output frequency	e _m	N	K _v	Pulses/ Liter	Meter output frequency	e _v	(T _{fluid} - T _{nom})	ΔT _{fluid}	Corrected meter error	Coriolis_Mass	e _{nor}		
	[m ³ /h]	[s]	[h]	[m ³ /h]	[m ³ /h]	[kg]	[m ³]	[kg/m ³]	[bar]	[°C]	[°C]	[bar]	[Pulses]	[Pulses/ Liter]	[%]	[Pulses]	[Pulses/ Liter]	[Pulses]	[Pulses]	[Pulses/ kg]	[Hz]	[%]	[Pulses]	[Pulses/ Liter]	[Hz]	[Hz]	[%]	[Pulses]	[Pulses/ Liter]	[Hz]	[%]	[Pulses]	[Pulses/ Liter]	[Hz]	[%]	[°C]	[%]	[%]	[%]				
*Original data set																																											
28.09.2016	30	119.684	30.144	30.209	1003.721	1003.890	997.840	1.64	2345	24.50	1.00	1.00		6.6330		100.0000	837.5712	0.030		100.0329	840.2493	0.133	3.453			100.0329	840.2493	0.133	3.453								3.453	0.051					
28.09.2016	30	119.641	30.152	30.217	1004.223	1004.418	997.834	1.64	2348	24.50	1.00	1.00		6.6330		100.0000	837.4418	-0.012		100.0204	839.5315	0.020	3.476			100.0204	839.5315	0.020	3.476									3.476	0.009				
28.09.2016	30	119.643	30.181	30.247	1003.049	1005.241	997.819	1.64	2354	24.20	1.00	1.00		6.6330		100.0000	836.3007	-0.008		100.0302	840.4556	0.030	3.541			100.0302	840.4556	0.030	3.541									3.541	0.013				
28.09.2016	30	119.632	30.132	30.198	1003.320	1003.515	997.813	1.65	2356	24.30	1.00	1.00		6.6330		100.0000	836.9682	-0.004		100.0255	839.0483	0.026	3.564			100.0255	839.0483	0.026	3.564										3.564	0.017			
28.09.2016	30	119.634	30.055	30.121	998.763	1000.958	997.807	1.65	2359	24.30	1.00	1.00		6.6330		100.0000	834.7947	-0.007		100.0154	836.8132	0.015	3.587			100.0154	836.8132	0.015	3.587										3.587	0.015			
28.09.2016	60	180.060	60.052	60.185	3003.620	3010.229	997.805	1.88	2364	24.30	1.00	1.00		6.6330		100.0000	1667.8901	-0.014		99.9866	1671.5690	-0.013	3.640			99.9866	1671.5690	-0.013	3.640									3.640	0.009				
28.09.2016	60	180.057	60.071	60.204	3004.523	3011.148	997.800	1.88	2366	24.30	1.00	1.00		6.6330		100.0000	1668.9892	0.020		100.0202	1673.0297	0.042	3.663			100.0202	1673.0297	0.042	3.663										3.663	0.043			
28.09.2016	60	180.061	60.067	60.199	3004.348	3010.990	997.794	1.88	2369	24.30	1.00	1.00		6.6330		100.0000	1668.5565	0.002		100.0409	1672.8897	0.041	3.685			100.0409	1672.8897	0.041	3.685											3.685	0.025		
28.09.2016	60	180.048	60.049	60.182	3003.224	3009.880	997.789	1.88	2371	24.30	1.00	1.00		6.6330		100.0000	1668.3990	0.023		100.0429	1672.4297	0.043	3.707			100.0429	1672.4297	0.043	3.707											3.707	0.046		
28.09.2016	60	180.052	60.065	60.199	3004.127	3010.799	997.784	1.89	2372	24.20	1.00	1.00		6.6330		100.0000	1668.5929	0.007		100.0425	1672.8984	0.043	3.724			100.0425	1672.8984	0.043	3.724												3.724	0.030	
28.09.2016	100	108.764	99.234	99.455	2998.068	3004.745	997.778	1.93	2375	24.30	1.00	1.00		6.6330		100.0000	2755.4111	-0.039		99.9824	2762.1406	-0.018	3.794			99.9824	2762.1406	-0.018	3.794											3.794	-0.024		
28.09.2016	100	108.767	99.261	99.483	2998.983	3005.671	997.772	1.93	2377	24.30	1.00	1.00		6.6330		100.0000	2755.0834	0.030		100.0386	2764.4716	0.039	3.766			100.0386	2764.4716	0.039	3.766												3.766	0.046	
28.09.2016	100	108.767	99.256	99.478	2998.579	3005.274	997.772	1.93	2378	24.30	1.00	1.00		6.6330		100.0000	2757.3775	0.009		100.0319	2764.1622	0.032	3.778			100.0319	2764.1622	0.032	3.778												3.778	0.025	
28.09.2016	100	108.768	99.233	99.455	2998.168	3004.873	997.769	1.93	2379	24.30	1.00	1.00		6.6330		100.0000	2756.5606	0.003		100.0232	2763.2726	0.023	3.794			100.0232	2763.2726	0.023	3.794												3.794	0.019	
28.09.2016	100	108.760	99.252	99.474	2998.520	3005.236	997.765	1.93	2381	24.30	1.00	1.00		6.6330		100.0000	2757.4294	0.016		100.0355	2764.1507	0.035	3.808			100.0355	2764.1507	0.035	3.808													3.808	0.031
28.09.2016	140	77.358	139.714	140.031	3002.224	3009.030	997.738	1.51	2384	24.30	1.00	1.00		6.6330		100.0000	3881.5519	0.016		100.0158	3890.5853	0.022	3.843			100.0158	3890.5853	0.022	3.843													3.843	0.030
28.09.2016	140	77.357	139.786	140.104	3003.729	3010.552	997.733	1.51	2386	24.30	1.00	1.00		6.6330		100.0000	3883.6507	0.018		100.0164	3892.4015	0.019	3.850			100.0164	3892.4015	0.019	3.850													3.850	0.031
28.09.2016	140	77.351	139.733	140.051	3002.360	3009.189	997.730	1.51	2387	24.30	1.00	1.00		6.6330		100.0000	3881.8218	0.009		100.0089	3891.9776	0.017	3.870			100.0089	3891.9776	0.017	3.870													3.870	0.023
28.09.2016	140	77.354	139.729	140.048	3002.384	3009.223	997.727	1.51	2389	24.30	1.00	1.00		6.6330		100.0000	3881.8218	0.009		100.0106	3891.7800	0.011	3.886			100.0106	3891.7800	0.011	3.886													3.886	0.025
28.09.2016	180	60.191	179.272	179.677	2997.398	3004.169	997.746	2.06	2391	24.30	1.00	1.00		6.6330		100.0000	4980.8000	0.020		100.0203	4992.4803	0.029	3.907			100.0203	4992.4803	0.029	3.907													3.907	0.036
28.09.2016	180	60.178	179.307	179.713	2997.312	3004.091	997.743	2.06	2392	24.30	1.00	1.00		6.6330		100.0000	4981.7556	0.020		100.0242	4993.2993	0.024	3.917			100.0242	4993.2993	0.024	3.917													3.917	0.036
28.09.2016	180	60.193	179.526	179.933	3000.725	3008.530	997.738	2.06	2394	24.30	1.00	1.00		6.6330		100.0000	4985.5679	-0.025		99.9747	4996.9944	-0.023	3.939			99.9747	4996.9944	-0.023	3.939												3.939	-0.010	
28.09.2016	180	60.191	179.451	179.859	3000.369	3007.181	997.735	2.07	2395	24.30	1.00	1.00		6.6330		100.0000	4985.4010	0.013		100.0129	4996.8310	0.015	3.954			100.0129	4996.8310	0.015	3.954													3.954	0.029
28.09.2016	180	60.200	179.649	180.057	3004.122	3010.954	997.731	2.07	2397	24.30	1.00	1.00		6.6330		100.0000	4985.1558	-0.102		99.9016	4996.6744	-0.098	3.970			99.9016	4996.6744	-0.098	3.970													3.970	-0.086
28.09.2016	200	54.005	200.087	200.549	3001.756	3008.526	997.760	2.69	2401	24.40	1.00	1.00		6.6330		100.0000	5558.5987	0.006		100.0229	5572.0684	0.023	4.006			100.0229	5572.0684	0.023	4.006												4.006	0.022	
28.09.2016	200	54.003	200.254	200.706	3003.952	3010.734	997.747	2.70	2402	24.30	1.00	1.00		6.6330		100.0000	5563.8487	0.022		100.0244	5576.5192	0.024	4.016			100.0244	5576.5192	0.024	4.016													4.016	0.038
28.09.2016	200	54.021	200.192	200.645	3004.056	3010.849	997.744	2.69	2403	24.40	1.00	1.00		6.6330		100.0000	5561.4125	0.009		100.0107	5575.1956	0.011	4.048			100.0107	5575.1956	0.011	4.048													4.048	0.025
28.09.2016	200	54.002	200.219	200.672	3003.414	3010.219	997.739	2.69	2405	24.40	1.00	1.00																															

NIST Laboratory - Day#2

Data report NIST: Day#2														*Original data set															
Date	Nominal flowrate	V _{nom} [m ³ /h]	Laboratory reference				Fluid				Ambient conditions				Turbine meter		Coriolis_Mass		Coriolis_Vol		Temperature correction of meter error								
			Meas-urment time	Standard mass flowrate	Standard volume flowrate	Mass	Volume	Water density	Line pressure	P _{fluid}	T _{fluid}	Water temp.	Air temp.	Air pressure	N	K _v	Meter error	k _{nominal}	100,000	k _{nominal}	100,000	Pulses/Liter	T _{nom}	20	°C	Corrected turbine meter error	Coriolis_Mass error	e _{meter}	
		[s]	[m ³ /h]	[m ³ /h]	[m ³ /h]	[kg/m ³]	[bar]	[bar]	[°C]	[°C]	[°C]	[bar]	[Pulses]	[Pulses/Liter]	[%]	[Pulses]	[Pulses/kg]	[Pulses/Liter]	[Pulses]	[Pulses/Liter]	[Hz]	[Pulses/Liter]	[°C]	[%]	[%]	[Pulses/Liter]	[%]	[%]	
29.09.2016	30	120.154	30.099	30.167	1004.597	997.755	1.62	23.80	24.10	1.00	1.00	100.1914	837.6938	0.000	100.1950	835.6089	0.000	3.804	0.022										
29.09.2016	30	120.149	30.097	30.165	1004.485	1006.757	1.63	23.85	24.00	1.01	1.01	99.9891	835.9385	-0.011	100.0184	838.0746	0.018	3.846	0.031										
29.09.2016	30	120.150	30.082	30.151	1003.995	997.735	1.64	23.89	23.90	1.01	1.01	99.9453	835.1608	-0.055	99.9665	837.2347	-0.034	3.886	-0.032										
29.09.2016	30	120.156	30.062	30.130	1003.354	997.725	1.64	23.93	23.90	1.01	1.01	99.9669	834.7682	-0.033	100.0004	836.7685	-0.022	3.926	-0.011										
29.09.2016	30	120.152	29.883	29.951	997.357	999.648	1.65	23.99	23.90	1.01	1.01	100.0164	830.2119	0.016	100.0004	831.9854	0.000	3.993	0.039										
29.09.2016	60	179.908	59.903	60.042	2993.631	997.691	1.88	24.10	24.00	1.01	1.01	100.0054	1664.0727	0.005	100.0181	1668.1355	0.018	4.102	0.030										
29.09.2016	60	179.913	59.922	60.061	2994.634	997.684	1.88	24.13	24.00	1.01	1.01	99.9665	1663.9319	-0.034	99.9699	1668.3881	0.002	4.129	-0.009										
29.09.2016	60	179.945	59.915	60.054	2994.811	997.678	1.89	24.15	24.00	1.01	1.01	99.9691	1663.7795	-0.031	99.9999	1668.1654	0.000	4.154	-0.006										
29.09.2016	60	179.918	59.905	60.045	2993.872	997.672	1.89	24.18	24.00	1.01	1.01	100.0113	1664.2107	0.011	100.0318	1668.4348	0.032	4.177	0.036										
29.09.2016	60	179.938	59.932	60.072	2995.584	997.667	1.89	24.20	24.00	1.01	1.01	99.9780	1664.4157	-0.022	99.9901	1668.5099	-0.010	4.201	0.003										
29.09.2016	100	108.615	99.292	99.525	2995.713	997.661	1.94	24.23	24.00	1.01	1.01	100.0031	2758.1907	0.003	100.0194	2765.1075	0.019	4.229	0.020										
29.09.2016	100	108.610	99.321	99.554	2996.458	997.657	1.94	24.24	24.00	1.01	1.01	99.9564	2757.7021	-0.044	99.9802	2764.8363	-0.020	4.242	-0.026										
29.09.2016	100	108.604	99.332	99.566	2996.641	997.654	1.94	24.26	24.00	1.01	1.01	100.0075	2759.4347	0.007	100.0217	2766.3180	0.022	4.258	0.025										
29.09.2016	100	108.617	99.285	99.518	2995.558	997.650	1.94	24.27	24.00	1.01	1.01	99.9948	2757.7625	-0.005	100.0240	2765.0668	0.024	4.273	0.012										
29.09.2016	100	108.620	99.370	99.604	2996.206	997.645	1.94	24.29	24.00	1.01	1.01	99.9896	2759.9791	-0.010	100.0028	2766.8595	0.003	4.289	0.007										
29.09.2016	140	77.481	139.372	139.702	2999.648	997.638	2.02	24.33	24.00	1.01	1.01	100.0036	3871.5792	0.004	100.0200	3881.3832	0.020	4.332	0.019										
29.09.2016	140	77.488	139.483	139.813	3002.305	997.635	2.02	24.34	24.00	1.01	1.01	99.9345	3871.9813	-0.065	99.9419	3881.4494	-0.058	4.345	-0.050										
29.09.2016	140	77.480	139.424	139.755	3000.727	997.632	2.02	24.36	24.00	1.01	1.01	100.0029	3872.9947	0.003	100.0317	3883.3085	0.032	4.356	0.019										
29.09.2016	140	77.487	139.381	139.712	3000.059	997.629	2.02	24.37	24.00	1.01	1.01	100.0032	3871.8208	0.003	100.0358	3882.3864	0.036	4.368	0.019										
29.09.2016	140	77.487	139.431	139.763	3001.145	997.626	2.02	24.38	24.10	1.01	1.01	100.0088	3873.4217	0.009	100.0309	3883.4985	0.031	4.379	0.025										
29.09.2016	180	60.372	178.676	179.101	2996.397	997.623	2.13	24.41	24.00	1.01	1.01	99.8958	4958.0436	-0.104	99.9104	4970.8832	-0.090	4.410	-0.087										
29.09.2016	180	60.375	178.431	178.857	2992.558	2999.694	997.621	2.14	24.42	24.10	1.01	100.0137	4957.1014	0.104	100.0212	4969.2961	0.021	4.420	0.031										
29.09.2016	180	60.375	178.518	178.944	2993.887	997.618	2.13	24.43	24.10	1.01	1.01	100.0116	4959.4152	0.012	100.0149	4971.4175	0.015	4.430	0.029										
29.09.2016	180	60.369	178.548	178.975	2994.121	997.614	2.12	24.44	24.10	1.01	1.01	100.0036	4959.8498	0.004	100.0075	4971.9031	0.007	4.444	0.021										
29.09.2016	200	60.390	178.534	178.961	2994.910	997.611	2.13	24.46	24.10	1.01	1.01	100.0069	4959.6144	0.007	100.0161	4971.9453	0.016	4.457	0.025										
29.09.2016	200	60.396	199.686	200.163	3000.618	997.618	2.48	24.49	24.30	1.01	1.01	100.0041	5547.0608	0.004	99.9995	5560.0479	-0.001	4.493	-0.002										
29.09.2016	200	54.088	199.651	200.129	2999.660	3006.833	997.614	2.48	24.50	1.01	1.01	99.9998	5545.8561	0.000	100.0006	5559.1658	0.001	4.505	0.018										
29.09.2016	200	54.077	199.626	200.104	2998.663	3005.844	997.611	2.47	24.52	1.01	1.01	100.0107	5545.7536	0.011	100.0289	5560.0491	0.029	4.519	0.028										
29.09.2016	200	54.072	199.585	200.064	2997.767	3004.954	997.608	2.48	24.53	1.00	1.00	100.0059	5544.3571	0.006	100.0148	5558.1465	0.015	4.532	0.024										
29.09.2016	200	54.089	199.466	199.945	2996.944	3004.139	997.605	2.49	24.55	1.00	1.00	100.0018	5540.8287	0.002	100.0116	5554.6738	0.012	4.545	0.020										

NIST Laboratory – Day#3

Data report NIST: Day#3											*Original data set								Temperature correction of meter error											
Date	Nominal flowrate V _{nom} [m³/h]	Measur- ment time t [s]	Standard mass flowrate V _{ref} [m³/h]	Laboratory reference					Fluid			Ambient conditions			Turbine meter			Coriolis_Mass			Coriolis_Vol			Temperature correction of meter error						
				Standard volume flowrate V _{ref} [m³/h]	Standard mass flowrate ṁ _{ref} [kg]	Volume V _{ref} [m³]	Water density ρ _{fluid} [kgm³]	Water pressure P _{fluid} [bar]	Line pressure P _{line} [bar]	Water temp. T _{fluid} [°C]	Air temp. T _{air} [°C]	Air pressure P _{air} [bar]	Pulse count N	K-factor K _v [Pulses/Liter]	e _v [%]	Meter error	Meter output frequency [Hz]	K-factor K _m [Pulses/kg]	e _m [%]	Meter error	Pulse count N	K-factor K _v [Pulses/Liter]	e _v [%]	Meter output frequency [Hz]	Meter error	Pulse count N	K-factor K _m [Pulses/Liter]	e _m [%]	Meter error	(T _{fluid} - T _{nom}) ΔT _{fluid} [°C]
29.09.2016	30	119,782	30,035	30,108	999,334	1001,762	997,576	1,92	24,30	1,01	100,0180	834,432	0,018	4,568	100,0451	836,6972	0,045	4,568	100,0451	836,6972	0,045	4,568	0,043							
29.09.2016	30	119,791	30,065	30,138	1000,404	1002,847	997,564	1,92	24,62	1,00	99,9200	834,8096	-0,038	4,617	99,9811	837,0480	-0,019	4,617	99,9811	837,0480	-0,019	4,617	-0,013							
29.09.2016	30	119,776	30,058	30,132	1000,067	1000,519	997,554	1,92	24,66	1,00	99,9981	834,9298	-0,002	4,657	100,0435	837,3566	0,043	4,657	100,0435	837,3566	0,043	4,657	0,023							
29.09.2016	30	119,782	30,050	30,124	999,841	1002,312	997,535	1,92	24,73	1,01	99,9629	834,5765	-0,017	4,729	100,0069	836,1435	0,007	4,729	100,0069	836,1435	0,007	4,729	0,028							
29.09.2016	30	119,767	30,025	30,099	998,878	1001,354	997,527	1,92	24,76	1,00	99,9648	833,7242	-0,035	4,758	100,0063	831,5452	0,006	4,758	100,0063	831,5452	0,006	4,758	-0,010							
29.09.2016	30	119,770	29,859	29,934	993,389	995,375	997,504	1,92	24,85	1,00	99,9819	829,2664	-0,018	4,849	100,0063	831,5452	0,006	4,849	100,0063	831,5452	0,006	4,849	0,008							
29.09.2016	30	119,812	30,059	30,134	1000,382	1002,893	997,496	1,92	24,88	1,00	99,9550	834,5845	-0,045	4,878	100,0078	834,2955	0,008	4,878	100,0078	834,2955	0,008	4,878	-0,019							
29.09.2016	30	119,781	29,980	30,055	997,495	1000,012	997,483	1,93	24,93	1,00	99,9494	832,3421	-0,051	4,905	100,0078	834,2955	0,008	4,905	100,0078	834,2955	0,008	4,905	-0,008							
29.09.2016	30	119,781	29,950	30,025	986,496	990,017	997,476	1,93	24,96	1,01	99,9901	831,8480	-0,010	4,959	100,0301	834,2866	0,030	4,959	100,0301	834,2866	0,030	4,959	0,016							
29.09.2016	100	108,727	99,333	99,587	3000,060	3007,738	997,447	1,57	25,00	1,01	99,9861	2766,8685	-0,014	5,001	100,0066	2766,8970	0,007	5,001	100,0066	2766,8970	0,007	5,001	0,006							
29.09.2016	100	108,710	99,373	99,627	3000,792	3008,481	997,444	1,57	25,01	1,01	100,0036	2760,6546	0,004	5,015	100,0183	2767,9863	0,018	5,015	100,0183	2767,9863	0,018	5,015	0,024							
29.09.2016	100	108,724	99,435	99,690	3003,026	3010,730	997,441	1,57	25,03	1,01	99,9901	2761,2980	-0,010	5,026	100,0118	2769,4828	0,012	5,026	100,0118	2769,4828	0,012	5,026	0,010							
29.09.2016	100	108,719	99,461	99,716	3003,677	3011,390	997,439	1,57	25,03	1,00	100,0068	2762,9839	0,007	5,035	100,0282	2770,6708	0,028	5,035	100,0282	2770,6708	0,028	5,035	0,027							
29.09.2016	100	108,721	99,457	99,713	3003,637	3011,359	997,436	1,57	25,05	1,00	100,0068	2762,8971	0,007	5,047	100,0267	2770,5510	0,027	5,047	100,0267	2770,5510	0,027	5,047	0,027							
29.09.2016	100	108,708	99,496	99,752	3004,454	3012,189	997,432	1,57	25,06	1,00	99,9891	2763,4772	-0,011	5,062	100,0114	2771,2116	0,011	5,062	100,0114	2771,2116	0,011	5,062	0,009							
29.09.2016	100	108,728	99,458	99,714	3003,839	3011,585	997,428	1,57	25,07	1,00	100,0002	2762,7213	0,000	5,074	100,0082	2770,6651	0,008	5,074	100,0082	2770,6651	0,008	5,074	0,020							
29.09.2016	100	108,716	99,541	99,798	3006,030	3013,792	997,425	1,57	25,09	1,00	100,0079	2765,2513	0,008	5,091	100,0271	2772,9247	0,027	5,091	100,0271	2772,9247	0,027	5,091	0,028							
29.09.2016	100	108,730	99,526	99,783	3005,949	3013,771	997,421	1,58	25,11	1,00	99,9440	2763,0544	-0,056	5,105	99,9730	2771,0021	-0,027	5,105	99,9730	2771,0021	-0,027	5,105	-0,036							
29.09.2016	100	108,716	99,641	99,899	3009,045	3016,837	997,417	1,57	25,12	1,00	99,9503	2766,4312	-0,049	5,122	99,9603	2773,8588	-0,040	5,122	99,9603	2773,8588	-0,040	5,122	-0,029							
29.09.2016	200	53,904	200,288	200,788	2988,954	3006,592	997,459	2,72	25,15	1,00	100,0047	5564,3584	0,005	5,146	100,0117	5578,9079	0,012	5,146	100,0117	5578,9079	0,012	5,146	0,025							
29.09.2016	200	53,913	200,306	200,817	2989,735	3007,375	997,459	2,71	25,15	1,00	100,0023	5563,8110	0,005	5,147	100,0159	5579,1270	0,016	5,147	100,0159	5579,1270	0,016	5,147	0,026							
29.09.2016	200	53,898	200,435	200,946	3000,817	3008,465	997,458	2,71	25,15	1,00	100,0058	5564,8910	0,006	5,154	100,0080	5582,8657	0,008	5,154	100,0080	5582,8657	0,008	5,154	0,029							
29.09.2016	200	53,911	200,330	200,841	3000,013	3007,665	997,456	2,72	25,16	1,00	100,0085	5568,0556	0,009	5,163	100,0105	5579,9953	0,010	5,163	100,0105	5579,9953	0,010	5,163	0,028							
29.09.2016	200	53,884	200,220	200,732	2996,872	3008,537	997,449	2,71	25,19	1,00	100,0216	5562,8750	0,022	5,190	100,0305	5577,5987	0,031	5,190	100,0305	5577,5987	0,031	5,190	0,042							
29.09.2016	200	53,927	200,380	200,894	3001,613	3009,304	997,445	2,72	25,21	1,00	100,0043	5566,5563	0,004	5,211	100,0108	5580,9796	0,014	5,211	100,0108	5580,9796	0,014	5,211	0,025							
29.09.2016	200	53,906	200,324	200,838	2999,645	3007,343	997,440	2,72	25,23	1,00	100,0144	5564,9712	0,007	5,228	100,0144	5579,6473	0,014	5,228	100,0144	5579,6473	0,014	5,228	0,028							
29.09.2016	200	53,905	200,289	200,804	2999,058	3006,767	997,436	2,71	25,24	1,00	100,0032	5563,7671	0,003	5,237	100,0238	5579,2180	0,024	5,237	100,0238	5579,2180	0,024	5,237	0,024							
29.09.2016	200	53,881	200,366	200,882	2988,891	3006,611	997,432	2,72	25,25	1,01	99,9971	5565,9653	-0,003	5,254	100,0021	5580,1690	0,002	5,254	100,0021	5580,1690	0,002	5,254	0,018							

CENAM Laboratory – Day#1

Data report CENAM: Day#1		*Original data set											Temperature correction of meter error																						
Date	Nominal flowrate V _{nom} [m³/h]	Measu-ment time	Laboratory reference											Turbine meter						Coriolis_Mass						Coriolis_Vol						Corrected meter error			
			Standard mass flowrate	Standard volume flowrate	Mass	Volume	Water density ρ _{fluid} [kg/m³]	Line pressure P _{line} [bar]	Water temp. T _{water} [°C]	Air temp.		Air pressure P _{air} [bar]	Water density ρ _{fluid} [kg/m³]	Pulse count	K-factor	Meter error	K _{nom}	Pulse count	K-factor	Meter error	K _{vol}	Pulse count	K-factor	Meter error	e _v [%]	K _{vol}	Pulse count	K-factor	Meter error	e _v [%]	T _{nom} [°C]	e _{vol} [%]	e _{Corbis} [%]	e _{Corbis} [%]	
										T _{air} [°C]	P _{air} [bar]																								ΔT _{fluid} [°C]
V _{nom} [m³/h]	[m³/h]	[s]	[m³/h]	[m³/h]	[kg]	[m³]	[kg/m³]	[bar]	[°C]	[°C]	[bar]	[Pulses]	[Pulses/Liter]	[%]	[Pulses]	[Pulses/kg]	[%]	[Pulses]	[Pulses/Liter]	[%]	[Pulses]	[Pulses/Liter]	[%]	[Pulses]	[Pulses/Liter]	[%]	[Pulses]	[Pulses/Liter]	[%]	[°C]	[%]	[%]	[%]		
21.02.2017	60	180.123	30.051	30.108	1503.561	1.506	998.087	2.99	23.53	19.57	0.81	9992	6.6329	-0.002	150412	100.0372	0.037	150434	100.1261	0.126	150438	100.1198	0.120	150618	100.1198	0.120	3.540	-0.002	0.052						
21.02.2017	30	180.123	30.009	30.067	1501.500	1.504	998.087	2.99	23.56	19.68	0.81	9979	6.6329	-0.002	150679	100.0373	0.037	150682	100.1239	0.124	150778	100.1159	0.116	150986	100.1159	0.116	3.570	0.006	0.052						
21.02.2019	60	180.124	30.020	30.078	1502.040	1.505	998.082	2.99	23.57	19.88	0.81	9984	6.6378	0.071	150169	100.0307	0.031	150586	100.1120	0.122	150566	100.1200	0.122	150566	100.1200	0.122	3.600	0.005	0.049						
21.02.2020	30	180.125	29.998	30.056	1500.937	1.504	998.080	2.99	23.57	20.02	0.81	9976	6.6337	0.011	150150	100.0375	0.037	150566	100.1200	0.122	150566	100.1200	0.122	150566	100.1200	0.122	3.600	0.005	0.049						
21.02.2017	60	90.126	60.047	60.168	1503.264	1.506	998.074	2.99	23.60	20.28	0.81	10028	6.6580	0.376	150366	100.0364	0.036	150777	100.1066	0.107	150777	100.1066	0.107	150777	100.1066	0.107	3.600	0.383	0.049						
21.02.2017	60	90.126	60.034	60.150	1502.963	1.506	998.072	2.99	23.61	20.35	0.81	10026	6.6580	0.376	150337	100.0271	0.027	150747	100.1065	0.106	150747	100.1065	0.106	150747	100.1065	0.106	3.610	0.383	0.050						
21.02.2018	60	90.125	60.029	60.145	1502.823	1.506	998.075	3.00	23.60	20.38	0.81	10025	6.6579	0.376	150337	100.0331	0.033	150741	100.1121	0.112	150741	100.1121	0.112	150741	100.1121	0.112	3.600	0.383	0.056						
21.02.2019	60	90.126	60.036	60.151	1502.983	1.506	998.074	2.99	23.60	20.40	0.81	10027	6.6586	0.385	150338	100.0264	0.026	150746	100.1047	0.105	150746	100.1047	0.105	150746	100.1047	0.105	3.600	0.392	0.049						
21.02.2020	60	90.125	60.050	60.166	1503.343	1.506	998.072	3.00	23.61	20.44	0.81	10030	6.6589	0.391	150370	100.0238	0.024	150777	100.1012	0.101	150777	100.1012	0.101	150777	100.1012	0.101	3.610	0.398	0.046						
21.02.2017	100	54.130	99.984	100.178	1503.376	1.506	998.062	2.99	23.65	20.57	0.81	10038	6.6640	0.468	150386	100.0322	0.032	150785	100.1032	0.103	150785	100.1032	0.103	150785	100.1032	0.103	3.650	0.465	0.047						
21.02.2017	100	54.131	99.997	100.191	1503.586	1.507	998.062	1.507	23.65	20.63	0.81	10039	6.6638	0.464	150408	100.0329	0.033	150808	100.1045	0.105	150808	100.1045	0.105	150808	100.1045	0.105	3.650	0.461	0.048						
21.02.2018	100	54.131	100.006	100.200	1503.715	1.507	998.059	2.98	23.66	20.70	0.81	10040	6.6638	0.465	150417	100.0302	0.030	150814	100.0996	0.100	150814	100.0996	0.100	150814	100.0996	0.100	3.660	0.462	0.045						
21.02.2019	100	54.130	100.003	100.198	1503.665	1.507	998.057	2.98	23.67	20.80	0.81	10040	6.6640	0.468	150413	100.0309	0.031	150810	100.1001	0.100	150810	100.1001	0.100	150810	100.1001	0.100	3.670	0.465	0.046						
21.02.2017	140	247.198	140.069	140.345	961.7988	9.637	998.032	2.98	23.77	21.47	0.81	64271	6.6692	0.546	961965	100.0173	0.017	96446	100.0779	0.078	96446	100.0779	0.078	96446	100.0779	0.078	3.770	0.525	0.031						
21.02.2018	140	247.198	140.054	140.331	961.6083	9.635	998.027	2.98	23.79	21.52	0.81	64261	6.6698	0.540	961979	100.0188	0.018	964350	100.0779	0.078	964350	100.0779	0.078	964350	100.0779	0.078	3.790	0.519	0.033						
21.02.2018	140	247.198	140.041	140.318	961.6083	9.635	998.020	2.98	23.82	21.62	0.81	64250	6.6683	0.532	961796	100.0195	0.020	964260	100.0772	0.077	964260	100.0772	0.077	964260	100.0772	0.077	3.810	0.516	0.034						
21.02.2020	140	247.198	140.032	140.311	961.5475	9.635	998.015	2.98	23.84	21.74	0.81	64245	6.6682	0.530	961752	100.0213	0.021	964314	100.0783	0.078	964314	100.0783	0.078	964314	100.0783	0.078	3.840	0.509	0.035						
21.02.2017	180	192.200	180.247	180.612	962.3188	9.643	997.979	3.00	23.99	22.00	0.81	64356	6.6741	0.619	962511	100.0200	0.020	964333	100.0690	0.069	964333	100.0690	0.069	964333	100.0690	0.069	3.990	0.603	0.036						
21.02.2017	180	192.200	180.243	180.610	962.2985	9.643	997.969	3.00	24.03	22.10	0.81	64354	6.6739	0.617	962505	100.0215	0.021	964288	100.0696	0.070	964288	100.0696	0.070	964288	100.0696	0.070	4.090	0.601	0.037						
21.02.2018	180	192.199	180.249	180.618	962.3284	9.643	997.961	3.00	24.06	22.15	0.81	64351	6.6734	0.609	962514	100.0193	0.019	964288	100.0668	0.067	964288	100.0668	0.067	964288	100.0668	0.067	4.060	0.592	0.035						
21.02.2019	180	192.200	180.230	180.600	962.2280	9.642	997.951	2.99	24.10	22.21	0.81	64341	6.6730	0.603	962418	100.0197	0.020	964842	100.0662	0.066	964842	100.0662	0.066	964842	100.0662	0.066	4.100	0.586	0.036						
21.02.2020	180	192.200	180.219	180.590	962.1675	9.641	997.944	2.99	24.13	22.27	0.81	64338	6.6730	0.603	962372	100.0213	0.021	964797	100.0671	0.067	964797	100.0671	0.067	964797	100.0671	0.067	4.130	0.587	0.038						
21.02.2017	200	173.203	200.393	200.811	964.1497	9.661	997.919	2.99	24.23	22.34	0.81	64498	6.6759	0.647	964327	100.0215	0.022	966736	100.0627	0.063	966736	100.0627	0.063	966736	100.0627	0.063	4.230	0.630	0.038						
21.02.2017	200	173.200	200.295	200.715	963.6391	9.657	997.906	2.98	24.28	22.39	0.81	64466	6.6758	0.646	963828	100.0196	0.020	966337	100.0596	0.060	966337	100.0596	0.060	966337	100.0596	0.060	4.280	0.628	0.037						
21.02.2018	200	173.200	200.288	200.710	963.6093	9.656	997.899	2.99	24.31	22.41	0.81	64460	6.6754	0.639	963827	100.0226	0.023	966337	100.0620	0.062	966337	100.0620	0.062	966337	100.0620	0.062	4.310	0.621	0.040						
21.02.2019	200	173.200	200.248	200.672	963.4817	9.655	997.889	2.99	24.35	22.42	0.81	64446	6.6752	0.636	963828	100.0217	0.022	966042	100.0606	0.061	966042	100.0606	0.061	966042	100.0606	0.061	4.350	0.618	0.039						
21.02.2020	200	173.200	200.228	200.653	963.3189	9.654	997.881	2.99	24.38	22.42	0.81	64439	6.6751	0.635	963511	100.0199	0.020	965925	100.0581	0.058	965925	100.0581	0.058	965925	100.0581	0.058	4.380	0.617	0.037						

CENAM Laboratory – Day#2

Data report CENAM: Day#2																			*Original data set					Temperature correction of meter error							
Date	Nominal flowrate V_{nom} [m³/h]	Measur-ment time [s]	Laboratory reference							Fluid				Ambient conditions				Turbine meter		Coriolis_Mass				Coriolis_Vol				Corrected meter error			
			Standard mass flowrate V_{ref} [m³/h]	Standard volume flowrate V_{ref} [m³/h]	Mass m_{ref} [kg]	Volume V_{ref} [m³]	Water density ρ_{fluid} [kg/m³]	Line pressure p_{fluid} [bar]	Water temp. T_{fluid} [°C]	Air temp. T_{air} [°C]	Air pressure p_{air} [bar]	Pulse count	K-factor K_v [Pulses/Liter]	Meter error e_v [%]	e_{cor} [%]	Pulse count	K-factor K_m [Pulses/kg]	Meter error e_m [%]	e_{cor} [%]	Pulse count	K-factor K_v [Pulses/Liter]	Meter error e_v [%]	e_{cor} [%]	Pulse count	K-factor K_v [Pulses/Liter]	Meter error e_v [%]	e_{cor} [%]		T_{nom} [°C]	20	°C
22.02.2017	30	180.123	29.966	60.141	60.287	1505.637	1.509	997.994	2.99	24.15	20.46	0.81	10044	6.6572	0.365	150597	100.0721	0.022	151033	100.1054	0.105	4.130	0.371	0.047							
22.02.2018	30	180.124	29.936	60.163	60.287	1506.167	1.509	997.939	2.99	24.15	20.46	0.81	10048	6.6575	0.369	150646	100.0194	0.019	151082	100.1021	0.102	4.150	0.376	0.044							
22.02.2019	30	180.124	29.929	60.182	60.314	1506.837	1.510	997.939	2.99	24.15	20.51	0.81	10052	6.6572	0.364	150723	100.0261	0.026	151158	100.1080	0.108	4.150	0.371	0.051							
22.02.2020	30	180.122	29.927	60.198	60.316	1506.897	1.510	997.936	2.99	24.16	20.53	0.81	10055	6.6573	0.366	150763	100.0241	0.024	151197	100.1057	0.106	4.160	0.367	0.050							
22.02.2021	30	180.123	29.913	60.192	60.316	1506.888	1.500	997.945	2.95	24.12	20.27	0.81	9945	6.6510	-0.030	149681	100.0081	0.008	150120	100.0953	0.095	4.120	-0.035	0.031							
22.02.2017	60	90.126	60.141	60.265	1505.637	1.509	997.994	2.99	24.13	20.40	0.81	10044	6.6572	0.365	150597	100.0721	0.022	151033	100.1054	0.105	4.130	0.371	0.047								
22.02.2018	60	90.126	60.163	60.287	1506.167	1.509	997.939	2.99	24.15	20.46	0.81	10048	6.6575	0.369	150646	100.0194	0.019	151082	100.1021	0.102	4.150	0.376	0.044								
22.02.2019	60	90.126	60.182	60.314	1506.837	1.510	997.939	2.99	24.15	20.51	0.81	10052	6.6572	0.364	150723	100.0261	0.026	151158	100.1080	0.108	4.150	0.371	0.051								
22.02.2020	60	90.125	60.207	60.331	1507.267	1.510	997.939	2.99	24.15	20.58	0.81	10055	6.6573	0.366	150763	100.0241	0.024	151197	100.1057	0.106	4.160	0.372	0.049								
22.02.2017	100	541.30	99.946	100.154	1502.801	1.506	997.924	2.99	24.21	20.74	0.81	10033	6.6623	0.442	150329	100.0325	0.033	150751	100.1051	0.105	4.210	0.438	0.037								
22.02.2018	100	541.31	99.973	100.181	1503.231	1.506	997.924	2.99	24.21	20.80	0.81	10036	6.6624	0.444	150363	100.0266	0.027	150785	100.0990	0.099	4.210	0.440	0.044								
22.02.2019	100	541.31	99.953	100.161	1502.830	1.506	997.921	2.99	24.22	20.81	0.81	10033	6.6617	0.433	150327	100.0226	0.023	150748	100.0942	0.094	4.220	0.430	0.040								
22.02.2020	100	541.31	99.968	100.176	1503.150	1.506	997.921	2.99	24.22	20.86	0.81	10036	6.6628	0.449	150358	100.0286	0.029	150778	100.0995	0.099	4.220	0.446	0.046								
22.02.2021	100	541.31	99.988	100.176	1503.150	1.506	997.921	2.99	24.22	20.86	0.81	10036	6.6628	0.449	150358	100.0286	0.029	150778	100.0995	0.099	4.220	0.446	0.046								
22.02.2017	140	247.199	139.618	139.618	139.618	9.607	997.898	2.97	24.31	21.33	0.81	64070	6.6689	0.541	958812	100.0107	0.011	961435	100.0735	0.073	4.310	0.517	0.026								
22.02.2018	140	247.199	139.496	139.791	9578.681	9.599	997.893	2.97	24.33	21.44	0.81	64013	6.6688	0.539	957979	100.0116	0.012	960588	100.0727	0.073	4.330	0.515	0.027								
22.02.2019	140	247.200	139.421	139.716	9573.572	9.594	997.891	2.98	24.34	21.52	0.81	63972	6.6681	0.528	957477	100.0125	0.013	960078	100.0711	0.071	4.340	0.504	0.028								
22.02.2020	140	247.199	139.284	139.579	9564.159	9.584	997.886	2.99	24.36	21.61	0.81	63908	6.6679	0.526	956529	100.0118	0.012	959123	100.0727	0.073	4.360	0.502	0.028								
22.02.2021	140	247.199	139.251	139.546	9561.853	9.582	997.881	2.99	24.38	21.68	0.81	63891	6.6677	0.523	956310	100.0130	0.013	958900	100.0714	0.071	4.380	0.499	0.029								
22.02.2017	180	192.200	180.085	180.471	9614.502	9.635	997.857	3.00	24.48	21.80	0.81	64303	6.6738	0.615	961581	100.0156	0.014	964133	100.0641	0.064	4.480	0.597	0.031								
22.02.2018	180	192.200	180.039	180.429	9612.096	9.633	997.839	3.00	24.52	21.87	0.81	64289	6.6737	0.613	961417	100.0174	0.017	963967	100.0667	0.067	4.520	0.595	0.031								
22.02.2019	180	192.200	180.039	180.429	9612.096	9.633	997.839	3.00	24.55	21.92	0.81	64286	6.6736	0.612	961361	100.0158	0.016	963910	100.0642	0.064	4.550	0.593	0.034								
22.02.2020	180	192.200	180.073	180.465	9613.894	9.635	997.829	3.00	24.59	21.99	0.81	64301	6.6738	0.615	961521	100.0137	0.014	964699	100.0610	0.061	4.590	0.597	0.032								
22.02.2021	180	192.200	180.130	180.523	9616.897	9.638	997.821	2.99	24.62	22.01	0.81	64323	6.6740	0.618	961889	100.0207	0.021	964441	100.0675	0.068	4.620	0.599	0.039								
22.02.2017	200	173.201	200.080	200.540	9626.077	9.648	997.703	3.00	25.08	22.53	0.81	64005	6.6753	0.638	962745	100.0143	0.014	965316	100.0510	0.051	5.080	0.618	0.034								
22.02.2018	200	173.200	200.053	200.517	9624.779	9.647	997.689	2.98	25.13	22.52	0.81	64397	6.6753	0.638	962655	100.0184	0.018	965228	100.0540	0.054	5.130	0.617	0.039								
22.02.2019	200	173.200	200.068	200.532	9625.477	9.648	997.684	2.98	25.15	22.54	0.81	64001	6.6752	0.636	962708	100.0166	0.017	965285	100.0522	0.052	5.150	0.615	0.037								
22.02.2020	200	173.201	200.075	200.541	9625.876	9.648	997.677	2.98	25.18	22.58	0.81	64403	6.6751	0.634	962740	100.0158	0.016	965320	100.0508	0.051	5.180	0.614	0.036								
22.02.2021	200	173.200	200.108	200.576	9627.378	9.650	997.666	2.98	25.22	22.60	0.81	64412	6.6749	0.631	962873	100.0140	0.014	965458	100.0485	0.048	5.220	0.611	0.034								

CENAM Laboratory – Day#3

Data report CENAM: Day#3		*Original data set			Laboratory reference													Turbine meter										Coriolis_Mass										Coriolis_Vol										Temperature correction of meter error		
Date	Nominal flowrate [m³/h]	Measu-remment time [h]	Standard mass flowrate [kg/h]	Standard volume flowrate [m³/h]	V _{ref} [m³]	m _{ref} [kg]	Volume [m³]	Water density [kg/m³]	Line pressure [bar]	Water temp. [°C]	Air Temp. [°C]	Air pressure [bar]	Ambient conditions		K _{v, nom}		K _{m, nom}		K _{v, nom}		Meter error		K-factor		e _m		Pulses/Liter		T _{fluid - T_{nom}} [°C]	e _{con} [%]	e _{con} [%]																			
													N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N				N	N	N	N	N	N	N	N	N	N	N								
22.02.2017	30	180.123	29.932	30.001	1497.639	1.501	997.726	2.94	24.98	21.46	0.81	9967	6.6403	0.106	149750	99.9907	-0.009	150196	100.0605	0.061	4.980	0.102	0.017	5.020	0.122	0.024	149624	99.9975	-0.002	150068	100.0652	0.065	5.020	0.122	0.024															
22.02.2018	30	180.124	29.905	29.973	1496.277	1.500	997.716	2.95	25.02	21.57	0.81	9960	6.6413	0.125	149624	99.9975	-0.002	150068	100.0652	0.065	5.020	0.122	0.024	149997	100.0674	0.067	5.020	0.111	0.027	149954	100.0642	0.064	5.020	0.111	0.027															
22.02.2019	30	180.124	29.890	29.959	1495.537	1.499	997.716	2.95	25.02	21.64	0.81	10052	6.6406	0.115	149555	100.0009	0.001	149997	100.0674	0.067	5.040	0.089	0.037	151519	100.0754	0.075	5.040	0.089	0.037	151519	100.0754	0.075	5.040	0.089	0.037															
22.02.2020	30	180.123	30.191	30.260	1510.583	1.514	997.711	2.94	25.04	21.76	0.81	10052	6.6392	0.093	151074	100.0104	0.010	151519	100.0754	0.075	5.020	0.131	0.032	151433	100.0710	0.071	5.050	0.151	0.034	151433	100.0710	0.071	5.050	0.151	0.034															
22.02.2021	30	180.124	30.157	30.226	1508.891	1.512	997.708	2.94	25.05	21.94	0.81	10047	6.6430	0.155	150908	99.9953	-0.005	151433	100.0710	0.071	5.130	0.064	0.033	151249	100.0566	0.057	5.130	0.139	0.024	151249	100.0566	0.057	5.130	0.139	0.024															
22.02.2022	30	180.123	30.142	30.212	1508.139	1.512	997.688	2.94	25.13	22.22	0.81	10041	6.6425	0.143	150810	99.9974	-0.003	151249	100.0566	0.057	5.130	0.064	0.033	151224	100.0646	0.065	5.130	0.074	0.009	151143	100.0402	0.040	5.130	0.074	0.009															
22.02.2023	30	180.124	30.135	30.205	1507.768	1.511	997.687	2.94	25.13	22.24	0.81	10031	6.6375	0.068	150786	100.0061	0.006	151224	100.0646	0.065	5.150	0.022	0.022	151155	100.0524	0.052	5.150	0.138	0.002	151155	100.0524	0.052	5.150	0.138	0.002															
22.02.2024	30	180.124	30.126	30.196	1507.328	1.511	997.687	2.93	25.13	22.26	0.81	10029	6.6381	0.077	150706	99.9822	-0.018	151143	100.0402	0.040	5.160	0.457	0.035	151025	100.0658	0.066	5.160	0.457	0.035	151025	100.0658	0.066	5.160	0.457	0.035															
22.02.2025	30	180.123	30.125	30.194	1507.257	1.511	997.683	2.95	25.15	22.28	0.81	10035	6.6424	0.141	150719	99.9955	-0.004	151155	100.0524	0.052	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029															
22.02.2026	30	180.123	30.125	30.194	1507.257	1.511	997.683	2.95	25.15	22.28	0.81	10035	6.6424	0.141	150719	99.9955	-0.004	151155	100.0524	0.052	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029															
22.02.2027	100	54.130	100.142	100.375	1505.758	1.509	997.681	2.98	25.16	22.33	0.81	10057	6.6635	0.460	150628	100.0068	0.007	151065	100.0566	0.057	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029															
22.02.2018	100	54.130	100.161	100.394	1506.037	1.510	997.678	2.97	25.17	22.37	0.81	10059	6.6636	0.461	150629	100.0161	0.016	151058	100.0566	0.057	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029															
22.02.2019	100	54.130	100.172	100.405	1506.187	1.510	997.678	2.97	25.17	22.40	0.81	10060	6.6636	0.461	150629	100.0161	0.016	151058	100.0566	0.057	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029															
22.02.2020	100	54.130	100.163	100.396	1506.047	1.510	997.679	2.98	25.17	22.42	0.81	10059	6.6636	0.461	150629	100.0161	0.016	151058	100.0566	0.057	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029															
22.02.2021	100	54.130	100.178	100.412	1506.287	1.510	997.676	2.98	25.18	22.41	0.81	10061	6.6638	0.465	150639	100.0068	0.007	151065	100.0566	0.057	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029	151058	100.0588	0.059	5.170	0.458	0.029															
22.02.2022	100	54.130	100.162	100.395	1506.037	1.510	997.679	2.97	25.17	22.39	0.81	10059	6.6636	0.462	150633	100.0115	0.011	151050	100.0603	0.060	5.170	0.458	0.029	151050	100.0603	0.060	5.170	0.455	0.032	151050	100.0603	0.060	5.170	0.455	0.032															
22.02.2023	100	54.130	100.165	100.398	1506.077	1.510	997.674	2.98	25.19	22.40	0.81	10059	6.6634	0.458	150625	100.0115	0.011	151050	100.0603	0.060	5.170	0.455	0.032	151050	100.0603	0.060	5.170	0.455	0.032	151050	100.0603	0.060	5.170	0.455	0.032															
22.02.2024	100	54.130	100.183	100.416	1506.357	1.510	997.676	2.97	25.18	22.42	0.81	10061	6.6635	0.460	150628	100.0148	0.014	151052	100.0588	0.059	5.170	0.458	0.029	151052	100.0588	0.059	5.170	0.458	0.029	151052	100.0588	0.059	5.170	0.458	0.029															
22.02.2025	100	54.130	100.180	100.414	1506.316	1.510	997.676	2.97	25.18	22.45	0.81	10059	6.6624	0.443	150638	100.0042	0.004	151063	100.0632	0.063	5.180	0.461	0.027	151065	100.0566	0.057	5.180	0.461	0.027	151065	100.0566	0.057	5.180	0.461	0.027															
22.02.2026	100	54.130	100.310	100.544	1508.267	1.512	997.673	2.97	25.19	22.46	0.81	10073	6.6630	0.452	150851	100.0161	0.016	151276	100.0645	0.064	5.180	0.461	0.027	151276	100.0645	0.064	5.180	0.461	0.027	151276	100.0645	0.064	5.180	0.461	0.027															
22.02.2017	200	173.199	199.662	200.136	9605.941	9.629	997.634	3.02	25.35	22.60	0.81	64311	6.6791	0.695	960707	100.0118	0.012	962299	100.0443	0.044	5.350	0.673	0.033	962299	100.0443	0.044	5.350	0.673	0.033	962299	100.0443	0.044	5.350	0.673	0.033															
22.02.2018	200	173.200	199.529	200.002	9599.529	9.622	997.631	3.02	25.36	22.64	0.81	64266	6.6788	0.691	960056	100.0107	0.011	962648	100.0432	0.043	5.380	0.668	0.032	962648	100.0432	0.043	5.380	0.668	0.032	962648	100.0432	0.043	5.380	0.668	0.032															
22.02.2019	200	173.200	199.497	199.972	9598.025	9.621	997.626	3.02	25.38	22.68	0.81	64255	6.6787	0.689	959903	100.0105	0.010	962495	100.0425	0.042	5.380	0.668	0.032	962495	100.0425	0.042	5.380	0.668	0.032	962495	100.0425	0.042	5.380	0.668	0.032															
22.02.2020	200	173.200	199.433	199.909	9594.923	9.618	997.603	3.02	25.42	22.72	0.81	64236	6.6788	0.691	959694	100.0112	0.011	962195	100.0426	0.043	5.470	0.665	0.032	962195	100.0426	0.043	5.470	0.665	0.032	962195	100.0426	0.043	5.470	0.665	0.032															
22.02.2021	200	173.200	199.453	199.933	9595.922	9.619	997.619	3.02	25.47	22.74	0.81	64241	6.6786	0.687	959694	100.0106	0.011	962295	100.0412	0.041	5.480	0.663	0.032	962295	100.0412	0.041	5.480	0.663	0.032	962295	100.0412	0.041	5.480	0.663	0.032															
22.02.2022	200	173.200	199.360	199.840	9591.416	9.615	997.597	3.02	25.49	22.77	0.81	64210	6.6784	0.685	959293	100.0158	0.016	961901	100.0467	0.047	5.480	0.663	0.032	961901	100.0467	0.047	5.480	0.663	0.032	961901	100.0467	0.047	5.480	0.663	0.032															
22.02.2023	200	173.200	199.378	199.860	9592.318	9.615	997.589	3.02	25.52	22.78	0.81	64214	6.6782	0.681	959332	100.0104	0.010	961946	100.0412	0.041	5.520	0.659	0.032	961946	100.0412	0.041	5.520	0.659	0.032	961946	100.0412	0.041	5.520	0.659	0.032															
22.02.2024	200	173.200	199.362	199.846	9591.517	9.615	997.579	3.02	25.56	22.81	0.80	64208	6.6780	0.679	959254	100.0107	0.011	961874	100.0410	0.041	5.560	0.657	0.032	961874	100.0410	0.041	5.560	0.657	0.032	961874	100.0410	0.041	5.560	0.657	0.032															
22.02.2025	200	173.199	199.344	199.829	9590.616	9.614	997.571	3.02	25.59	22.83	0.80	64200	6.6778	0.675	959165	100.0108	0.011	961789	100.0408	0.041	5.590	0.653	0.032	961789	100.0408	0.041	5.590	0.653	0.032	961789	100.0408	0.041	5.590	0.653	0.032															
22.02.2026	200	173.199	199.369	199.856	9591.817	9.615	997.561	3.03	25.63																																									

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Date	Nominal flowrate [m³/h]	Measur-remant time [s]	Standard mass flowrate [t/h]	Standard volume flowrate [m³/h]	Laboratory reference						Fluid			Ambient conditions			Turbine meter			Conolis_Mass			Conolis_Vol			Temperature correction of meter error																									
					V _{ref} [m³/h]	m _{ref} [kg]	V _{ref} [m³]	ρ _{water} [kg/m³]	P _{line} [bar]	T _{water} [°C]	T _{air} [°C]	P _{air} [bar]	N [Pulses]	K _v [Pulses/Liter]	e _v [%]	N [Pulses]	K _m [Pulses/Liter]	e _m [%]	N [Pulses]	K _v [Pulses/Liter]	e _v [%]	ΔT _{fluid - T_{nom}} [°C]	e _v [%]	e _m [%]	e _v [%]	Pulses/kg	K _{v, nom}	Pulses/Liter	T _{nom} [°C]	Corrected meter error																					
																															V _{ref} [m³]	m _{ref} [kg]	V _{ref} [m³]	ρ _{water} [kg/m³]	P _{line} [bar]	T _{water} [°C]	T _{air} [°C]	P _{air} [bar]	N [Pulses]	K _v [Pulses/Liter]	e _v [%]	N [Pulses]	K _m [Pulses/Liter]	e _m [%]	N [Pulses]	K _v [Pulses/Liter]	e _v [%]	ΔT _{fluid - T_{nom}} [°C]	e _v [%]	e _m [%]	e _v [%]
27.06.2017	30	658.479	30.195	30.311	523.068	5.544	996.198	2.695	28.79	32.18	1.00	36930	6.6611	0.423	525.62	100.0462	0.046	54.510	100.0172	0.017	8.424	0.084																													
27.06.2017	30	658.504	30.190	30.303	522.267	5.543	996.283	2.694	28.50	32.19	1.00	36919	6.6606	0.416	524.839	100.0384	0.038	54.439	100.0111	0.011	8.489	0.076																													
27.06.2017	30	658.442	30.187	30.298	521.266	5.542	996.329	2.697	28.34	32.26	1.00	36911	6.6607	0.418	525.330	100.0368	0.037	54.498	100.0666	0.067	8.337	0.074																													
27.06.2017	30	658.500	30.186	30.296	521.486	5.542	996.360	2.697	28.23	32.28	1.00	36911	6.6607	0.417	525.333	100.0338	0.034	54.478	100.0286	0.028	8.227	0.070																													
27.06.2017	30	658.600	30.182	30.291	521.567	5.542	996.382	2.694	28.15	32.31	1.00	36911	6.6607	0.417	525.345	100.0341	0.034	54.472	100.0019	0.002	8.149	0.070																													
27.06.2017	60	330.840	60.257	60.509	537.584	5.561	995.824	2.647	30.06	32.20	1.00	37089	6.6697	0.554	535.940	100.0328	0.033	55.033	100.0040	0.004	10.061	0.076																													
27.06.2017	60	330.837	60.242	60.495	536.188	5.559	995.813	2.644	30.10	32.10	1.00	37079	6.6695	0.551	535.781	100.0293	0.029	55.018	100.0018	0.002	10.100	0.072																													
27.06.2017	60	330.736	60.261	60.496	536.283	5.558	996.117	2.638	29.07	32.02	1.00	37076	6.6698	0.555	535.785	100.0341	0.034	55.016	100.0067	0.007	9.997	0.077																													
27.06.2017	60	330.777	60.273	60.504	537.990	5.559	996.177	2.635	28.86	31.93	1.00	37078	6.6696	0.552	535.972	100.0312	0.031	55.092	100.0950	0.095	8.864	0.072																													
27.06.2017	100	198.958	100.554	100.967	557.212	5.580	995.906	2.530	29.79	31.88	1.00	37264	6.6781	0.679	556.010	100.0520	0.052	58.125	100.0214	0.021	9.787	0.085																													
27.06.2017	100	198.758	100.555	100.969	557.100	5.575	995.899	2.537	29.81	32.15	1.00	37224	6.6775	0.671	555.404	100.0421	0.042	58.750	100.0081	0.008	9.810	0.060																													
27.06.2017	100	198.694	100.607	101.022	552.801	5.576	995.985	2.541	29.82	32.10	1.00	37230	6.6772	0.666	555.493	100.0383	0.038	58.756	100.0013	0.001	9.824	0.056																													
27.06.2017	100	198.834	100.614	101.030	557.106	5.580	995.891	2.545	29.84	32.15	1.00	37260	6.6774	0.669	555.943	100.0418	0.042	58.807	100.0114	0.011	9.837	0.075																													
27.06.2017	100	198.670	100.638	101.053	553.803	5.577	995.887	2.537	29.85	32.10	1.00	37239	6.6776	0.672	555.615	100.0423	0.042	58.746	100.0130	0.013	9.850	0.062																													
27.06.2017	140	143.354	140.059	140.628	577.234	5.600	995.957	2.396	29.62	31.78	1.00	37438	6.6855	0.792	557.946	100.0399	0.040	59.980	99.9987	-0.001	9.616	0.070																													
27.06.2017	140	143.097	140.079	140.649	568.034	5.591	995.946	2.390	29.65	31.71	1.00	37382	6.6865	0.806	557.094	100.0524	0.052	59.950	100.0146	0.015	9.654	0.083																													
27.06.2017	140	143.153	140.082	140.653	570.021	5.593	995.940	2.386	29.67	32.13	1.00	37391	6.6853	0.788	557.235	100.0364	0.036	59.903	100.0000	0.000	9.674	0.067																													
27.06.2017	140	143.303	139.978	140.549	572.023	5.595	995.935	2.394	29.69	32.05	1.00	37404	6.6855	0.792	557.427	100.0403	0.040	59.924	100.0067	0.007	9.690	0.076																													
27.06.2017	180	111.633	180.293	181.017	559.079	5.613	995.931	2.385	29.70	31.98	1.00	37408	6.6854	0.790	557.466	100.0344	0.034	59.603	100.0096	0.010	9.705	0.065																													
27.06.2017	180	111.633	180.293	181.017	559.079	5.613	995.931	2.385	29.70	31.98	1.00	37408	6.6854	0.790	557.466	100.0344	0.034	59.603	100.0096	0.010	9.705	0.065																													
27.06.2017	180	111.615	180.235	180.961	558.046	5.611	995.989	3.667	29.51	31.65	1.00	37548	6.6924	0.895	559.050	100.0439	0.044	56.1054	99.9998	-0.004	9.461	0.087																													
27.06.2017	180	111.757	180.064	180.791	589.848	5.612	995.980	3.667	29.54	31.52	1.00	37564	6.6930	0.905	559.283	100.0533	0.053	56.1311	100.0124	0.012	9.540	0.089																													
27.06.2017	180	111.633	180.100	180.828	584.743	5.607	995.972	3.661	29.57	31.64	1.00	37528	6.6927	0.900	559.740	100.0476	0.048	56.0730	99.9995	-0.001	9.566	0.086																													
27.06.2017	180	111.777	180.013	180.743	589.248	5.612	995.963	3.680	29.60	31.78	1.00	37563	6.6935	0.911	559.951	100.0584	0.058	56.1262	100.0128	0.013	9.596	0.087																													
27.06.2017	200	99.977	201.425	202.222	593.853	5.616	996.037	4.453	29.28	31.63	1.00	37598	6.6948	0.932	559.564	100.0319	0.032	56.1328	99.9517	-0.048	9.276	0.067																													
27.06.2017	200	100.054	201.960	202.159	599.780	5.622	996.049	4.471	29.30	31.64	1.00	37641	6.6953	0.940	560.198	100.0397	0.040	56.1932	99.9560	-0.044	9.305	0.066																													
27.06.2017	200	100.054	201.960	202.290	599.960	5.622	996.042	4.479	29.33	31.67	1.00	37643	6.6954	0.941	560.231	100.0420	0.042	56.1932	99.9485	-0.051	9.330	0.076																													
27.06.2017	200	99.991	201.424	202.227	591.250	5.614	996.031	4.458	29.37	31.68	1.00	37586	6.6956	0.944	559.352	100.0406	0.041	56.1023	99.9412	-0.059	9.366	0.076																													
27.06.2017	200	99.914	201.473	202.278	591.650	5.614	996.019	4.456	29.41	31.69	1.00	37589	6.6956	0.944	559.376	100.0377	0.038	56.1188	99.9623	-0.038	9.406	0.073																													

ITRI Laboratory – Day#3

																				Temperature correction of meter error			
		* Original data set																					
Date	Nominal flowrate V _{nom} [m ³ /h]	Laboratory reference			Fluid			Ambient conditions			Turbine meter			Coriolis_Mass			Coriolis_Vol			Corrected meter error			
		Measur-remnent time [s]	Standard mass flowrate [kg]	Standard volume flowrate [m ³ /h]	V _{ref} [m ³]	Water density [kg/m ³]	Line pressure P _{fluid} [bar]	Water temp. T _{fluid} [°C]	Air temp. T _{air} [°C]	Air pressure P _{air} [bar]	N	K _v [Pulses/Liter]	Meter error e _m [%]	Pulse count N	K _f [Pulses/Liter]	e _m [%]	k _{nominal}	100,000	Pulses/liter	100,000	(T _{fluid} - T _{nom}) [°C]	T _{nom} [°C]	20
		t	m _{ref}	V _{ref}	ρ _{water}	P _{fluid}	T _{fluid}	T _{air}	P _{air}	N	K _v	e _m	N	K _f	e _m	k _{nominal}	100,000	Pulses/liter	100,000	ΔT _{fluid}	T _{nom}	e _{turbine}	e _{coriolis}
29.06.2017	30	668.017	29.761	29.861	996.737	2.749	26.87	31.02	1.00	36906	6.6006	0.415	552470	100.0326	0.033	554103	100.0009	0.001	6.870	6.870	0.414	0.065	
29.06.2017	30	668.563	29.731	29.829	996.725	2.748	26.91	31.04	1.00	36898	6.6008	0.420	552269	100.0224	0.023	553908	99.9917	-0.008	6.913	6.913	0.419	0.056	
29.06.2017	30	668.679	29.722	29.817	996.824	2.746	26.55	31.01	1.00	36890	6.6009	0.423	552364	100.0361	0.036	553858	100.0053	0.005	6.547	6.547	0.419	0.068	
29.06.2017	30	669.078	29.710	29.799	997.004	2.742	26.57	31.04	1.00	36891	6.6611	0.421	552384	100.0388	0.039	553866	100.0066	0.007	5.870	5.870	0.421	0.068	
29.06.2017	30	668.585	29.733	29.820	997.092	2.754	25.53	31.19	1.00	36888	6.6608	0.419	552437	100.0269	0.027	553789	99.9963	-0.004	5.532	5.532	0.416	0.055	
29.06.2017	30	668.581	29.736	29.820	997.153	2.756	25.30	31.14	1.00	36890	6.6611	0.423	552437	100.0388	0.036	553837	100.0038	0.004	5.296	5.296	0.420	0.063	
29.06.2017	30	668.420	29.741	29.825	997.184	2.759	25.17	31.12	1.00	36887	6.6612	0.425	552426	100.0410	0.041	553803	100.0080	0.001	5.175	5.175	0.422	0.068	
29.06.2017	30	668.776	29.727	29.810	997.206	2.757	25.09	31.24	1.00	36886	6.6607	0.418	552415	100.0319	0.032	553779	99.9987	-0.001	5.089	5.089	0.414	0.058	
29.06.2017	30	668.888	29.719	29.807	997.045	2.747	25.71	31.52	1.00	36886	6.6605	0.414	552375	100.0374	0.037	553846	100.0074	0.007	5.715	5.715	0.412	0.066	
29.06.2017	100	199.357	100.356	100.654	997.039	2.527	25.74	31.33	1.00	37217	6.6770	0.663	556087	100.0620	0.062	557540	100.0264	0.026	5.736	5.736	0.659	0.084	
29.06.2017	100	199.094	100.424	100.726	997.002	2.523	25.88	31.18	1.00	37192	6.6766	0.657	555686	100.0547	0.055	557142	100.0160	0.016	5.879	5.879	0.652	0.077	
29.06.2017	100	199.092	100.481	100.785	996.982	2.528	25.95	31.20	1.00	37214	6.6767	0.658	556000	100.0553	0.055	557480	100.0189	0.019	5.953	5.953	0.654	0.078	
29.06.2017	100	199.178	100.407	100.712	996.974	2.523	25.99	31.20	1.00	37205	6.6770	0.664	555823	100.0541	0.054	557319	100.0197	0.020	5.986	5.986	0.659	0.077	
29.06.2017	100	199.200	100.448	100.754	996.966	2.517	26.01	31.04	1.00	37224	6.6769	0.662	556132	100.0574	0.057	557672	100.0301	0.030	6.014	6.014	0.657	0.081	
29.06.2017	100	199.089	100.407	100.713	996.959	2.524	26.04	31.12	1.00	37187	6.6763	0.663	555606	100.0547	0.055	557132	100.0243	0.024	6.042	6.042	0.649	0.078	
29.06.2017	100	199.153	100.396	100.703	996.951	2.516	26.07	31.22	1.00	37196	6.6768	0.661	555710	100.0572	0.057	557222	100.0235	0.024	6.070	6.070	0.656	0.081	
29.06.2017	100	199.217	100.420	100.727	996.944	2.525	26.10	31.28	1.00	37215	6.6765	0.655	555980	100.0500	0.050	557480	100.0133	0.013	6.099	6.099	0.651	0.073	
29.06.2017	100	199.099	100.427	100.735	996.936	2.522	26.13	31.38	1.00	37199	6.6770	0.664	555748	100.0605	0.061	557290	100.0307	0.031	6.129	6.129	0.659	0.084	
29.06.2017	100	199.074	100.443	100.752	996.928	2.519	26.16	31.38	1.00	37199	6.6767	0.659	555738	100.0551	0.055	557265	100.0219	0.022	6.156	6.156	0.655	0.079	
29.06.2017	200	100.354	200.672	201.294	996.910	4.453	26.23	31.26	1.00	37562	6.6940	0.919	559649	100.0452	0.045	560862	99.9521	-0.048	6.227	6.227	0.895	0.069	
29.06.2017	200	100.418	200.670	201.294	996.901	4.463	26.26	31.24	1.00	37589	6.6945	0.928	560068	100.0574	0.057	561328	99.9717	-0.028	6.260	6.260	0.903	0.082	
29.06.2017	200	100.459	200.631	201.257	996.890	4.464	26.30	31.28	1.00	37601	6.6952	0.937	560216	100.0623	0.062	561476	99.9755	-0.025	6.303	6.303	0.913	0.087	
29.06.2017	200	100.357	200.630	201.259	996.878	4.449	26.35	31.28	1.00	37559	6.6944	0.936	559572	100.0493	0.049	560797	99.9552	-0.045	6.348	6.348	0.901	0.074	
29.06.2017	200	100.393	200.716	201.347	996.868	4.458	26.38	31.34	1.00	37592	6.6950	0.934	560055	100.0568	0.057	561250	99.9563	-0.044	6.383	6.383	0.910	0.082	
29.06.2017	200	100.356	200.643	201.278	996.847	4.458	26.40	31.40	1.00	37567	6.6953	0.939	559629	100.0541	0.054	560855	99.9572	-0.043	6.461	6.461	0.914	0.079	
29.06.2017	200	100.376	200.855	201.492	996.837	4.466	26.50	31.38	1.00	37610	6.6945	0.927	560300	100.0487	0.049	561572	99.9587	-0.041	6.498	6.498	0.902	0.074	
29.06.2017	200	100.219	200.788	201.438	996.824	4.448	26.55	31.36	1.00	37541	6.6948	0.932	559294	100.0587	0.059	560491	99.9544	-0.046	6.546	6.546	0.907	0.084	
29.06.2017	200	100.158	200.896	201.538	996.815	4.452	26.58	31.21	1.00	37541	6.6952	0.938	559254	100.0587	0.059	560524	99.9665	-0.034	6.582	6.582	0.913	0.084	
29.06.2017	200	105.540	201.104	201.697	997.060	4.476	25.66	31.54	1.00	39582	6.6940	0.919	589820	100.0425	0.042	591047	99.9559	-0.044	5.655	5.655	0.897	0.065	

NIM Laboratory – Day#1

Date	Nominal flowrate [m³/h]	Measuriment time [s]	Laboratory reference						Fluid				Ambient conditions				Turbine meter				Coriolis_Mass				Coriolis_Vol				Temperature correction of meter error										
			Standard mass flowrate [kg/h]	Standard volume flowrate [m³/h]	Mass [kg]	Volume [m³]	Water density ρ_{fluid} [kg/m³]	Line pressure p_{fluid} [bar]	Water temp. T_{fluid} [°C]	Air temp. T_{air} [°C]	Air pressure p_{air} [bar]	$K_{V,nom}$	Pulse count	K-factor	ev	$K_{m,nom}$	Pulse count	K-factor	e _m	$K_{V,nom}$	Pulse count	K-factor	ev	$K_{m,nom}$	Pulse count	K-factor	e _m	$K_{V,nom}$	Pulse count	K-factor	ev	$\Delta T_{fluid} - T_{nom}$ [°C]	T _{nom}	20	°C	Corrected meter error			
*Original data set																																							
29.08.2017	30	239.113	30.023	30.112	1994.123	2.005	997.020	1.65	26.22	27.10	1.01	13300.81	6.6501	0.258	199409.4	99.9986	-0.001	200043.5	100.0176	0.018	6.220	0.256	0.029	0.031															
29.08.2017	30	239.645	30.032	30.122	1999.177	2.005	997.020	1.65	26.22	27.10	1.01	13334.45	6.6501	0.258	199518.8	99.9943	-0.006	200135.5	100.0134	0.013	6.220	0.263	0.025	0.028															
29.08.2017	30	239.098	30.040	30.129	1995.124	2.001	997.020	1.65	26.22	27.10	1.01	13308.35	6.6506	0.265	199501.0	99.9981	-0.002	200755.4	100.0171	0.017	6.220	0.268	0.028	0.033															
29.08.2017	30	239.881	30.033	30.123	2001.229	2.007	997.020	1.65	26.22	27.10	1.01	13349.82	6.6509	0.270	200119.1	99.9981	-0.002	200755.4	100.0171	0.017	6.220	0.268	0.028	0.033															
29.08.2017	60	119.040	60.208	60.388	1990.870	1.997	997.015	1.60	26.23	27.10	1.01	13298.24	6.6597	0.402	199095.9	100.0045	0.004	199724.8	100.0210	0.021	6.230	0.407	0.037	0.043															
29.08.2017	60	119.869	60.235	60.415	2005.633	2.012	997.015	1.60	26.23	27.10	1.01	13396.64	6.6596	0.401	200568.8	100.0027	0.003	201201.9	100.0190	0.019	6.230	0.405	0.036	0.043															
29.08.2017	60	119.608	60.209	60.390	2000.428	2.006	997.013	1.60	26.24	27.10	1.01	13362.59	6.6599	0.406	200056.1	100.0066	0.007	200687.6	100.0226	0.023	6.240	0.410	0.039	0.038															
29.08.2017	60	119.662	60.206	60.387	2001.229	2.007	997.010	1.60	26.25	27.10	1.01	13366.89	6.6594	0.398	200132.5	100.0048	0.005	200765.2	100.0210	0.021	6.250	0.402	0.038	0.037															
29.08.2017	60	119.104	60.194	60.374	1991.470	1.997	997.010	1.60	26.25	27.10	1.01	13301.80	6.6594	0.398	199155.1	100.0041	0.004	199784.2	100.0200	0.020	6.250	0.403	0.037	0.038															
29.08.2017	100	79.774	100.921	101.226	2236.348	2.243	996.994	1.55	26.30	27.10	1.01	14952.00	6.6658	0.495	223665.1	100.0135	0.014	224366.7	100.0257	0.026	6.300	0.490	0.038	0.033															
29.08.2017	100	79.635	100.909	101.214	2232.194	2.239	996.989	1.55	26.32	27.10	1.01	14923.27	6.6653	0.488	22343.3	100.0107	0.011	223944.9	100.0229	0.023	6.320	0.483	0.035	0.033															
29.08.2017	100	79.541	100.911	101.216	2229.592	2.236	996.984	1.55	26.34	27.10	1.01	14907.31	6.6659	0.497	222977.8	100.0084	0.008	223680.0	100.0207	0.021	6.340	0.492	0.033	0.039															
29.08.2017	100	79.213	100.910	101.216	2220.383	2.227	996.981	1.55	26.35	27.10	1.01	14846.64	6.6653	0.503	222071.8	100.0151	0.015	222771.5	100.0273	0.027	6.350	0.498	0.039	0.043															
29.08.2017	100	79.509	100.842	101.148	2227.190	2.234	996.976	1.55	26.37	27.10	1.01	14891.14	6.6658	0.495	222760.7	100.0187	0.019	223463.0	100.0306	0.031	6.370	0.490	0.043	0.036															
29.08.2017	140	59.381	140.328	140.755	2314.674	2.322	996.971	1.70	26.41	27.10	1.01	15492.15	6.6727	0.599	231498.6	100.0135	0.013	232221.1	100.0218	0.022	6.410	0.564	0.036	0.033															
29.08.2017	140	59.616	140.365	140.792	2324.434	2.332	996.963	1.70	26.44	27.10	1.01	15557.02	6.6725	0.595	232467.6	100.0104	0.010	233194.3	100.0184	0.018	6.440	0.560	0.033	0.033															
29.08.2017	140	59.539	140.294	140.723	2320.280	2.327	996.955	1.70	26.47	27.10	1.01	15529.80	6.6727	0.598	232051.8	100.0103	0.010	232779.8	100.0186	0.019	6.470	0.563	0.033	0.032															
29.08.2017	140	59.682	140.307	140.736	2326.035	2.333	996.950	1.70	26.49	27.10	1.01	15567.11	6.6721	0.590	232624.7	100.0091	0.009	233356.4	100.0177	0.018	6.490	0.554	0.032	0.034															
29.08.2017	140	59.620	140.271	140.701	2323.032	2.330	996.942	1.70	26.52	27.10	1.01	15547.46	6.6723	0.592	232330.4	100.0117	0.012	233062.1	100.0198	0.020	6.520	0.556	0.034	0.035															
29.08.2017	180	44.418	179.901	180.456	2219.683	2.227	996.929	1.90	26.60	27.10	1.01	14869.19	6.6782	0.682	221989.1	100.0094	0.009	222677.4	100.0114	0.011	6.600	0.656	0.035	0.039															
29.08.2017	180	44.515	180.026	180.583	2209.523	2.216	996.915	1.90	26.65	27.10	1.01	14800.44	6.6778	0.676	220972.8	100.0093	0.009	221660.6	100.0111	0.011	6.650	0.650	0.035	0.039															
29.08.2017	180	44.281	179.955	180.518	2213.477	2.220	996.894	1.90	26.79	27.10	1.01	14826.66	6.6774	0.670	221375.5	100.0126	0.013	222072.8	100.0143	0.014	6.740	0.644	0.039	0.036															
29.08.2017	180	44.830	180.008	180.574	2241.604	2.249	996.863	1.90	26.84	27.10	1.01	15015.20	6.6774	0.670	224182.2	100.0097	0.010	224891.9	100.0117	0.012	6.840	0.643	0.036	0.042															
29.08.2017	200	44.754	199.109	199.737	2475.234	2.483	996.857	2.30	26.93	27.10	1.01	16587.17	6.6802	0.711	247553.3	100.0122	0.012	248332.9	100.0147	0.012	6.930	0.685	0.039	0.041															
29.08.2017	200	44.583	199.218	199.850	2467.126	2.475	996.837	2.30	27.00	27.10	1.01	16532.53	6.6799	0.708	246748.7	100.0146	0.015	247529.9	100.0140	0.014	7.000	0.681	0.042	0.039															
29.08.2017	200	44.367	199.195	199.831	2454.914	2.463	996.818	2.30	27.07	27.10	1.01	16449.51	6.6793	0.698	245520.6	100.0119	0.012	246302.1	100.0110	0.011	7.070	0.671	0.039	0.041															
29.08.2017	200	44.654	199.214	199.855	2469.929	2.478	996.793	2.30	27.16	27.10	1.01	16551.24	6.6796	0.703	247026.0	100.0134	0.013	247819.2	100.0128	0.013	7.160	0.675	0.041	0.041															
29.08.2017	200	44.206	199.157	199.801	2445.504	2.453	996.777	2.30	27.22	27.10	1.01	16387.29	6.6794	0.699	244579.8	100.0120	0.012	245369.8	100.0116	0.012	7.220	0.672	0.040	0.041															

NIM Laboratory – Day#2

Date	Nominal flowrate V_{nom} [m³/h]	Measurment time t [s]	Laboratory reference							Fluid							Ambient conditions							Turbine meter					Coriolis_Mass					Coriolis_Vol					Temperature correction of meter error																												
			Standard mass flowrate m^{*}_{ref} [t/h]	Standard volume flowrate V^{*}_{ref} [m³/h]	Mass m_{ref} [kg]	Volume V_{ref} [m³]	Water density ρ_{water} [kg/m³]	Line pressure P_{fluid} [bar]	Temp. T_{fluid} [°C]	Air temp. T_{air} [°C]	Air pressure P_{air} [bar]	$K_{V,nom}$	Pulse count	K-factor K_v [Pulses/Liter]	Meter error e_v [%]	Pulses/Liter	$K_{m,nom}$	Pulse count	K-factor K_m [Pulses/kg]	Meter error e_m [%]	Pulses/kg	$K_{V,nom}$	Pulse count	K-factor K_v [Pulses/liter]	Meter error e_v [%]	Pulses/Liter	$K_{m,nom}$	Pulse count	K-factor K_m [Pulses/kg]	Meter error e_m [%]	Pulses/kg	Pulses/Liter	Corrected meter error	T_{nom}	ΔT_{fluid} [°C]	Turbine meter $e_{T,cor}$ [%]	Coriolis_Mass $e_{m,cor}$ [%]																														
																																						V_{nom}	m^{*}_{ref}	V^{*}_{ref}	m_{ref}	V_{ref}	ρ_{water}	P_{fluid}	T_{fluid}	T_{air}	P_{air}	Pulse count	K-factor K_v [Pulses/Liter]	Meter error e_v [%]	Pulses/Liter	Pulse count	K-factor K_m [Pulses/kg]	Meter error e_m [%]	Pulses/kg	Pulse count	K-factor K_v [Pulses/liter]	Meter error e_v [%]	Pulses/Liter	Pulse count	K-factor K_m [Pulses/kg]	Meter error e_m [%]	Pulses/kg	T_{nom}	ΔT_{fluid}	$e_{T,cor}$	$e_{m,cor}$
30.08.2017	30	239.870	30.132	2001.767	2.008	997.052	2.30	26.21	23.70	1.01	13351.63	6.6593	0.260	2001.484	99.9859	-0.014	200820.5	100.0259	0.026	6.210	0.258	0.016																																													
30.08.2017	30	239.686	30.001	30.090	1997.463	2.003	997.036	2.30	26.27	23.70	1.01	13320.97	6.6492	0.244	1997.169	99.9853	-0.015	200395.0	100.0274	0.027	6.270	0.242	0.016																																												
30.08.2017	30	239.613	29.991	30.080	1996.162	2.002	997.031	2.30	26.29	23.70	1.01	13312.60	6.6493	0.246	1995.748	99.9792	-0.021	200256.8	100.0230	0.023	6.300	0.244	0.010																																												
30.08.2017	30	239.629	29.989	30.078	1996.162	2.002	997.028	2.30	26.30	23.70	1.01	13311.38	6.6487	0.236	1996.609	99.9867	-0.003	200292.9	100.0408	0.041	6.300	0.234	0.027																																												
30.08.2017	30	239.878	29.979	30.069	1997.614	2.004	997.028	2.30	26.30	23.70	1.01	13321.41	6.6488	0.239	1997.357	99.9872	-0.013	200419.8	100.0314	0.031	6.300	0.237	0.018																																												
30.08.2017	60	119.659	60.030	60.209	1995.311	2.001	997.031	2.30	26.29	23.70	1.01	13325.28	6.6585	0.384	1995.416	100.0052	0.005	200222.3	100.0484	0.048	6.290	0.389	0.038																																												
30.08.2017	60	119.972	60.049	60.228	2001.167	2.007	997.031	2.30	26.29	23.70	1.01	13364.43	6.6585	0.384	2001.000	99.9917	-0.008	200782.0	100.0346	0.035	6.290	0.389	0.037																																												
30.08.2017	60	119.660	60.036	60.215	1995.512	2.001	997.028	2.30	26.30	23.70	1.01	13327.29	6.6588	0.389	1995.588	100.0038	0.004	200238.2	100.0461	0.046	6.300	0.393	0.037																																												
30.08.2017	60	119.880	60.020	60.199	1998.665	2.005	997.025	2.30	26.31	23.70	1.01	13348.70	6.6589	0.391	1998.711	100.0023	0.002	200552.8	100.0449	0.045	6.310	0.396	0.035																																												
30.08.2017	100	74.349	99.452	99.751	2053.915	2.060	997.002	2.00	26.35	23.70	1.01	13331.86	6.6657	0.492	2054.115	100.0098	0.010	206105.7	100.0469	0.047	6.340	0.496	0.034																																												
30.08.2017	100	74.882	99.376	99.676	2067.077	2.073	996.993	2.00	26.37	23.70	1.01	13319.92	6.6656	0.492	2067.313	100.0114	0.011	207429.9	100.0477	0.048	6.370	0.487	0.036																																												
30.08.2017	100	74.351	99.415	99.715	2053.214	2.059	996.991	2.00	26.38	23.70	1.01	13326.98	6.6655	0.490	2053.560	100.0169	0.017	206950.5	100.0531	0.053	6.380	0.485	0.041																																												
30.08.2017	100	74.089	99.365	99.665	2044.956	2.051	996.988	2.00	26.39	23.70	1.01	13371.06	6.6651	0.484	2052.223	100.0130	0.013	205214.8	100.0494	0.049	6.390	0.479	0.037																																												
30.08.2017	140	59.820	139.038	139.464	2310.356	2.317	996.950	1.70	26.49	23.70	1.01	15461.16	6.6717	0.581	2282.402	100.0164	0.016	229004.2	100.0459	0.046	6.460	0.545	0.039																																												
30.08.2017	140	59.929	139.040	139.467	2314.610	2.322	996.942	1.70	26.52	23.70	1.01	15489.31	6.6715	0.581	2314.954	100.0149	0.015	23274.1	100.0444	0.044	6.520	0.544	0.037																																												
30.08.2017	140	59.178	138.981	139.408	2284.651	2.292	996.934	1.70	26.55	23.70	1.01	15289.28	6.6717	0.584	2284.932	100.0132	0.013	229262.8	100.0423	0.042	6.550	0.547	0.036																																												
30.08.2017	180	44.693	179.854	180.120	2229.228	2.236	996.913	1.90	26.66	23.70	1.01	14931.73	6.6775	0.671	2229.997	100.0141	0.014	223694.3	100.0363	0.036	6.660	0.645	0.040																																												
30.08.2017	180	44.880	179.660	180.219	2239.738	2.247	996.896	1.90	26.72	23.70	1.01	15002.47	6.6775	0.671	2239.997	100.0116	0.012	224746.9	100.0337	0.034	6.720	0.645	0.037																																												
30.08.2017	180	44.193	179.533	180.094	2203.904	2.211	996.885	1.90	26.76	23.70	1.01	14763.19	6.6778	0.675	2204.281	100.0171	0.017	221166.5	100.0396	0.040	6.760	0.649	0.043																																												
30.08.2017	180	44.381	179.527	180.091	2213.213	2.220	996.869	1.90	26.82	23.70	1.01	14825.21	6.6775	0.671	2213.457	100.0110	0.011	222089.9	100.0331	0.033	6.820	0.645	0.037																																												
30.08.2017	180	44.099	179.479	180.045	2198.549	2.205	996.858	1.90	26.86	23.70	1.01	14727.48	6.6777	0.674	2198.558	100.0141	0.014	220627.8	100.0362	0.036	6.860	0.647	0.040																																												
30.08.2017	200	44.037	199.531	200.162	2440.784	2.448	996.851	2.30	26.95	23.70	1.01	16357.89	6.6808	0.721	2441.167	100.0157	0.016	248933.9	100.0345	0.035	6.950	0.694	0.042																																												
30.08.2017	200	44.241	199.534	200.168	2452.095	2.460	996.835	2.30	27.01	23.70	1.01	16432.73	6.6803	0.713	2452.541	100.0182	0.018	246979.4	100.0371	0.037	7.010	0.686	0.045																																												
30.08.2017	200	44.414	199.429	200.065	2460.404	2.468	996.821	2.30	27.06	23.70	1.01	16488.52	6.6802	0.712	2460.807	100.0164	0.016	246917.0	100.0352	0.035	7.060	0.685	0.044																																												
30.08.2017	200	44.150	199.409	200.048	2445.539	2.453	996.804	2.30	27.12	23.70	1.01	16389.80	6.6805	0.716	2445.914	100.0153	0.015	245421.8	100.0342	0.034	7.120	0.689	0.043																																												
30.08.2017	200	44.028	199.407	200.050	2438.732	2.447	996.785	2.30	27.19	23.70	1.01	16343.74	6.6802	0.711	2439.055	100.0132	0.013	244737.4	100.0317	0.032	7.190	0.684	0.041																																												

NIM Laboratory – Day#3

Date	Nominal flowrate	Data report NIM: Day#3		*Original data set		Laboratory reference						Fluid						Ambient conditions		Turbine meter		Coriolis_Mass		Coriolis_Vol		Temperature correction of meter error																																	
		V _{nom}	t	Standard mass flowrate	Standard volume flowrate	Mass	Volume	Water density	Line pressure	Water temp.	Air temp.	Air pressure	P _{air}	P _{fluid}	P _{line}	T _{fluid}	T _{air}	P _{air}	K _{v, nom}	6.6330	Pulses/Liter	K _{m, nom}	100.0000	Pulses/kg	K _{v, nom}	100.0000	Pulses/Liter	Corrected meter error	ε _{cor}	ε _{uncor}	ε _{total}	T _{nom}	20	°C																									
																																			Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate	Flowrate
31.08.2017	30	239.531	30.150	2000.017	2.006	996.982	2.30	26.47	23.40	1.01	13333.55	6.6526	0.396	200010.3	100.0043	0.004	200677.1	100.0349	0.035	6.470	0.294	0.035	6.470	0.294	0.035	6.470	0.294	0.035	6.470	0.294	0.035	6.470	0.294	0.035	6.470	0.294	0.035	6.470	0.294	0.035	6.470	0.294	0.035	6.470	0.294	0.035	6.470	0.294	0.035	6.470	0.294	0.035							
31.08.2017	30	239.159	30.078	30.168	1998.165	2.004	997.000	2.30	26.37	23.40	1.01	13333.55	6.6520	0.301	199851.4	100.0175	0.017	200515.1	100.0495	0.049	6.370	0.299	0.048	6.370	0.299	0.048	6.370	0.299	0.048	6.370	0.299	0.048	6.370	0.299	0.048	6.370	0.299	0.048	6.370	0.299	0.048	6.370	0.299	0.048	6.370	0.299	0.048	6.370	0.299	0.048	6.370	0.299	0.048						
31.08.2017	30	239.487	30.218	30.308	2010.226	2.016	997.028	2.30	26.30	23.40	1.01	13411.35	6.6517	0.282	201057.3	100.0173	0.017	201723.0	100.0502	0.050	6.300	0.281	0.048	6.300	0.281	0.048	6.300	0.281	0.048	6.300	0.281	0.048	6.300	0.281	0.048	6.300	0.281	0.048	6.300	0.281	0.048	6.300	0.281	0.048	6.300	0.281	0.048	6.300	0.281	0.048	6.300	0.281	0.048						
31.08.2017	30	239.382	30.393	30.483	2020.785	2.027	997.031	2.30	26.29	23.40	1.01	13413.30	6.6522	0.287	202088.0	100.0047	0.005	202758.1	100.0384	0.038	6.290	0.287	0.035	6.290	0.287	0.035	6.290	0.287	0.035	6.290	0.287	0.035	6.290	0.287	0.035	6.290	0.287	0.035	6.290	0.287	0.035	6.290	0.287	0.035	6.290	0.287	0.035	6.290	0.287	0.035	6.290	0.287	0.035						
31.08.2017	30	239.865	30.183	30.273	2014.426	2.018	997.025	2.30	26.31	23.40	1.01	13413.30	6.6520	0.287	201442.2	100.0152	0.015	201853.5	100.0496	0.050	6.310	0.285	0.047	6.310	0.285	0.047	6.310	0.285	0.047	6.310	0.285	0.047	6.310	0.285	0.047	6.310	0.285	0.047	6.310	0.285	0.047	6.310	0.285	0.047	6.310	0.285	0.047	6.310	0.285	0.047	6.310	0.285	0.047	6.310	0.285	0.047			
31.08.2017	30	239.836	30.184	30.275	2014.926	2.017	997.020	2.30	26.33	23.40	1.01	13416.49	6.6519	0.285	201111.6	100.0094	0.009	201782.1	100.0438	0.044	6.330	0.283	0.040	6.330	0.283	0.040	6.330	0.283	0.040	6.330	0.283	0.040	6.330	0.283	0.040	6.330	0.283	0.040	6.330	0.283	0.040	6.330	0.283	0.040	6.330	0.283	0.040	6.330	0.283	0.040	6.330	0.283	0.040	6.330	0.283	0.040			
31.08.2017	30	239.605	30.183	30.273	2008.875	2.015	997.020	2.30	26.33	23.40	1.01	13403.02	6.6520	0.287	200900.4	100.0064	0.006	201571.3	100.0414	0.041	6.330	0.285	0.037	6.330	0.285	0.037	6.330	0.285	0.037	6.330	0.285	0.037	6.330	0.285	0.037	6.330	0.285	0.037	6.330	0.285	0.037	6.330	0.285	0.037	6.330	0.285	0.037	6.330	0.285	0.037	6.330	0.285	0.037	6.330	0.285	0.037			
31.08.2017	30	240.011	30.178	30.268	2011.927	2.018	997.017	2.30	26.34	23.40	1.01	13422.42	6.6515	0.279	201216.6	100.0119	0.012	201889.1	100.0468	0.047	6.340	0.278	0.037	6.340	0.278	0.037	6.340	0.278	0.037	6.340	0.278	0.037	6.340	0.278	0.037	6.340	0.278	0.037	6.340	0.278	0.037	6.340	0.278	0.037	6.340	0.278	0.037	6.340	0.278	0.037	6.340	0.278	0.037	6.340	0.278	0.037			
31.08.2017	30	239.468	30.179	30.269	2007.473	2.013	997.017	2.30	26.34	23.40	1.01	13392.66	6.6515	0.279	200759.1	100.0059	0.006	201429.4	100.0405	0.040	6.340	0.277	0.037	6.340	0.277	0.037	6.340	0.277	0.037	6.340	0.277	0.037	6.340	0.277	0.037	6.340	0.277	0.037	6.340	0.277	0.037	6.340	0.277	0.037	6.340	0.277	0.037	6.340	0.277	0.037	6.340	0.277	0.037	6.340	0.277	0.037			
31.08.2017	100	75.003	100.758	101.062	2099.207	2.106	996.997	1.90	26.35	23.40	1.01	14035.02	6.6658	0.494	209957.1	100.0173	0.017	210649.6	100.0458	0.046	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042	6.350	0.489	0.042
31.08.2017	100	74.620	100.809	101.112	2089.548	2.096	996.997	1.90	26.35	23.40	1.01	13969.82	6.6655	0.490	208970.9	100.0077	0.008	209660.4	100.0363	0.036	6.350	0.485	0.032	6.350	0.485	0.032	6.350	0.485	0.032	6.350	0.485	0.032	6.350	0.485	0.032	6.350	0.485	0.032	6.350	0.485	0.032	6.350	0.485	0.032	6.350	0.485	0.032	6.350	0.485	0.032	6.350	0.485	0.032	6.350	0.485	0.032			
31.08.2017	100	74.225	100.788	101.092	2078.038	2.084	996.991	1.90	26.37	23.40	1.01	13894.44	6.6662	0.501	207837.0	100.0160	0.016	208522.7	100.0441	0.044	6.370	0.496	0.040	6.370	0.496	0.040	6.370	0.496	0.040	6.370	0.496	0.040	6.370	0.496	0.040	6.370	0.496	0.040	6.370	0.496	0.040	6.370	0.496	0.040	6.370	0.496	0.040	6.370	0.496	0.040	6.370	0.496	0.040	6.370	0.496	0.040			
31.08.2017	100	74.606	100.773	101.078	2088.387	2.095	996.989	1.90	26.38	23.40	1.01	13963.12	6.6659	0.496	208874.9	100.0169	0.017	209565.1	100.0452	0.045	6.380	0.491	0.041	6.380	0.491	0.041	6.380	0.491	0.041	6.380	0.491	0.041	6.380	0.491	0.041	6.380	0.491	0.041	6.380	0.491	0.041	6.380	0.491	0.041	6.380	0.491	0.041	6.380	0.491	0.041	6.380	0.491	0.041	6.380	0.491	0.041			
31.08.2017	100	74.323	100.712	101.017	2079.239	2.086	996.983	1.90	26.40	23.40	1.01	13901.77	6.6658	0.495	207961.3	100.0180	0.018	208650.1	100.0465	0.047	6.400	0.490	0.042	6.400	0.490	0.042	6.400	0.490	0.042	6.400	0.490	0.042	6.400	0.490	0.042	6.400	0.490	0.042	6.400	0.490	0.042	6.400	0.490	0.042	6.400	0.490	0.042	6.400	0.490	0.042	6.400	0.490	0.042	6.400	0.490	0.042			
31.08.2017	100	74.574	100.763	101.068	2087.296	2.094	996.980	1.90	26.41	23.40	1.01	13954.99	6.6655	0.490	208748.8	100.0092	0.009	209440.4	100.0376	0.038	6.410	0.485	0.034	6.410	0.485	0.034	6.410	0.485	0.034	6.410	0.485	0.034	6.410	0.485	0.034	6.410	0.485	0.034	6.410	0.485	0.034	6.410	0.485	0.034	6.410	0.485	0.034	6.410	0.485	0.034	6.410	0.485	0.034	6.410	0.485	0.034			
31.08.2017	100	74.838	100.667	100.973	2092.701	2.099	996.975	1.90	26.43	23.40	1.01	13948.11	6.6660	0.498	209317.5	100.0210	0.021	210011.7	100.0500	0.050	6.430	0.493	0.047	6.430	0.493	0.047	6.430	0.493	0.047	6.430	0.493	0.047	6.430	0.493	0.047	6.430	0.493	0.047	6.430	0.493	0.047	6.430	0.493	0.047	6.430	0.493	0.047	6.430	0.493	0.047	6.430	0.493	0.047	6.430	0.493	0.047			
31.08.2017	100	74.650	100.622	100.928	2092.651	2.099	996.967	1.90	26.46	23.40	1.01	13991.65	6.6658	0.495	209300.0	100.0167	0.017	209996.8	100.0453	0.045	6.460	0.490	0.041	6.460	0.490	0.041	6.460	0.490	0.041	6.460	0.490	0.041	6.460	0.490	0.041	6.460	0.490	0.041	6.460	0.490	0.041	6.460	0.490	0.041	6.460	0.490	0.041	6.460	0.490	0.041	6.460	0.490	0.041	6.460	0.490	0.041			
31.08.2017	200	44.396	199.557	200.168	2460.955	2.468	996.950	2.30	26.59	23.40	1.01	16492.84	6.6814	0.729	246152.9</																																												

NMIJ Laboratory – Day#3

Data report NMII: Day#3													*Original data set							Temperature correction of meter error				
Date	Nominal flowrate V _{nom} [m³/h]	Measu-rement time t [s]	Standard mass flowrate m _{ref} [l/h]	Standard volume flowrate V _{ref} [m³/h]	Mass m _{ref} [kg]	Volume V _{ref} [m³]	Laboratory reference					Turbine meter			Coriolis_Mass			Coriolis_Vol			T _{nom} [°C]	Corrected meter error	Coriolis_Mass e _{m,cor} [%]	
							Water density ρ _{fluid} [kg/m³]	Water line pressure p _{fluid} [bar]	Water temp. T _{fluid} [°C]	Air temp. T _{air} [°C]	Air pressure p _{air} [bar]	Pulse count N	K-factor [Pulses/Liter]	Meter error e _v [%]	K-factor K _m [Pulses/kg]	Pulse count N	Meter error e _m [%]	Pulse count N	K-factor K _v [Pulses/Liter]	Meter error e _v [%]				Pulse count N
Ambient conditions																								
07.12.2017	30	434.638	29.929	29.939	3613.461	3.615	999.668	2.36	13.03	16.97	1.02	24055	66548	0.329	361393	100.0130	0.013	361796	100.0913	0.091	-6.972	0.291	-0.015	
07.12.2017	30	436.249	29.811	29.821	3612.554	3.614	999.667	2.36	13.01	17.34	1.02	24051	66554	0.338	361364	100.0301	0.030	361769	100.1092	0.109	-6.993	0.300	0.002	
07.12.2017	30	430.901	30.183	30.193	3612.746	3.614	999.674	2.36	12.99	17.84	1.02	24053	66556	0.341	361385	100.0306	0.031	361790	100.1100	0.110	-7.015	0.303	0.002	
07.12.2017	30	431.291	30.164	30.174	3613.738	3.615	999.669	2.36	13.02	18.45	1.02	24058	66552	0.334	361495	100.0335	0.034	361901	100.1127	0.113	-6.980	0.296	0.005	
07.12.2017	30	431.381	30.147	30.157	3612.428	3.614	999.668	2.36	13.03	18.86	1.02	24058	66559	0.345	361384	100.0391	0.039	361790	100.1182	0.118	-6.972	0.308	0.011	
07.12.2017	30	432.365	30.088	30.099	3613.667	3.615	999.640	2.36	13.25	20.30	1.02	24056	66546	0.325	361503	100.0377	0.038	361900	100.1115	0.112	-6.753	0.288	0.011	
07.12.2017	30	432.353	30.084	30.095	3613.059	3.614	999.636	2.36	13.28	20.19	1.01	24053	66548	0.329	361448	100.0393	0.039	361845	100.1127	0.113	-6.720	0.292	0.012	
07.12.2017	30	432.387	30.079	30.090	3612.753	3.614	999.632	2.36	13.31	19.88	1.01	24052	66551	0.333	361427	100.0420	0.042	361820	100.1139	0.114	-6.691	0.296	0.015	
07.12.2017	30	432.435	30.077	30.088	3612.848	3.614	999.627	2.36	13.34	20.06	1.01	24051	66546	0.326	361419	100.0371	0.037	361812	100.1086	0.109	-6.656	0.289	0.011	
07.12.2017	30	432.465	30.070	30.082	3612.343	3.614	999.623	2.36	13.38	20.07	1.01	24050	66552	0.335	361375	100.0389	0.039	361768	100.1100	0.110	-6.622	0.299	0.013	
07.12.2017	100	130.513	100.132	100.173	3630.157	3.632	999.598	1.97	13.42	19.93	1.01	24208	66659	0.496	363267	100.0692	0.069	363644	100.1329	0.133	-6.578	0.485	0.034	
07.12.2017	100	130.477	100.209	100.251	3631.957	3.633	999.586	1.97	13.51	20.11	1.01	24221	66661	0.499	363454	100.0711	0.071	363833	100.1340	0.134	-6.487	0.488	0.037	
07.12.2017	100	130.484	100.182	100.224	3631.155	3.633	999.579	1.97	13.57	20.20	1.01	24216	66661	0.500	363368	100.0695	0.070	363751	100.1328	0.133	-6.430	0.489	0.035	
07.12.2017	100	130.495	100.185	100.227	3631.553	3.633	999.573	1.97	13.61	20.07	1.01	24222	66670	0.513	363442	100.0789	0.079	363824	100.1414	0.141	-6.389	0.502	0.045	
07.12.2017	100	130.335	100.233	100.276	3628.849	3.630	999.570	1.97	13.64	20.00	1.01	24199	66656	0.492	363117	100.0640	0.064	363499	100.1261	0.126	-6.364	0.481	0.030	
07.12.2017	100	130.404	100.240	100.284	3631.050	3.633	999.566	1.97	13.66	20.29	1.01	24215	66660	0.497	363336	100.0636	0.064	363719	100.1256	0.126	-6.336	0.487	0.030	
07.12.2017	100	130.468	100.224	100.268	3632.249	3.634	999.565	1.97	13.67	20.12	1.01	24227	66671	0.514	363535	100.0854	0.085	363918	100.1472	0.147	-6.325	0.503	0.052	
07.12.2017	100	130.376	100.234	100.278	3630.046	3.632	999.561	1.97	13.70	19.98	1.01	24211	66667	0.508	363291	100.0789	0.079	363674	100.1404	0.140	-6.300	0.497	0.045	
07.12.2017	100	130.383	100.235	100.279	3630.245	3.632	999.560	1.97	13.71	20.20	1.01	24213	66669	0.511	363315	100.0800	0.080	363697	100.1412	0.141	-6.293	0.500	0.047	
07.12.2017	100	130.506	100.223	100.268	3633.247	3.635	999.558	1.97	13.73	20.21	1.01	24232	66666	0.506	363593	100.0738	0.074	363975	100.1347	0.135	-6.273	0.496	0.041	
07.12.2017	200	65.858	200.136	200.237	3661.274	3.663	999.496	0.82	13.78	19.98	1.01	24473	66809	0.722	366438	100.0848	0.085	366770	100.1250	0.125	-6.217	0.747	0.056	
07.12.2017	200	65.805	200.271	200.373	3660.770	3.663	999.492	0.82	13.81	19.89	1.01	24468	66804	0.715	366388	100.0849	0.085	366723	100.1255	0.125	-6.189	0.739	0.056	
07.12.2017	200	65.769	200.242	200.344	3658.270	3.660	999.489	0.82	13.83	20.05	1.01	24452	66806	0.718	366137	100.0847	0.085	366473	100.1254	0.125	-6.168	0.742	0.056	
07.12.2017	200	65.853	200.197	200.299	3662.074	3.664	999.487	0.82	13.85	20.30	1.01	24479	66810	0.724	366536	100.0897	0.090	366870	100.1295	0.130	-6.154	0.748	0.061	
07.12.2017	200	65.878	200.207	200.311	3663.674	3.666	999.485	0.82	13.86	20.50	1.01	24490	66811	0.725	366714	100.0946	0.095	367048	100.1342	0.134	-6.139	0.749	0.066	
07.12.2017	200	65.887	200.235	200.339	3664.674	3.667	999.482	0.81	13.88	20.54	1.01	24496	66809	0.722	366798	100.0902	0.095	367134	100.1300	0.130	-6.120	0.746	0.062	
07.12.2017	200	65.910	200.264	200.368	3666.475	3.668	999.480	0.81	13.89	20.30	1.01	24508	66809	0.722	366966	100.0869	0.087	367302	100.1264	0.126	-6.106	0.746	0.058	
07.12.2017	200	65.716	200.245	200.350	3655.364	3.657	999.479	0.82	13.91	20.03	1.01	24432	66804	0.714	366585	100.0817	0.082	366169	100.1208	0.121	-6.093	0.738	0.053	
07.12.2017	200	65.801	200.260	200.365	3660.370	3.662	999.476	0.81	13.92	19.89	1.01	24466	66805	0.716	366364	100.0893	0.089	366698	100.1281	0.128	-6.076	0.740	0.061	
07.12.2017	200	65.936	200.242	200.347	3666.977	3.669	999.475	0.81	13.93	19.79	1.01	24511	66807	0.720	367019	100.0876	0.088	367354	100.1264	0.126	-6.067	0.743	0.059	

KRISS Laboratory – Day#1

Data report KRISS: Day#1										*Original data set																
Date	Nominal flowrate V_{nom} [m ³ /h]	Measurment time t [s]	Laboratory reference						Ambient conditions		Turbine meter			Coriolis_Mass			Coriolis_Vol			Temperature correction of meter error						
			Standard mass flowrate V_{ref}^* [m ³ /h]	Standard volume flowrate V_{ref} [m ³ /h]	Mass m _{ref} [kg]	Volume V _{ref} [m ³]	Water density ρ_{fluid} [kg/m ³]	Line pressure p_{fluid} [bar]	Water temp. T _{fluid} [°C]	Air temp. T _{air} [°C]	Air pressure p _{air} [bar]	Pulse count N	K-factor K _v [Pulses/Liter]	Meter error e _v [%]	Pulse count N	K-factor K _m [Pulses/kg]	Meter error e _m [%]	Pulse count N	K-factor K _v [Pulses/Liter]	Meter error e _v [%]	Pulse count N	K-factor K _v [Pulses/Liter]	Meter error e _v [%]	$(T_{fluid} - T_{nom})$ [°C]	Turbine meter e _{v,cor} [%]	Coriolis_Mass e _{m,cor} [%]
24.01.2018	30	243.371	29.955	29.960	2025.018	2.025	999.818	2.04	10.95	18.70	1.02	13475	6.6530	0.302	202688	100.0919	0.092						-9.050	0.255	0.051	
24.01.2018	30	243.552	29.960	29.966	2026.921	2.027	999.817	2.04	10.96	18.70	1.02	13489	6.6537	0.312	202819	100.0626	0.063						-9.040	0.265	0.022	
24.01.2018	30	243.293	29.966	29.971	2025.119	2.026	999.812	2.04	11.01	18.60	1.02	13477	6.6537	0.312	202668	100.0771	0.077						-8.990	0.265	0.037	
24.01.2018	30	243.555	29.922	29.927	2024.318	2.025	999.808	2.04	11.05	18.60	1.02	13471	6.6533	0.306	202554	100.0604	0.060						-8.950	0.260	0.020	
24.01.2018	30	243.712	29.933	29.939	2026.421	2.027	999.805	2.04	11.08	18.60	1.02	13486	6.6538	0.313	202778	100.0671	0.067						-8.920	0.267	0.027	
24.01.2018	60	121.687	60.542	60.554	2046.442	2.047	999.795	2.04	11.17	18.60	1.02	13627	6.6575	0.370	204775	100.0639	0.064						-8.830	0.350	0.003	
24.01.2018	60	122.071	60.272	60.284	2043.739	2.044	999.794	2.04	11.18	18.60	1.02	13614	6.6599	0.406	204524	100.0735	0.073						-8.820	0.386	0.013	
24.01.2018	60	122.571	60.194	60.206	2049.445	2.050	999.794	2.04	11.18	18.60	1.02	13649	6.6585	0.384	205041	100.0471	0.047						-8.820	0.364	-0.013	
24.01.2018	60	122.693	60.146	60.158	2049.845	2.050	999.793	2.04	11.19	18.60	1.02	13651	6.6581	0.379	205060	100.0368	0.037						-8.810	0.359	-0.023	
24.01.2018	60	122.594	60.188	60.201	2049.645	2.050	999.793	2.04	11.19	18.60	1.02	13654	6.6603	0.411	205113	100.0724	0.072						-8.810	0.391	0.012	
24.01.2018	100	74.191	100.817	100.838	2077.674	2.078	999.791	2.04	11.21	18.60	1.02	13845	6.6623	0.442	207763	99.9979	-0.002						-8.790	0.426	-0.051	
24.01.2018	100	74.148	100.665	100.686	2073.370	2.074	999.790	2.04	11.22	18.60	1.02	13818	6.6631	0.454	207339	100.0010	0.001						-8.780	0.438	-0.048	
24.01.2018	100	75.992	100.794	100.815	2071.668	2.072	999.791	2.04	11.21	18.60	1.02	13810	6.6647	0.478	207244	100.0373	0.037						-8.790	0.462	-0.012	
24.01.2018	100	74.072	100.870	100.891	2075.472	2.076	999.791	2.04	11.21	18.60	1.02	13836	6.6650	0.483	207616	100.0331	0.033						-8.790	0.467	-0.016	
24.01.2018	100	74.134	100.801	100.822	2075.773	2.076	999.790	2.04	11.22	18.60	1.02	13836	6.6641	0.468	207645	100.0326	0.033						-8.780	0.462	-0.017	
24.01.2018	140	79.191	140.631	140.661	3093.538	3.094	999.790	2.04	11.22	18.60	1.02	20635	6.6690	0.542	309413	100.0191	0.019						-8.780	0.562	-0.029	
24.01.2018	140	79.299	140.836	140.866	3102.247	3.103	999.788	2.04	11.24	18.60	1.02	20695	6.6696	0.551	310301	100.0246	0.025						-8.760	0.571	-0.023	
24.01.2018	140	79.450	140.799	140.829	3107.353	3.108	999.787	2.04	11.25	18.60	1.02	20727	6.6689	0.541	310769	100.0109	0.011						-8.750	0.561	-0.037	
24.01.2018	140	79.212	140.816	140.847	3098.443	3.099	999.785	2.04	11.27	18.60	1.02	20668	6.6690	0.543	309899	100.0176	0.018						-8.730	0.563	-0.030	
24.01.2018	180	62.392	180.276	180.309	3124.372	3.125	999.817	2.83	11.32	18.50	1.02	20860	6.6753	0.638	312521	100.0268	0.027						-8.680	0.673	-0.015	
24.01.2018	180	62.473	180.399	180.432	3130.578	3.131	999.816	2.83	11.33	18.50	1.02	20902	6.6755	0.641	313140	100.0263	0.026						-8.670	0.676	-0.015	
24.01.2018	180	62.451	180.162	180.195	3125.373	3.126	999.816	2.83	11.33	18.50	1.02	20866	6.6751	0.635	312579	100.0133	0.013						-8.670	0.670	-0.028	
24.01.2018	180	62.410	180.078	180.111	3121.869	3.122	999.816	2.83	11.33	18.50	1.02	20845	6.6759	0.646	312285	100.0314	0.031						-8.670	0.681	-0.010	
24.01.2018	180	62.631	180.393	180.427	3138.387	3.139	999.815	2.83	11.34	18.50	1.02	20953	6.6751	0.635	313912	100.0234	0.023						-8.660	0.670	-0.018	
24.01.2018	200	74.869	199.908	199.948	4157.454	4.158	999.799	2.64	11.40	18.50	1.02	27771	6.6785	0.686	415932	100.0449	0.045						-8.600	0.720	0.004	
24.01.2018	200	74.633	199.834	199.874	4142.839	4.144	999.800	2.64	11.39	18.50	1.02	27669	6.6774	0.670	414426	100.0343	0.034						-8.610	0.705	-0.007	
24.01.2018	200	74.695	199.693	199.734	4143.339	4.144	999.799	2.64	11.40	18.50	1.02	27674	6.6778	0.676	414461	100.0307	0.031						-8.600	0.710	-0.011	
24.01.2018	200	74.835	199.661	199.701	4150.447	4.151	999.800	2.64	11.39	18.50	1.02	27727	6.6792	0.696	415205	100.0386	0.039						-8.610	0.731	-0.003	
24.01.2018	200	74.815	199.482	199.522	4145.642	4.146	999.800	2.64	11.39	18.50	1.02	27695	6.6792	0.696	414738	100.0419	0.042						-8.610	0.731	0.001	

KRISS Laboratory – Day#2

Date	Nominal flowrate V _{nom} [m ³ /h]	Laboratory reference										Turbine meter		Coriolis_Mass		Coriolis_Vol		Temperature correction of meter error					
		Measur-rement time t [s]	Standard mass flowrate m ^{ref} [kg]	Standard volume flowrate V ^{ref} [m ³ /h]	Volume V _{ref} [m ³]	Water density ρ [kg/m ³]	Line pressure p _{fluid} [bar]	Water temp. T _{fluid} [°C]	Air temp. T _{air} [°C]	Air pressure p _{air} [bar]	Ambient conditions	K _{v, nom}	Pulse count N	K-factor [Pulses/Liter]	Meter error e _m [%]	K _{v, nom}	Pulse count N	K-factor [Pulses/Liter]	Meter error e _v [%]	T _{nom} [°C]	Corrected meter error		
02.02.2018	30	242,151	30,087	30,087	2023,782	2,024	998,779	2,04	11,32	23,30	1,00	13470	6,6537	0,313	202489	100,0597	0,060	202655	100,1049	0,105	-8,680	0,267	0,021
02.02.2018	30	242,314	30,110	30,120	2026,685	2,027	998,775	2,04	11,36	23,30	1,00	13491	6,6534	0,325	202788	100,0590	0,059	202941	100,1022	0,102	-8,640	0,280	0,021
02.02.2018	30	241,914	30,127	30,137	2024,483	2,025	998,774	2,04	11,37	23,30	1,00	13477	6,6549	0,330	202570	100,0601	0,060	202720	100,1018	0,102	-8,630	0,284	0,022
02.02.2018	30	241,916	30,131	30,141	2024,783	2,025	998,772	2,04	11,39	23,30	1,00	13476	6,6534	0,307	202585	100,0527	0,053	202735	100,0942	0,094	-8,610	0,262	0,015
02.02.2018	30	242,094	30,127	30,137	2025,484	2,026	998,769	2,04	11,42	23,30	1,00	13483	6,6545	0,324	202683	100,0664	0,066	202833	100,1076	0,108	-8,580	0,279	0,029
02.02.2018	60	122,713	59,953	59,973	2043,603	2,044	998,763	2,04	11,47	23,30	1,00	13614	6,6595	0,400	204485	100,0610	0,061	204631	100,0990	0,099	-8,530	0,381	0,003
02.02.2018	60	122,630	60,005	60,025	2044,003	2,045	998,762	2,04	11,48	23,30	1,00	13618	6,6602	0,410	204536	100,0664	0,066	204683	100,1047	0,105	-8,520	0,391	0,009
02.02.2018	60	122,655	60,072	60,092	2046,706	2,047	998,761	2,04	11,49	23,30	1,00	13634	6,6592	0,395	204762	100,0447	0,045	204909	100,0828	0,083	-8,510	0,376	-0,013
02.02.2018	60	122,453	60,124	60,144	2045,104	2,046	998,761	2,04	11,49	23,30	1,00	13625	6,6600	0,407	204625	100,0560	0,056	204771	100,0937	0,094	-8,510	0,389	-0,002
02.02.2018	60	122,434	60,142	60,163	2045,405	2,046	998,759	2,04	11,51	23,30	1,00	13625	6,6590	0,392	204639	100,0482	0,048	204785	100,0857	0,086	-8,490	0,374	-0,009
02.02.2018	100	75,171	99,581	99,615	2079,340	2,080	998,757	2,04	11,53	23,30	1,00	13864	6,6652	0,486	208011	100,0370	0,037	208153	100,0713	0,071	-8,470	0,471	-0,010
02.02.2018	100	74,950	99,615	99,649	2073,934	2,075	998,758	2,04	11,52	23,30	1,00	13828	6,6653	0,486	207487	100,0451	0,045	207629	100,0796	0,080	-8,480	0,471	-0,002
02.02.2018	100	75,249	99,569	99,603	2081,242	2,082	998,757	2,04	11,53	23,30	1,00	13876	6,6649	0,481	208190	100,0316	0,032	208331	100,0653	0,065	-8,470	0,466	-0,016
02.02.2018	100	74,975	99,515	99,549	2072,533	2,073	998,754	2,04	11,55	23,30	1,00	13819	6,6654	0,488	207337	100,0404	0,040	207479	100,0746	0,075	-8,450	0,473	-0,007
02.02.2018	100	75,115	99,584	99,618	2077,838	2,079	998,753	2,04	11,56	23,30	1,00	13850	6,6653	0,457	207800	100,0078	0,008	207942	100,0417	0,042	-8,440	0,441	-0,039
02.02.2018	140	79,272	140,740	140,789	3099,083	3,100	998,752	2,04	11,57	23,30	1,00	20676	6,6694	0,548	309986	100,0251	0,025	310188	100,0557	0,056	-8,430	0,567	-0,021
02.02.2018	140	79,332	140,765	140,814	3101,986	3,103	998,748	2,04	11,59	23,30	1,00	20692	6,6683	0,531	310205	100,0021	0,002	310407	100,0325	0,032	-8,410	0,551	-0,044
02.02.2018	140	79,312	140,704	140,753	3099,984	3,101	998,748	2,04	11,61	23,30	1,00	20680	6,6689	0,541	310040	100,0167	0,017	310242	100,0469	0,047	-8,390	0,560	-0,029
02.02.2018	140	79,475	140,662	140,711	3105,289	3,106	998,748	2,04	11,61	23,30	1,00	20717	6,6692	0,546	310572	100,0139	0,014	310775	100,0443	0,044	-8,390	0,565	-0,032
02.02.2018	140	79,535	140,614	140,664	3106,591	3,108	998,747	2,04	11,62	23,30	1,00	20723	6,6683	0,532	310687	100,0090	0,009	310893	100,0402	0,040	-8,380	0,552	-0,036
02.02.2018	180	62,774	179,617	179,681	3132,013	3,133	998,777	2,83	11,69	23,90	1,00	20921	6,6773	0,668	313322	100,0385	0,039	313518	100,0653	0,065	-8,310	0,702	-0,001
02.02.2018	180	62,973	179,639	179,704	3142,323	3,143	998,777	2,83	11,69	23,90	1,00	20886	6,6761	0,650	314325	100,0295	0,029	314524	100,0570	0,057	-8,310	0,683	-0,010
02.02.2018	180	62,753	179,465	179,529	3128,309	3,129	998,775	2,83	11,70	23,90	1,00	20888	6,6747	0,629	312850	100,0061	0,006	313047	100,0331	0,033	-8,300	0,662	-0,034
02.02.2018	180	62,950	179,526	179,591	3139,220	3,140	998,773	2,83	11,72	23,90	1,00	20962	6,6750	0,634	313951	100,0092	0,009	314152	100,0371	0,037	-8,280	0,667	-0,030
02.02.2018	180	62,892	179,377	179,442	3133,715	3,135	998,773	2,83	11,72	23,90	1,00	20929	6,6762	0,652	313466	100,0302	0,030	313666	100,0578	0,058	-8,280	0,685	-0,009
02.02.2018	200	74,851	199,249	199,322	4142,750	4,144	998,761	2,64	11,75	23,90	1,00	27682	6,6796	0,703	414407	100,0319	0,032	414655	100,0552	0,055	-8,250	0,736	-0,008
02.02.2018	200	75,074	198,873	198,946	4147,255	4,149	998,759	2,64	11,77	23,90	1,00	27711	6,6793	0,698	414840	100,0276	0,028	415093	100,0519	0,052	-8,230	0,731	-0,012
02.02.2018	200	75,071	198,915	198,988	4145,753	4,147	998,759	2,64	11,77	23,90	1,00	27699	6,6788	0,691	414677	100,0245	0,025	414926	100,0479	0,048	-8,230	0,724	-0,015
02.02.2018	200	75,030	199,095	199,168	4151,659	4,153	998,758	2,64	11,78	23,90	1,00	27742	6,6797	0,704	415305	100,0335	0,033	415554	100,0566	0,057	-8,220	0,737	-0,006
02.02.2018	200	74,893	198,930	199,003	4138,446	4,140	998,758	2,64	11,78	23,90	1,00	27655	6,6800	0,709	414025	100,0436	0,044	414265	100,0648	0,065	-8,220	0,742	0,004

KRISS Laboratory – Day#3

Data report KRISS: Day#3												*Original data set			Temperature correction of meter error																								
Date	Nominal flowrate	V _{nom}	Measurment time t	Standard mass flowrate	Standard volume flowrate	Laboratory reference			Fluid			Ambient conditions			Turbine meter			Coriolis_Mass			Coriolis_Vol																		
						m _{ref}	V _{ref}	V _{ref}	ρ _{fluid}	Water density	Line pressure	Water temp.	Water temp.	Air temp.	Air pressure	K _{v,nom}	6,633	Pulses/Liter	K _{v,nom}	100,000	Pulses/kg	K _{v,nom}	100,000	Pulses/Liter	K _{v,nom}	100,000	Pulses/Liter												
		[m ³ /h]	[s]	[kg]	[m ³ /h]	[kg/m ³]	[bar]	[°C]	[°C]	[bar]	[°C]	[°C]	[bar]	[m ³ /h]	[kg]	[m ³ /h]	[m ³ /h]	[Pulses]	[Pulses/Liter]	[Pulses]	[Pulses]	[Pulses/Liter]	[Pulses]	[Pulses/Liter]	[Pulses]	[Pulses/Liter]	[Pulses]	[Pulses/Liter]	[Pulses]	[Pulses/Liter]	[Pulses]	[Pulses/Liter]							
30.01.2018	30	242,556	30,088	2,027	2,027	999,865	2,04	10,47	21,30	1,00	13,495	6,6561	0,348	202,872	100,0750	0,075																							
30.01.2018	30	242,175	30,098	2,025	2,025	999,863	2,04	10,49	21,30	1,00	13,477	6,6554	0,338	202,616	100,0722	0,072																							
30.01.2018	30	242,177	30,108	2,025	2,025	999,861	2,04	10,52	21,30	1,00	13,481	6,6550	0,332	202,669	100,0638	0,064																							
30.01.2018	30	241,933	30,104	2,023	2,023	999,859	2,04	10,54	21,30	1,00	13,466	6,6552	0,335	202,452	100,0704	0,070																							
30.01.2018	30	243,052	30,090	2,032	2,032	999,856	2,04	10,57	21,30	1,00	13,520	6,6542	0,320	203,275	100,0613	0,061																							
30.01.2018	30	242,491	30,099	2,028	2,028	999,854	2,04	10,59	21,30	1,00	13,493	6,6543	0,322	202,840	100,0493	0,049																							
30.01.2018	30	242,356	30,109	2,027	2,027	999,851	2,04	10,62	21,30	1,00	13,491	6,6547	0,326	202,814	100,0562	0,056																							
30.01.2018	30	242,115	30,107	2,024	2,024	999,849	2,04	10,64	21,30	1,00	13,475	6,6540	0,316	202,578	100,0485	0,049																							
30.01.2018	30	242,194	30,109	2,026	2,026	999,846	2,04	10,67	21,30	1,00	13,479	6,6533	0,306	202,656	100,0475	0,047																							
30.01.2018	30	242,096	30,099	2,024	2,024	999,844	2,04	10,69	21,30	1,00	13,473	6,6533	0,336	202,545	100,0668	0,067																							
30.01.2018	100	74,433	100,319	2,074	2,074	999,842	2,04	10,71	18,90	1,00	13,827	6,6532	0,486	207,504	100,0420	0,042																							
30.01.2018	100	74,331	100,302	2,071	2,071	999,842	2,04	10,71	18,90	1,00	13,805	6,6649	0,481	207,161	100,0311	0,031																							
30.01.2018	100	74,232	100,425	2,071	2,071	999,840	2,04	10,73	18,90	1,00	13,798	6,6622	0,440	207,069	99,9963	-0,004																							
30.01.2018	100	74,653	100,265	2,080	2,080	999,839	2,04	10,74	18,90	1,00	13,855	6,6626	0,447	207,929	100,0055	0,006																							
30.01.2018	100	74,537	100,197	2,075	2,075	999,839	2,04	10,74	18,90	1,00	13,830	6,6654	0,488	207,543	100,0414	0,041																							
30.01.2018	100	74,492	100,312	2,076	2,076	999,838	2,04	10,75	19,20	1,00	13,836	6,6647	0,478	207,635	100,0328	0,033																							
30.01.2018	100	74,691	100,300	2,081	2,081	999,838	2,04	10,75	19,20	1,00	13,871	6,6645	0,476	208,157	100,0286	0,029																							
30.01.2018	100	74,531	100,302	2,077	2,077	999,837	2,04	10,76	19,20	1,00	13,842	6,6647	0,478	207,713	100,0270	0,027																							
30.01.2018	100	74,676	100,282	2,081	2,081	999,836	2,04	10,77	19,20	1,00	13,865	6,6642	0,471	208,041	100,0114	0,011																							
30.01.2018	100	74,392	100,204	2,070	2,070	999,834	2,04	10,79	19,20	1,00	13,800	6,6634	0,459	207,095	100,0139	0,014																							
30.01.2018	200	74,389	200,329	4,140	4,140	999,874	2,89	10,80	18,50	1,00	27,656	6,6801	0,710	414,111	100,0381	0,038																							
30.01.2018	200	74,395	200,391	4,142	4,142	999,865	2,89	10,88	18,50	1,00	27,666	6,6799	0,707	414,250	100,0329	0,033																							
30.01.2018	200	74,735	200,410	4,161	4,161	999,866	2,89	10,87	18,50	1,00	27,792	6,6791	0,696	416,146	100,0241	0,024																							
30.01.2018	200	74,935	200,034	4,164	4,164	999,865	2,89	10,88	18,50	1,00	27,814	6,6791	0,695	416,469	100,0223	0,022																							
30.01.2018	200	74,436	200,116	4,138	4,138	999,864	2,89	10,89	18,50	1,00	27,642	6,6796	0,702	413,903	100,0313	0,031																							
30.01.2018	200	74,415	200,096	4,135	4,135	999,863	2,89	10,90	18,50	1,00	27,625	6,6800	0,708	413,649	100,0377	0,038																							
30.01.2018	200	74,631	200,008	4,147	4,147	999,862	2,89	10,91	18,50	1,00	27,699	6,6794	0,700	414,735	100,0243	0,024																							
30.01.2018	200	74,634	199,904	4,145	4,145	999,862	2,89	10,91	18,50	1,00	27,686	6,6795	0,701	414,571	100,0331	0,033																							
30.01.2018	200	74,835	199,797	4,154	4,154	999,860	2,89	10,93	18,50	1,00	27,746	6,6796	0,703	415,457	100,0318	0,032																							
30.01.2018	200	74,436	199,972	4,135	4,135	999,859	2,89	10,94	18,50	1,00	27,620	6,6791	0,694	413,572	100,0239	0,024																							

10.3 Additional documents

Declaration of NEL



Report from TÜV SÜD National Engineering Laboratory regarding Key Comparison CCM.FF-K1.2015

TÜV SÜD National Engineering Laboratory
East Kilbride
Glasgow
G75 0QF

27/02/2020

In 2015, TÜV SÜD National Engineering Laboratory (NEL) participated in the key comparison CCM.FF-K1.2015 for water flow which was led by Physikalisch-Technische Bundesanstalt (PTB). This comparison followed on from EURAMET Project No. E 1201 between PTB and NEL and was completed in 2011 over comparable conditions with similar test meters. The results from EURAMET Project No. E 1201 were satisfactory and provided verification of NEL's water flow facility Calibration and Measurement Capability (CMC) value of 0.10 % ($k=2$).

Unfortunately, due to unexpected technical problems with the data collection system during the CCM.FF-K1.2015 key comparison, the results were deemed to be unacceptable. Whilst the test data recorded at NEL by PTB's own logging system indicated acceptable results, regrettably NEL's measurement system did not. As such, NEL have decided to withdraw from key comparison CCM.FF-K1.2015 due to technical issues during the calibrations which have proven impossible to rectify retrospectively. NEL will seek to participate in future water flow comparisons to maintain verification of our CMC.

10.4 Comparison results - based on Reynolds number

Submitted by KRISS (Dr. Sejong Chun) in January 2021

Use of weighted linear regression to investigate the relationship between Re and meter error

For a research purpose, two kinds of linear regressions (linear regression and weighted linear regression) were applied to the data of Draft A report (Appendix 10.2). Input parameter: nominal diameter of pipe, reference flow rate, fluid temperature and density, viscosity, temperature corrected meter error e_{corr} of turbine meter and Coriolis meter. Based on these data set, Reynolds numbers were calculated. A weighted linear regression using MATLAB was applied to the results.

The first step was to use Deming's linear regression, obtained from MATLAB Centrals and NCSS software manual. The parameter λ was so small that the Deming's linear regression was not meaningful. So, λ was defined as the variance of meter error divided by the variance of Reynolds number. The value of λ was in order of 10^{-8} to 10^{-10} in this case.

The Deming's linear regression was changed into normal linear regression by letting λ equal to 1. Instead, the weighting factor was introduced, based on the definition of key comparison reference value and its uncertainty (Section 5.3).

$$w_i = \frac{\frac{1}{u_{\text{CMC},i}^2}}{\left(\frac{1}{u_{\text{CMC},1}^2} + \frac{1}{u_{\text{CMC},2}^2} + \cdots + \frac{1}{u_{\text{CMC},i}^2} + \cdots + \frac{1}{u_{\text{CMC},N}^2} \right)} \quad (1)$$

$u_{\text{CMC},i}$ was the calibration and measurement capability (CMC) of a participating laboratory. w_i was the weighting factor of the participating laboratory. In other words, the weighting factor was the normalized value of a reciprocal of squared CMC's. At first, all the reciprocals of squared CMC's were collected. After that, the reciprocals were normalized by summing to 1.

The uncertainty of the linear regression and the weighted linear regression was calculated as follows:

If $y = ax + b$ is sought, then its standard uncertainty (type B) is $u(\delta y) = au(\delta x)$.

At first, $u(y) = \sqrt{a^2 u^2(x) + x^2 u^2(a) + u^2(b)}$ was assumed. However, there was a problem that $u(y)$ was indefinitely increasing while x was increasing. Instead, the mathematical expression was rearranged as $y = y_0 + a \delta x$, $y_0 = ax_0 + b$, and $\delta x = x - x_0$. After that, $u(y) = \sqrt{u^2(y_0) + a^2 u^2(\delta x)}$ was calculated, followed by definitions of $u(y)$ as the standard uncertainty by meter error (u_A), and $au(\delta x)$ as the standard uncertainty by linear regression or weighted linear regression (u_B). The term of $au(\delta x)$ was set as the standard uncertainty of KCRV (u_{KCRV}).

Finally, the weighted linear regression could be used as KCRV in case that all the measurement data were arranged as a function of Reynolds number. The results of E_N numbers were similar with the original data suggested in the Draft A report as follows.

Turbine flowmeter

Figure 1: Scatter of linear regression and weighted linear regression between Reynolds number and temperature corrected meter error for turbine meter

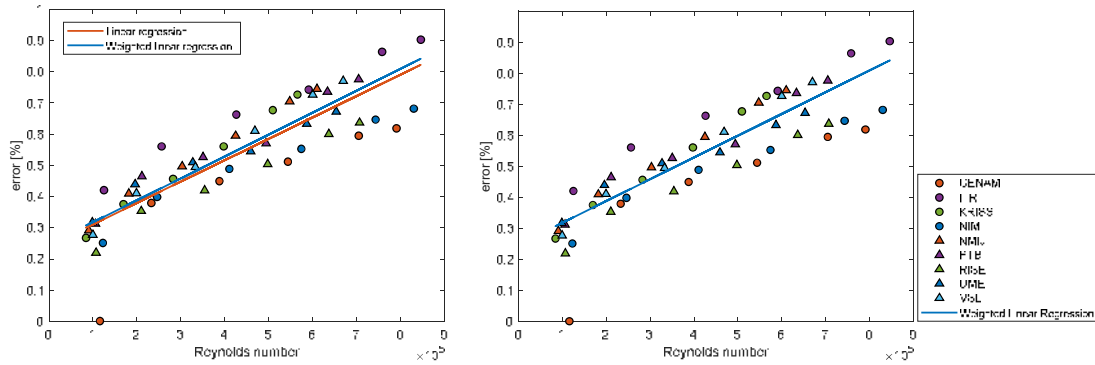


Table 1: Summary of E_N -values of each participating laboratory for turbine meter - based on weighted linear regression between Reynolds number and temperature corrected meter error for Turbine meter

Red color: Non-compliance
 Orange color: Warning level
 Blue color: Inconclusiveness

Nominal flowrate	30 m ³ /h		60 m ³ /h		100 m ³ /h		140 m ³ /h		180 m ³ /h		200 m ³ /h	
	E_N	u_{comp}/u_{CMC}	E_N	u_{comp}/u_{CMC}	E_N	u_{comp}/u_{CMC}	E_N	u_{comp}/u_{CMC}	E_N	u_{comp}/u_{CMC}	E_N	u_{comp}/u_{CMC}
CENAM	-1.29	6.57	-0.15	5.58	-0.34	5.37	-0.58	5.27	-0.74	5.16	-0.91	5.21
ITRI	0.34	6.20	0.61	5.30	0.56	5.10	0.39	5.00	0.42	4.91	0.30	4.95
KRISS	-0.16	4.14	0.04	3.54	0.05	3.41	0.16	3.34	0.35	3.28	0.40	3.30
NIM	-0.33	4.96	-0.10	4.24	-0.23	4.08	-0.48	4.00	-0.61	3.92	-0.73	3.96
NMIJ	-0.08	5.91	0.16	5.05	0.17	4.86	0.24	4.77	0.36	4.67	0.34	4.72
PTB	-0.04	12.41	0.32	10.60	0.16	10.20	-0.06	16.13	0.22	9.80	0.17	9.90
RISE	-0.41	4.13	-0.19	3.53	-0.36	3.40	-0.45	3.33	-0.46	3.27	-0.52	3.30
UME	0.00	3.56	0.24	3.05	0.15	2.93	-0.12	2.87	-0.13	2.85	-0.16	2.83
VSL	-0.16	5.51	0.11	4.71	0.06	4.53	0.17	4.45	0.29	4.36	0.26	4.40

Coriolis Mass flowmeter

Figure 2: Scatter of linear regression and weighted linear regression between Reynolds number and temperature corrected meter error for Coriolis_Mass meter

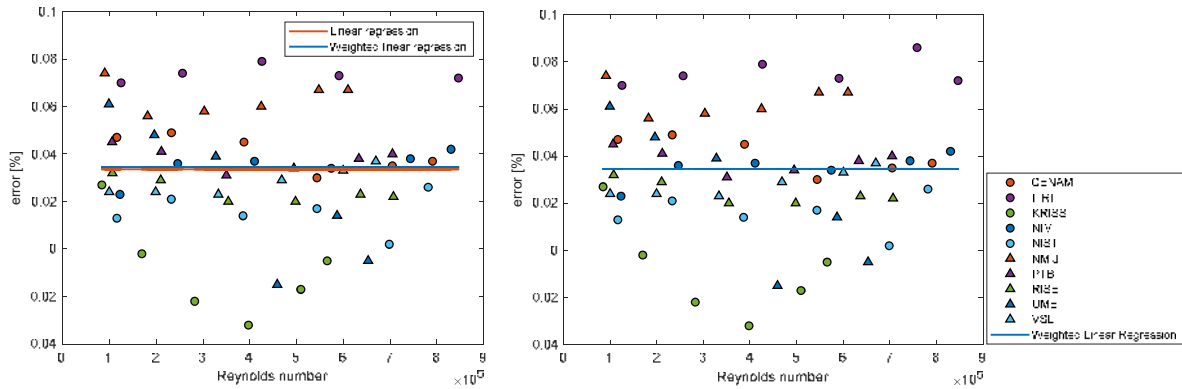


Table 2: Summary of E_N -values of each participating laboratory for Coriolis_Mass meter – based on weighted linear regression between Reynolds number and temperature corrected meter error for Coriolis_Mass meter

Red color: Non-compliance
 Orange color: Warning level
 Blue color: Inconclusiveness

Nominal flowrate	30 t/h		60 t/h		100 t/h		140 t/h		180 t/h		200 t/h	
	E_N	u_{comp}/u_{CMC}	E_N	u_{comp}/u_{CMC}	E_N	u_{comp}/u_{CMC}	E_N	u_{comp}/u_{CMC}	E_N	u_{comp}/u_{CMC}	E_N	u_{comp}/u_{CMC}
CENAM	0.23	1.49	0.37	0.81	0.29	0.68	-0.13	0.60	0.02	0.54	0.08	0.47
ITRI	0.59	1.11	0.85	0.60	0.99	0.51	0.86	0.48	1.16	0.44	0.88	0.37
KRISS	-0.10	0.76	-0.54	0.46	-0.83	0.44	-1.04	0.33	-0.80	0.34	-0.63	0.26
NIM	-0.17	0.89	0.03	0.49	0.05	0.41	-0.01	0.36	0.07	0.32	0.14	0.28
NIST	-0.34	1.69	-0.29	1.01	-0.41	1.03	-0.33	1.12	-0.44	1.65	-0.25	0.50
NMIJ	0.64	1.06	0.44	0.58	0.50	0.49	0.54	0.47	0.72	0.38	0.71	0.37
PTB	0.21	2.22	0.20	1.23	-0.12	1.00	-0.02	0.91	0.13	0.81	0.22	0.71
RISE	-0.03	0.55	-0.07	0.31	-0.18	0.25	-0.18	0.23	-0.14	0.20	-0.15	0.18
UME	0.30	0.72	0.17	0.49	0.06	0.37	-0.65	0.36	-0.28	0.25	-0.54	0.25
VSL	-0.20	1.48	-0.37	1.61	-0.46	1.34	-0.23	1.21	-0.07	1.07	0.12	0.95