

*BIPM Workshop  
on Challenges in Metrology for Dynamic Measurement*

Dynamic measurements of thermophysical  
properties for material metrology standards

Measurement by impulse heating and analysis  
by response functions and transfer functions

*Tetsuya Baba*

National Metrology Institute of Japan (NMIJ),  
National Institute of Advanced Industrial  
Science and Technology (AIST)

# BIPM Workshop on Challenges in Metrology for Dynamic Measurement

- Session 1 Dynamic Mechanical Quantities  
Force, Torque, Vibration, etc
- Session 2 Dynamic Fluid and Flowmetry  
Pressure, temperature, and volume of fluid
- Session 3 Thermo Physical Quantities  
Thermal properties, material properties, etc  
Temperature



Dynamic response of  
sensor, measurement

Frequency response, Step response, **Impulse response**

Mathematical  
presentation



**Impulse response function**  
**Transfer function**

# Outline of the presentation

## 1. Introduction

- Needs for thermophysical quantities
- Common interest with dynamic measurement of mechanical quantities, fluid and flowmetry

## 2. Pulsed light heating methods

- Laser flash method for thermal diffusivity measurements
- Ultra fast laser flash method for thin films measurement

## 3. Analysis by impulse response function and transfer function

- Analysis of heat diffusion
- Analysis of finite response time of temperature detection
- Transfer function and areal heat diffusion time

## 4. Summary

# Needs for thermal metrology 1

- Energy production:
  - Electric power generator
  - Nuclear power plant
  - Natural energy
    - Geothermal power generation
    - Solar power generation

## Needs for thermal metrology 2

- Energy saving:
  - Industrial sector
    - Production line
    - Plants
    - Furnaces, kilns, heat treatment
    - Steel making, ceramics industry
  - Transportation sector
    - Automobiles
    - Trains, ships, aircrafts
  - Commercial and residential sector
    - Buildings and houses

## Needs for thermal metrology 3

- Electronics:
  - Thermal design and management
    - PC, server, data center, projector
    - Home electric appliance
    - LED illumination
    - Flat panel display
  - Device
    - CPU
    - Memory and storage
      - Phase change memory
      - Hard disk (Heat assisted)
      - Organic EL

# CMC service categories covered by WG9

## 6. Thermophysical properties

### 6.1 Thermal transport property

#### 6.1.1 Thermal conductivity

#### 6.1.2 Thermal diffusivity

### 6.2 Caloric property

#### 6.2.1 Specific heat capacity

#### 6.2.2 Heat of fusion

#### 6.2.3 Calorific value

### 6.3 Radiative property

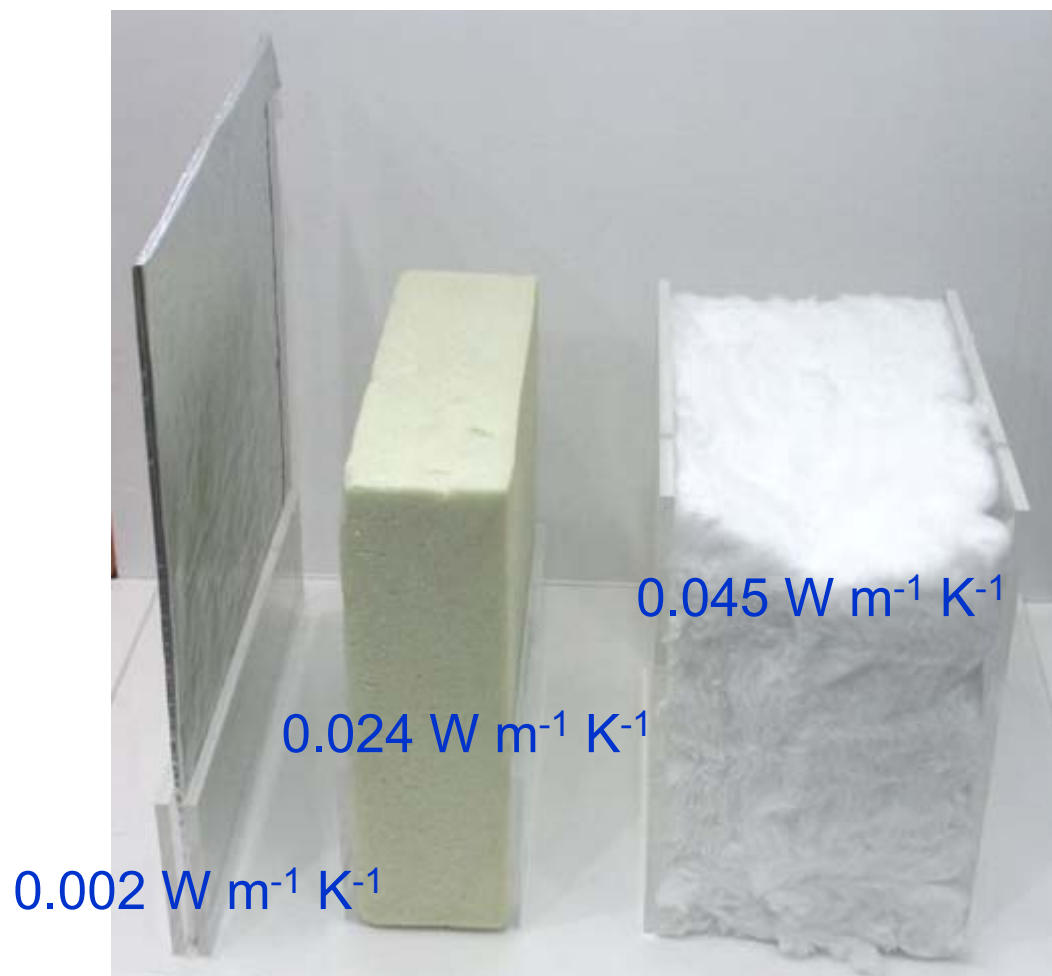
#### 6.3.1 Spectral emissivity

#### 6.3.2 Total emissivity

### 6.4 Thermo-mechanical property

#### 6.4.1 Thermal expansion coefficient

# Vacuum insulation panel (VIP)



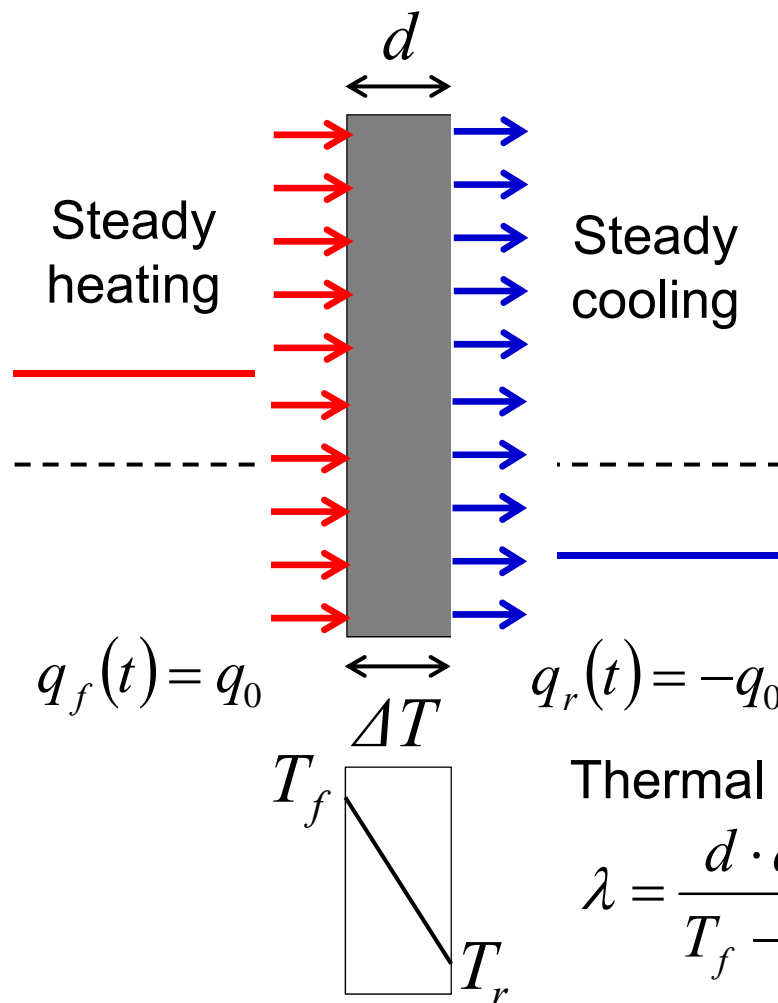
VIP   Urethane foam   Glass wool





# Measurement of thermal conductivity

Thermal conductivity,  $\lambda$ ,  
measurement by steady method



Thermal conductivity

$$\lambda = \frac{d \cdot q_0}{T_f - T_r} = \frac{d \cdot q_0}{\Delta T_{fr}}$$



## Three pilot studies organized by CCT WG9

### CCT-P01 (CCT-S2)

Thermal conductivity of insulating materials

Temperature range	0 - 100 ° C
Measurement technique	guarded hot plate method
Pilot institute	LNE, France

### CCT-S2

#### Information

Metrology area, branch	Thermometry, Thermophysical quantities
Description	Thermal conductivity
Time of measurement	2007 - 2010
Status	Report in progress, Draft A
Reference(s)	No references available
Measurand	Thermal conductivity: 0.01 Wm <sup>-1</sup> K <sup>-1</sup> to 0.1 Wm <sup>-1</sup> K <sup>-1</sup>
Parameter(s)	Temperature: 10 °C, 23 °C and 40 °C
Transfer device(s)	Two thermal insulating materials
Comparison type	Supplementary comparison
Consultative Committee	CCT (Consultative Committee for Thermometry)
Conducted by	CCT (Consultative Committee for Thermometry)

# Ceramics and compound semiconductors

AlN



SiC



$\text{Si}_3\text{N}_4$

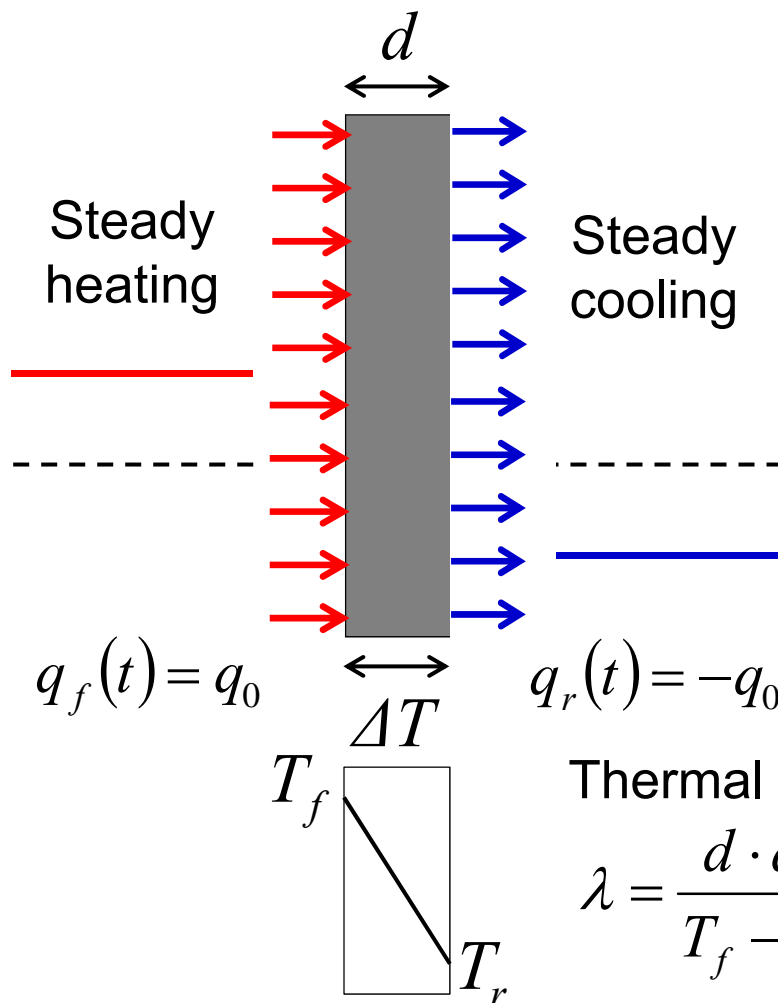


GaN



# Measurement of thermal conductivity and thermal diffusivity

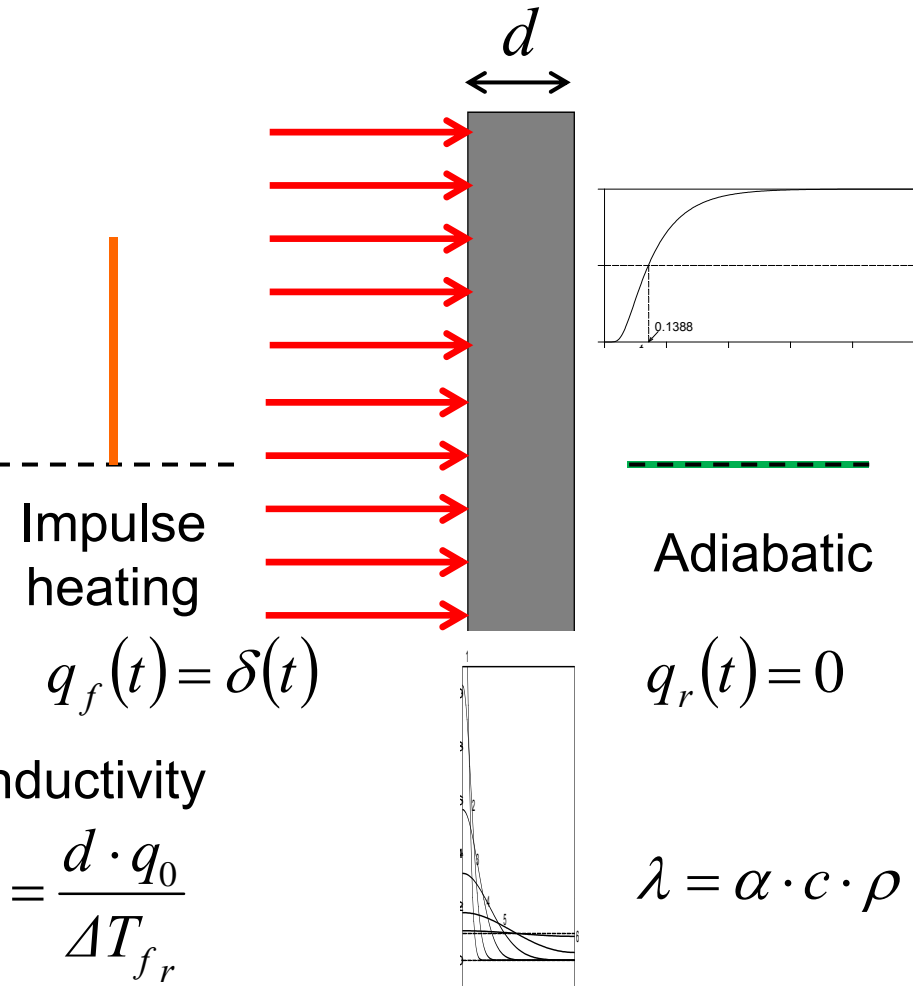
Thermal conductivity,  $\lambda$ ,  
measurement by steady method



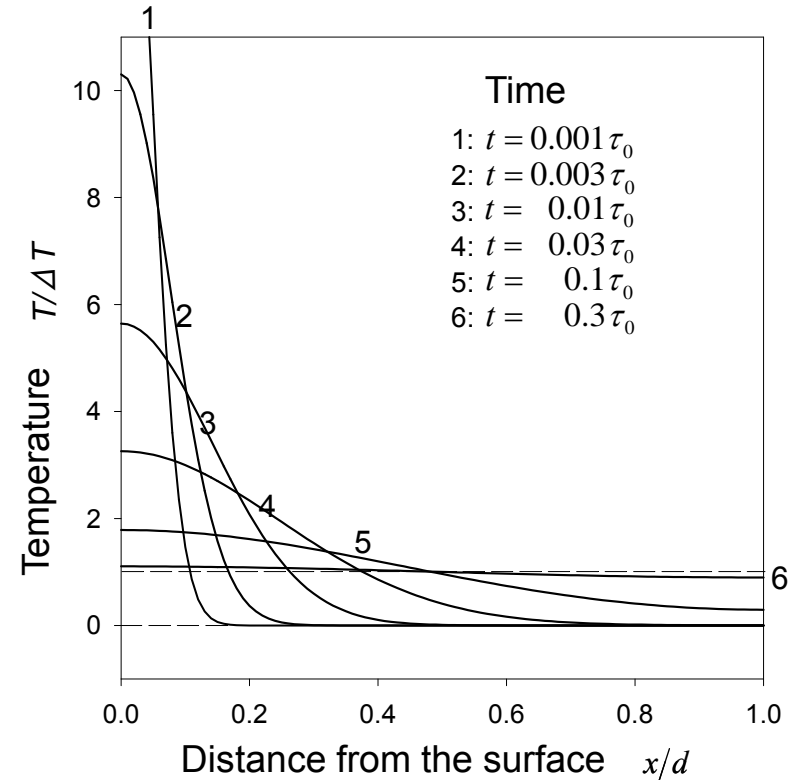
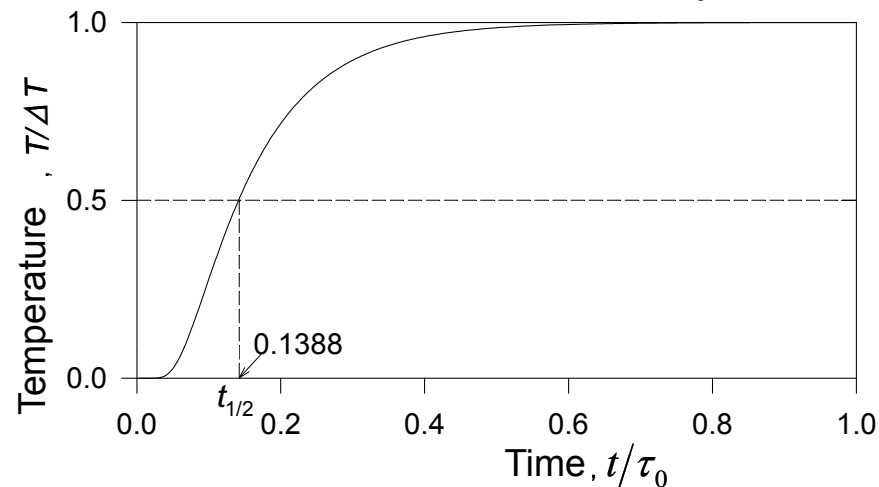
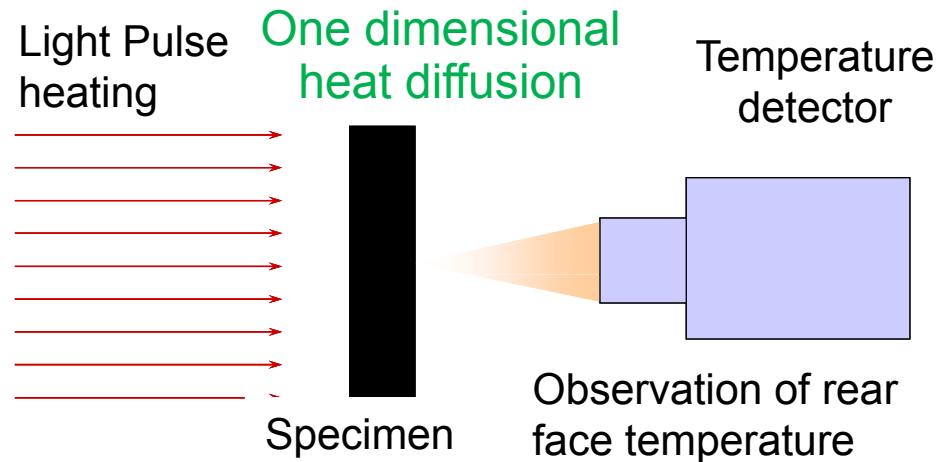
Thermal conductivity

$$\lambda = \frac{d \cdot q_0}{T_f - T_r} = \frac{d \cdot q_0}{\Delta T_{f_r}}$$

Thermal diffusivity,  $\alpha$ ,  
measurement by dynamic method



# Laser flash method

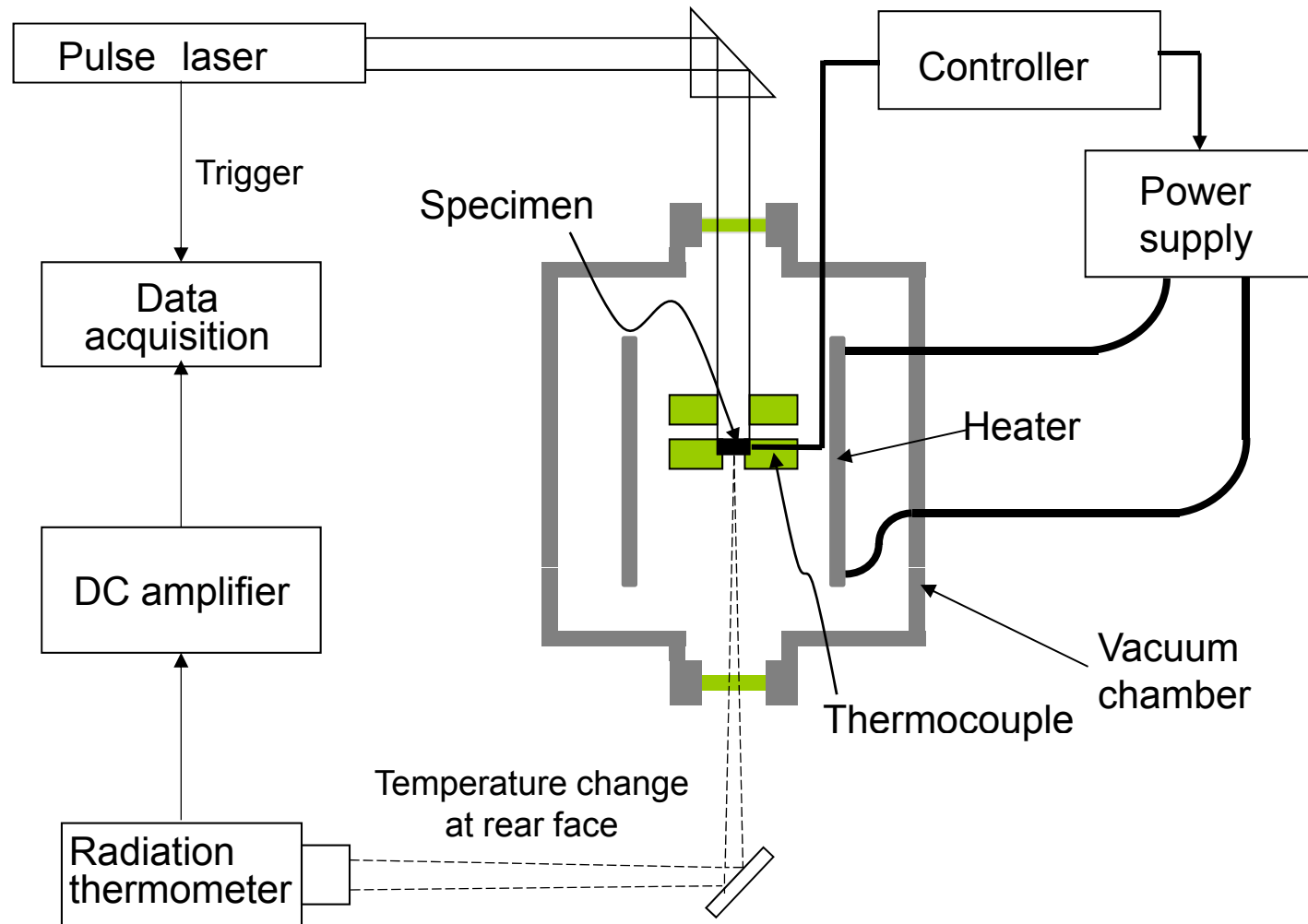


Thermal diffusivity

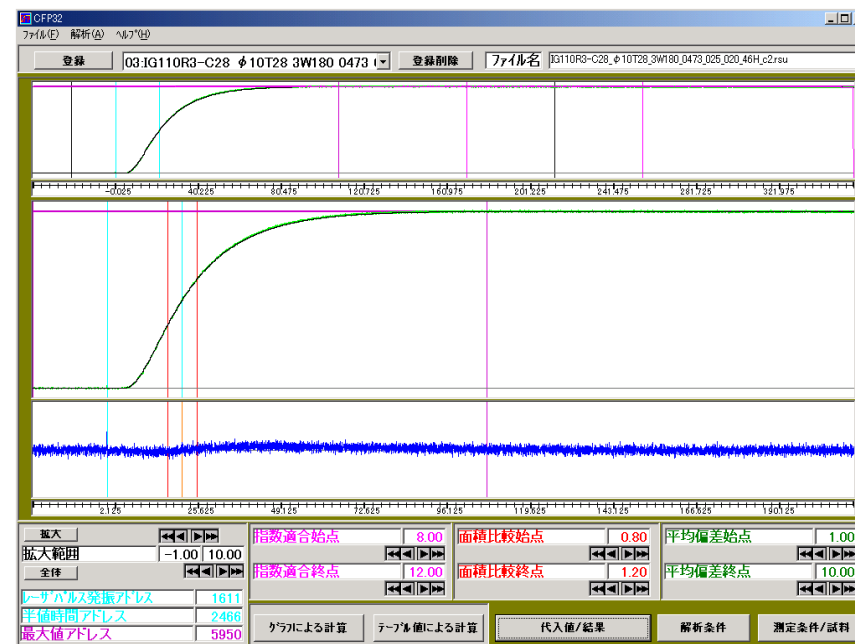
$$\kappa = \frac{d^2}{\tau_0} = 0.1388 \frac{d^2}{t_{1/2}}$$

W. J. Parker, et. al. *J. Appl. Phys.*, vol.32, **1961**, pp1679–84

# Block diagram of the laser flash method



# Thermal diffusivity measurement of carbon by the laser flash method



## Three pilot studies organized by CCT WG9

### CCT-P02 (CCT-S3)

Thermal diffusivity of dense materials

Temperature range

RT - 1000 ° C

Measurement technique

laser flash method

Pilot institute

NMIJ, Japan

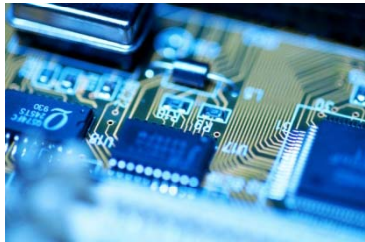
### CCT-S3

#### Information

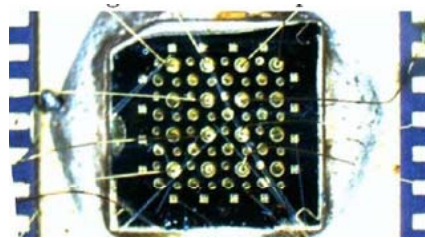
Metrology area, branch	Thermometry, Thermophysical quantities
Description	Thermal diffusivity
Time of measurement	2007 - 2008
Status	Report in progress, Draft A
Reference(s)	No references available
Measurand	Thermal diffusivity in $\text{m}^2\text{s}^{-1}$
Parameter(s)	Temperature: 300 K to 1200 K
Transfer device(s)	Dense materials
Comparison type	Supplementary comparison
Consultative Committee	CCT (Consultative Committee for Thermometry)
Conducted by	CCT (Consultative Committee for Thermometry)
Comments	Measurements using laser flash method for dense materials



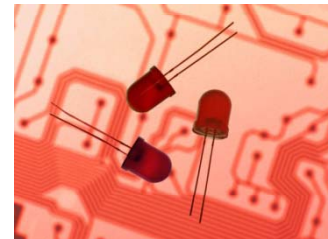
# Needs for thermophysical property data by electronics industry



LSI



Power device



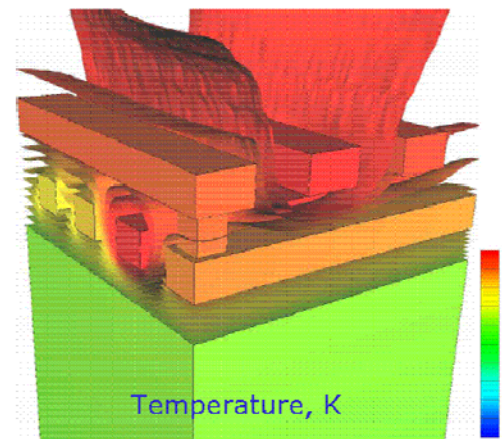
Lighting



Flat panel display

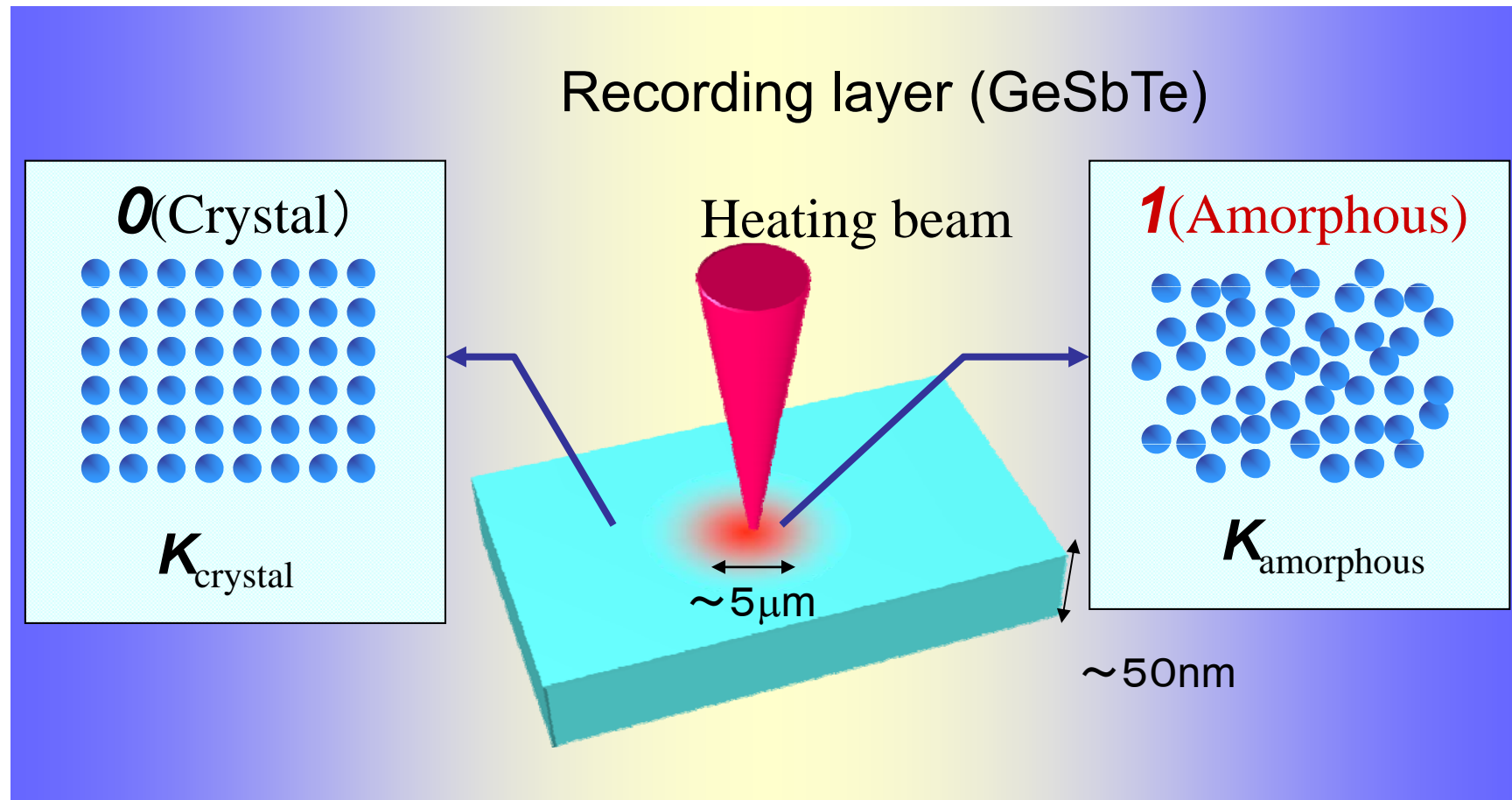
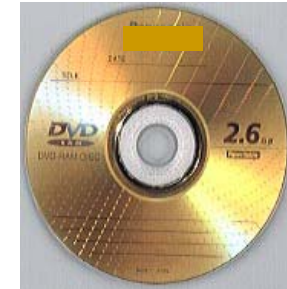
Low K in LSI, AlN and diamond for heat spreader,  
GaN for LED, ITO and IZO in FPD

Thermophysical property data  
Thermal conductivity  
Thermal diffusivity  
Specific heat capacity



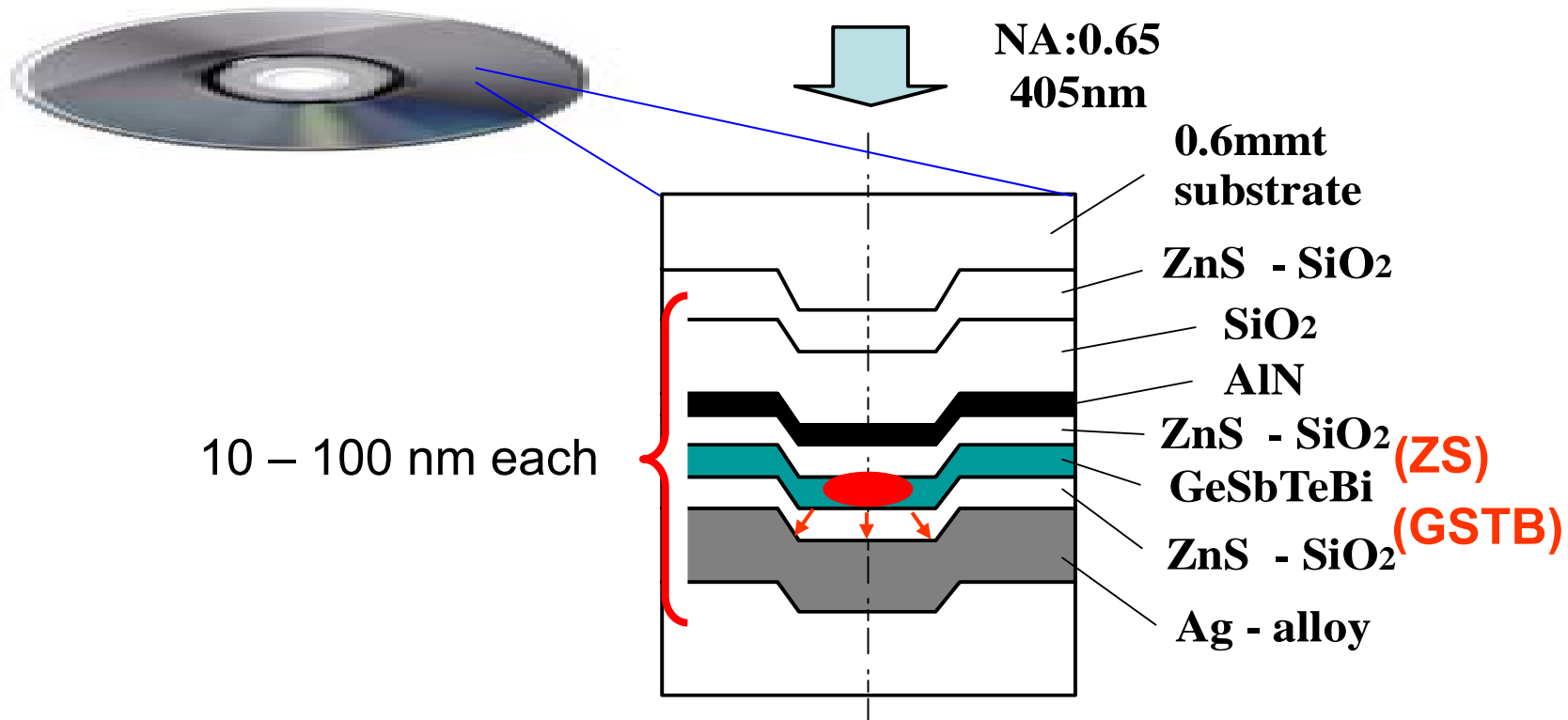
Thermal design  
and simulation

# Recording by phase change in optical recording media

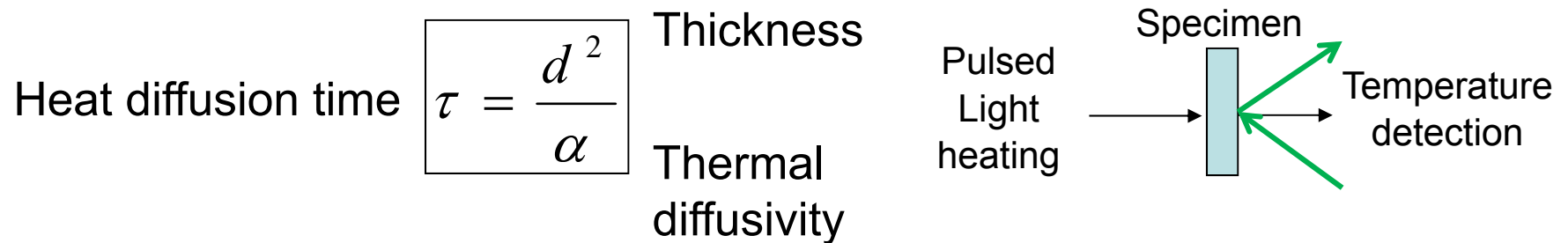


## The Structure of Thin Film Stack : HD DVD-ARW Medium

Reliable values are especially needed for ZS, GSTB and boundary resistance between them.



# Length and time scale of pulsed light heating methods



Laser flash method  
Bulk materials, 1mm

→ 10ms-10s

Observation of radiation

Nanosecond TR method  
Thin films, 1μm

Change of reflectivity  
as a function of  
surface temperature

10ns-10μs

Picosecond TR method  
Thin films, 30nm

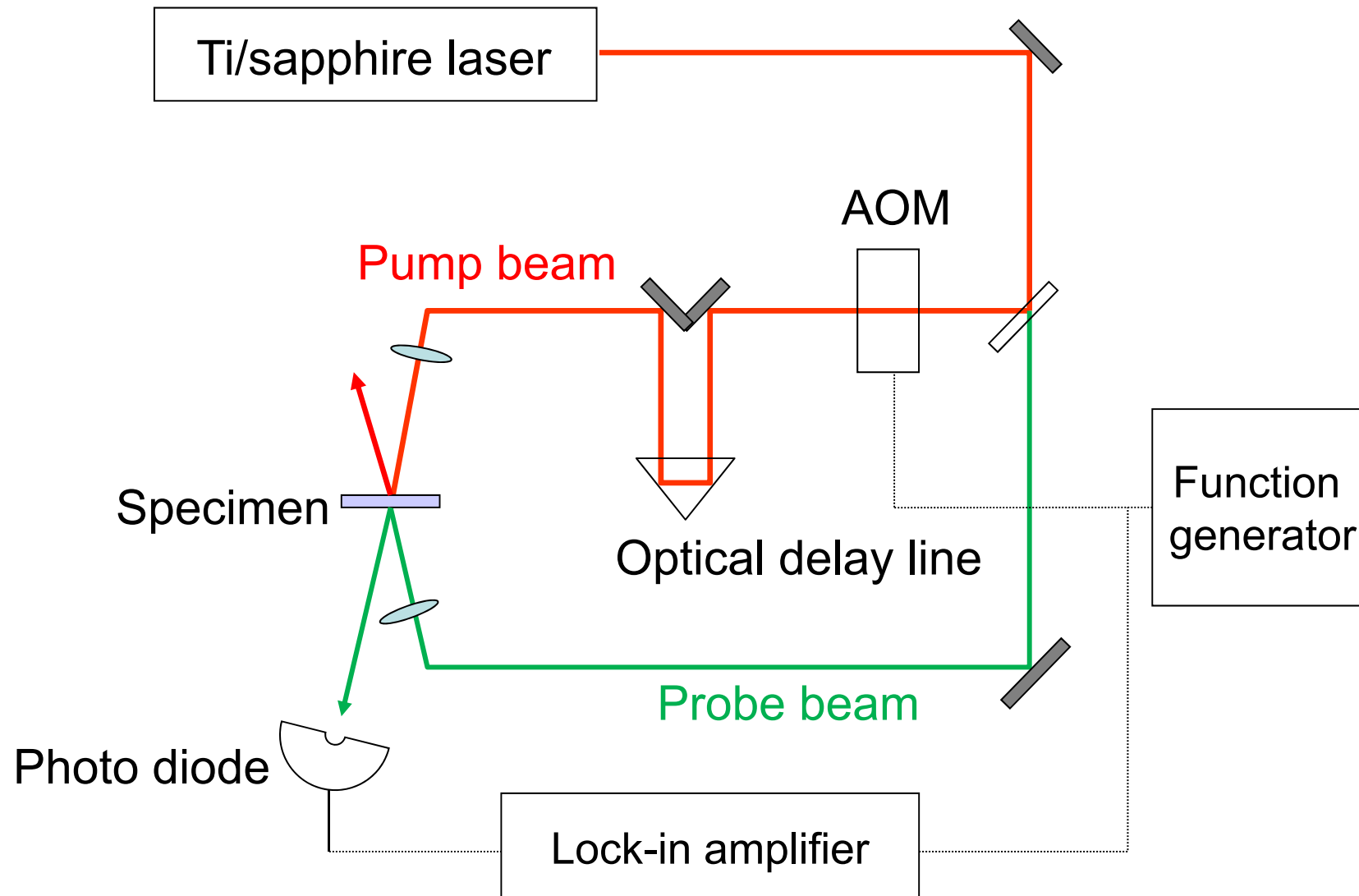
$$R = R_0 + \frac{dR}{dT} \Delta T$$

$$\frac{1}{R} \frac{dR}{dT} = 10^{-4} \sim 10^{-5}$$

Thermoreflectance  
method

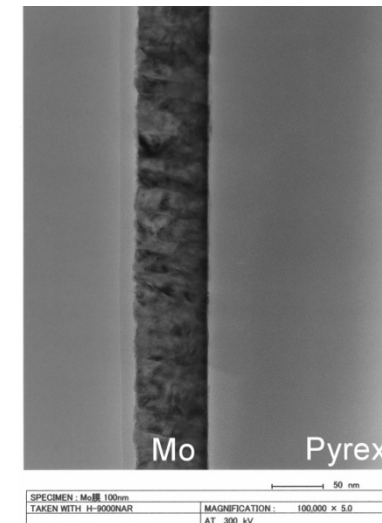
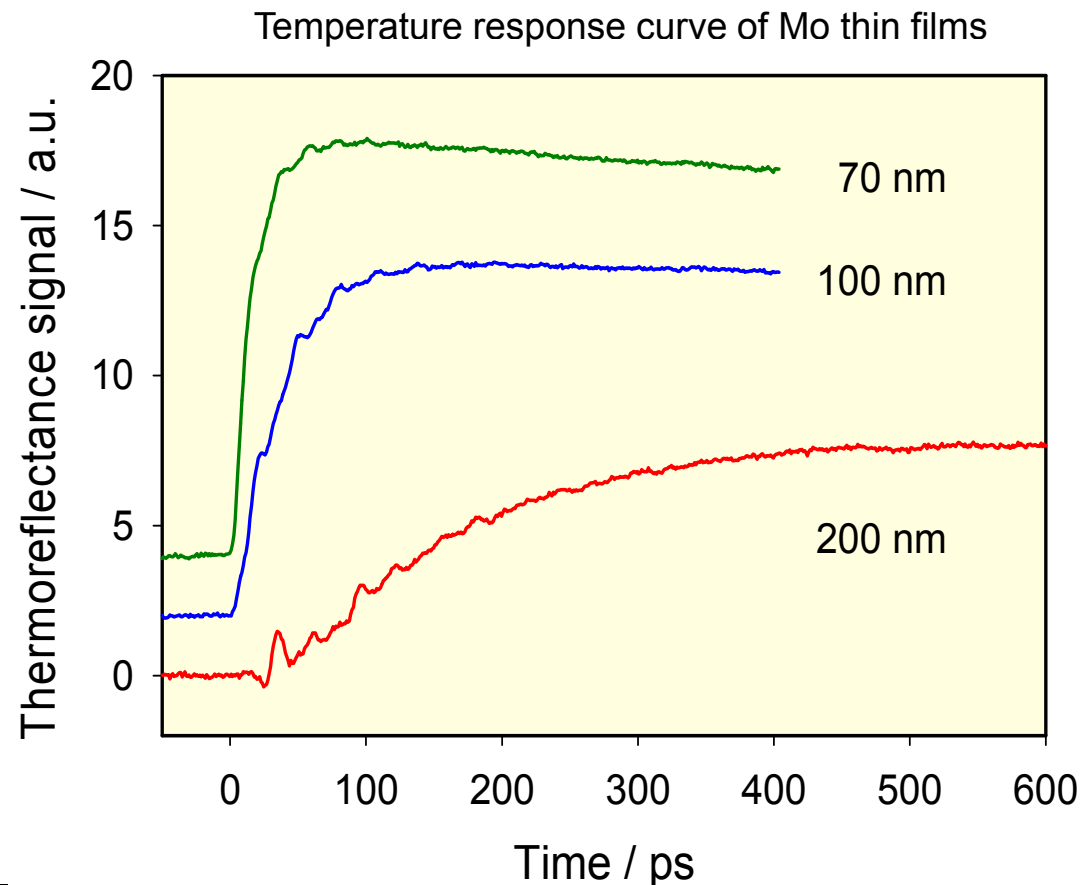
10ps-10ns

# Block diagram of measurement system by the picosecond thermoreflectance method



# Thermal diffusivity of molybdenum thin films measured with the picosecond thermoreflectance method

Synthesized by magnetron DC sputtering  
Substrate: Corning 7740 glass

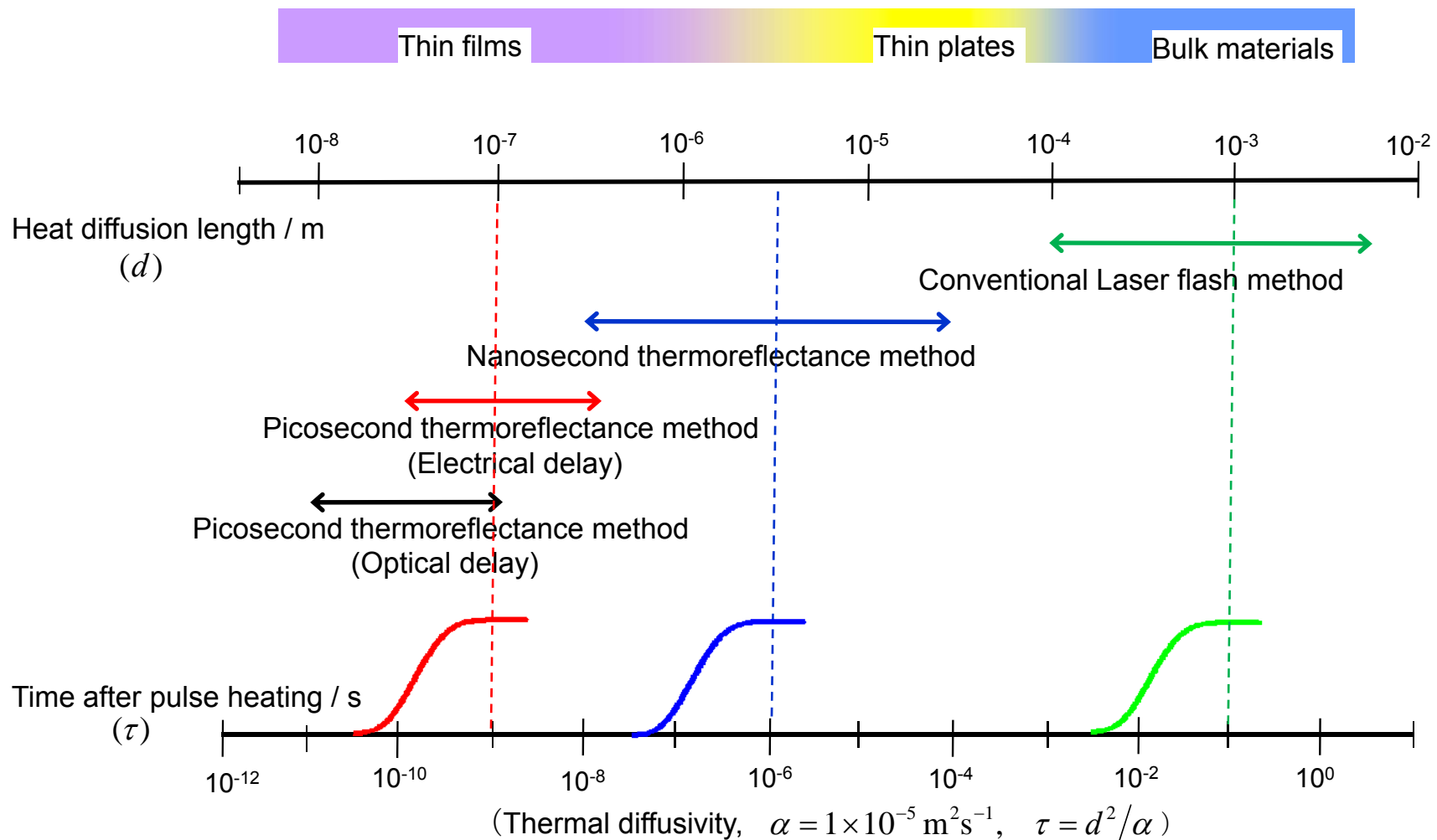


# Thermal diffusivity of molybdenum thin films measured with the picosecond thermoreflectance method

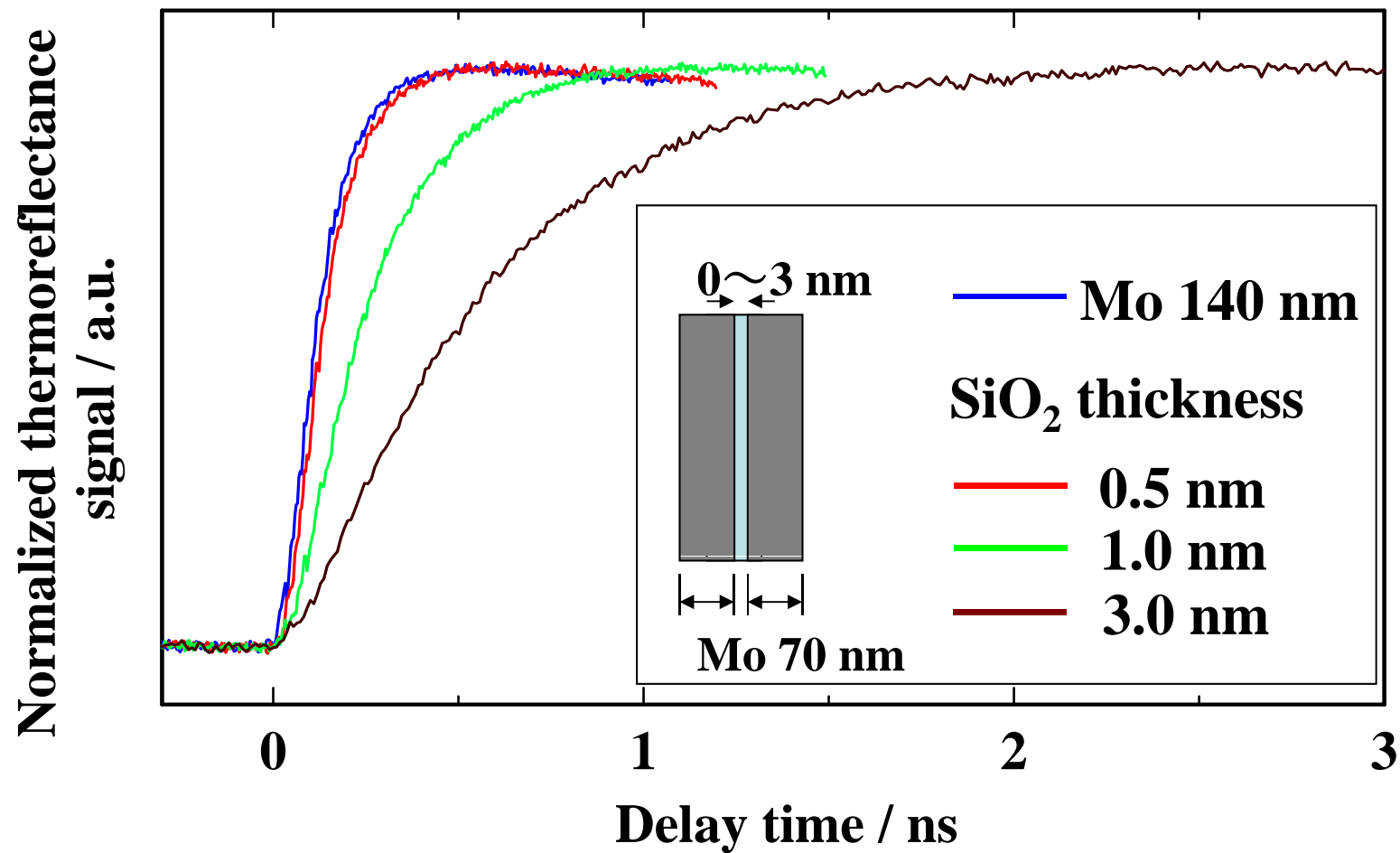
Synthesized by magnetron DC sputtering  
Substrate: Corning 7740 glass

Nominal thickness nm	Measured thickness nm	Absorption coefficient $\times 10^7 \text{ m}^{-1}$	Thermal diffusivity $10^{-5} \text{ m}^2 \text{ s}^{-1}$
70	65.4	5.8	3.0
100	94.6	5.4	3.6
200	191.0	5.0	3.0
Bulk	—	5.5	5.4

# Thermal diffusivity measurements from bulk materials to thin films by pulsed light heating methods







# Definition of areal heat diffusion time

## Areal heat diffusion time

$$A = \int_0^{\infty} [1 - T_r(t) / T_{\max}] dt$$

$$= \lim_{\xi \rightarrow 0} \int_0^{\infty} \exp(-\xi t) [1 - T_r(t) / T_{\max}] dt$$

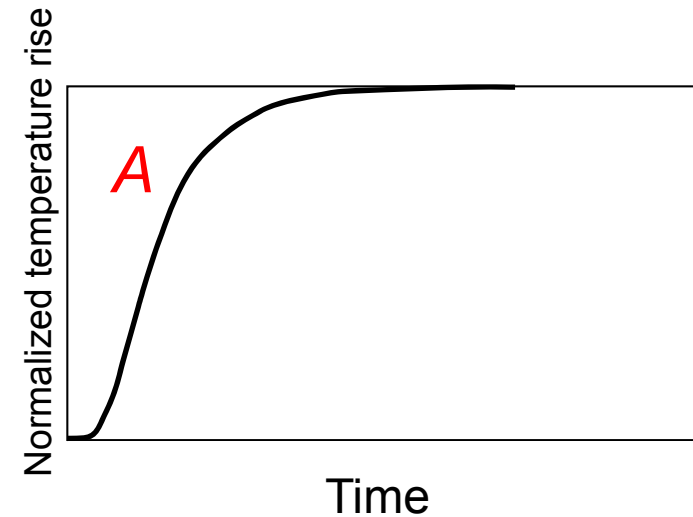
$$= \lim_{\xi \rightarrow 0} \left[ \frac{1}{\xi} - \frac{\tilde{T}_r(\xi)}{T_{\max}} \right]$$

$$= \lim_{\xi \rightarrow 0} \left[ \frac{1}{\xi} - \frac{\tilde{R}_{rf}(\xi)}{T_{\max}} \right]$$

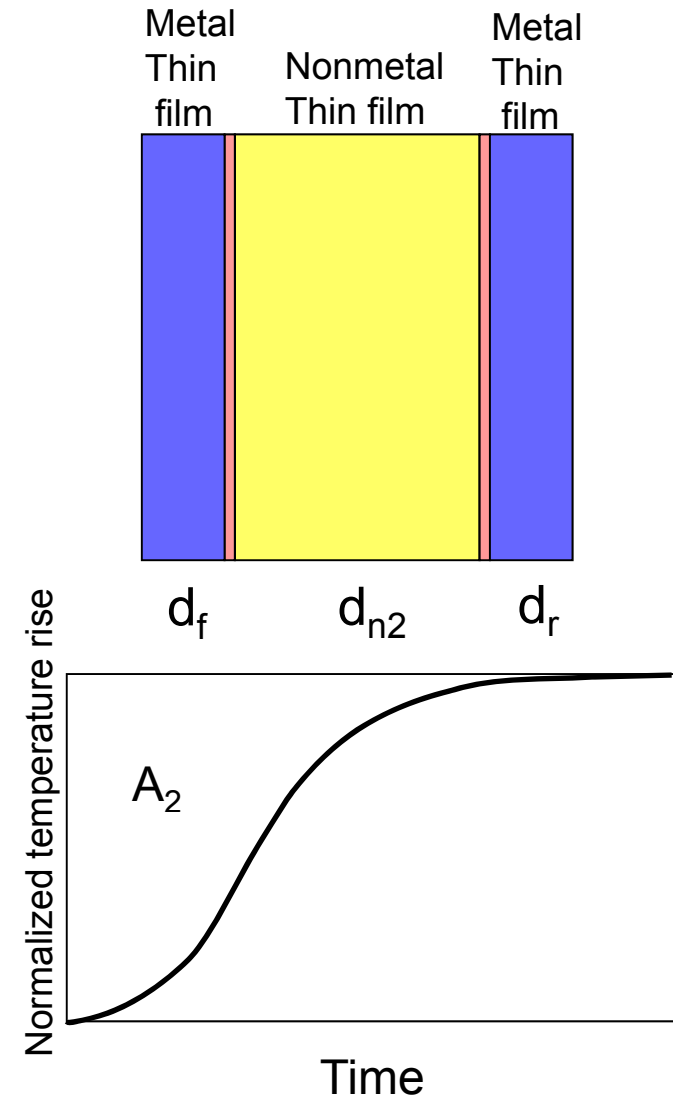
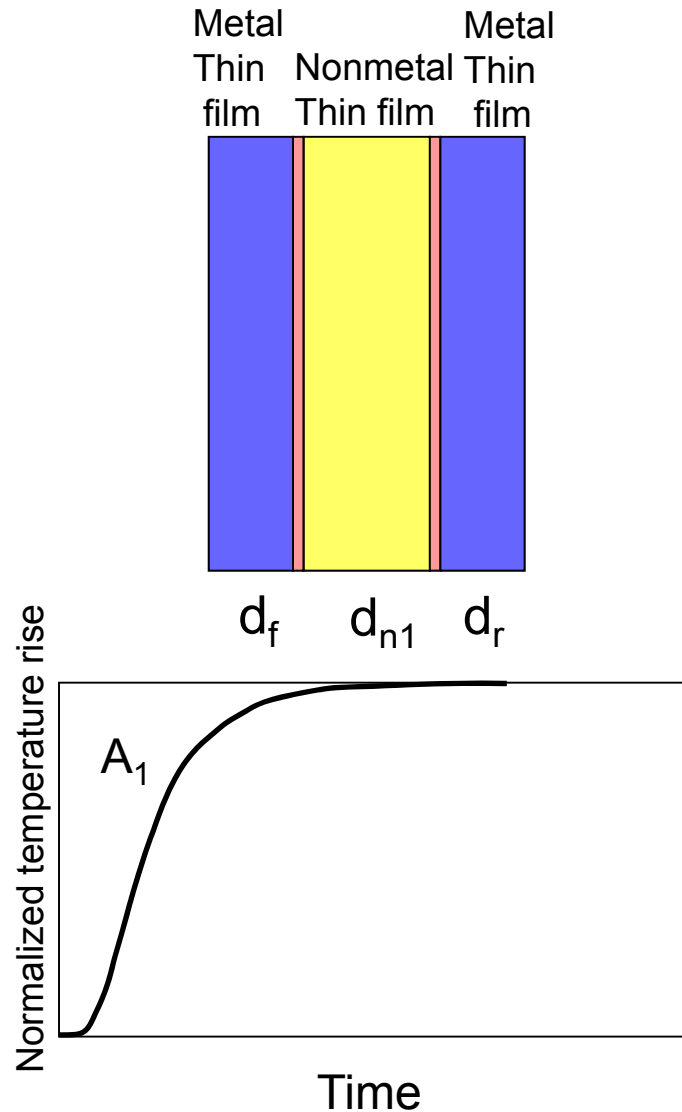
Transfer function

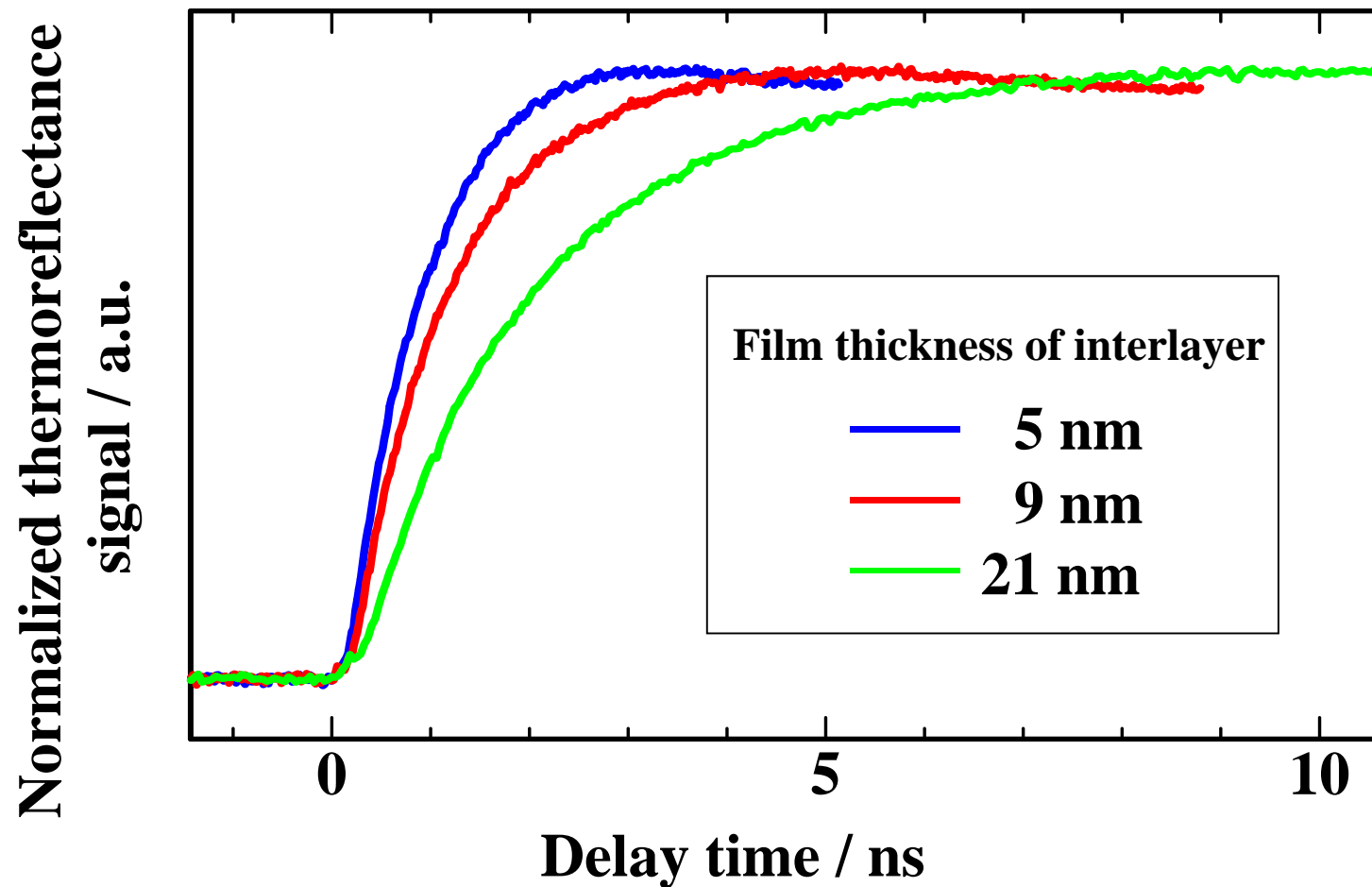
Laplace transformation

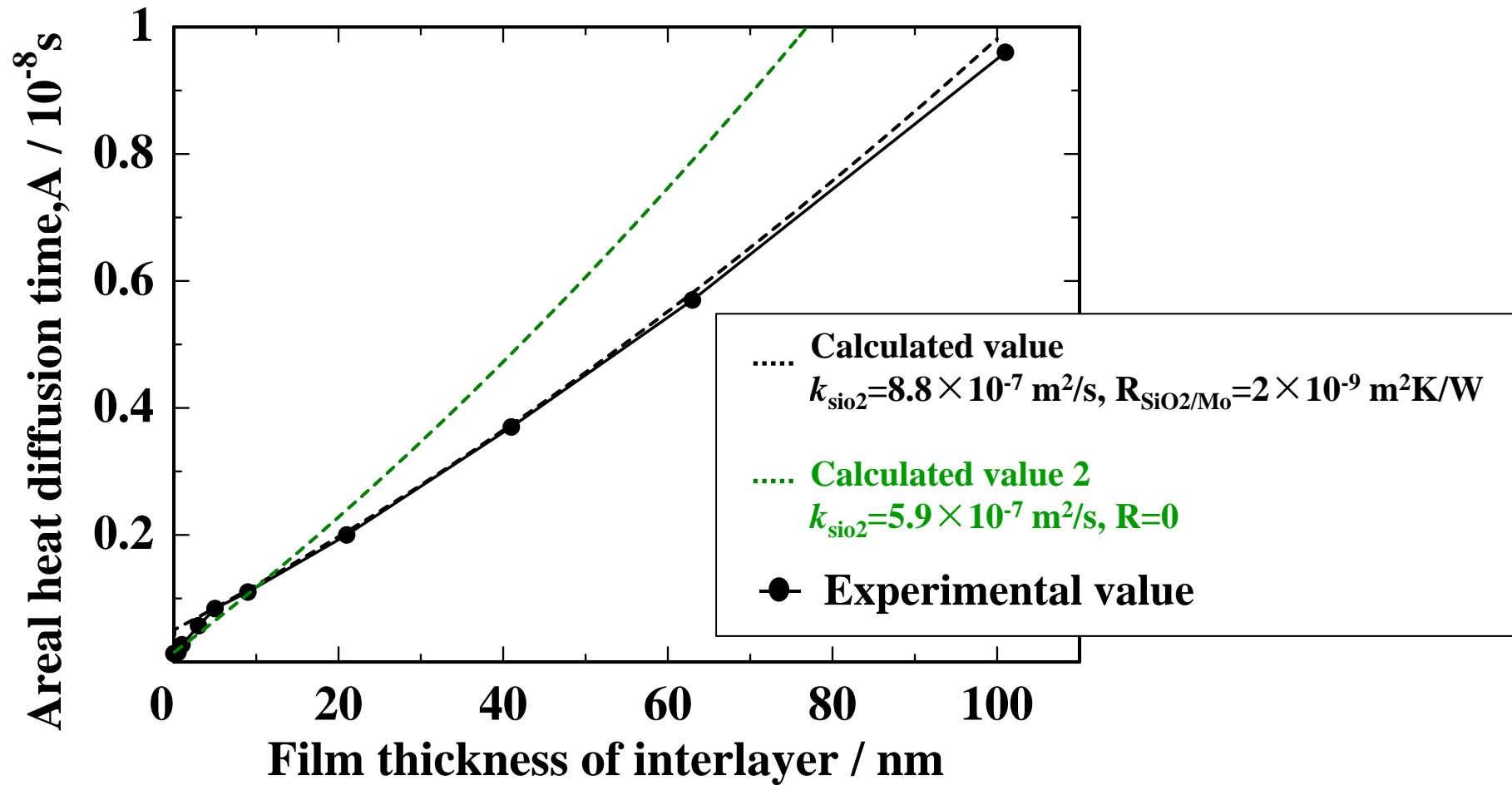
$$\tilde{f}(\xi) = \int_0^{\infty} \exp(-\xi t) f(t) dt$$



# Temperature history curves of 3 layer specimens with different thickness of nonmetal thin film





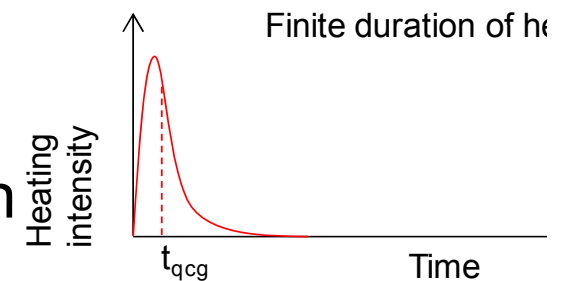


# Thin films and boundary thermal resistances measured by this study

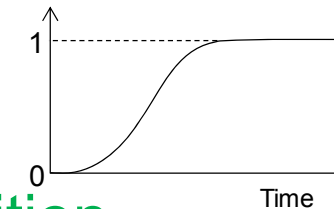
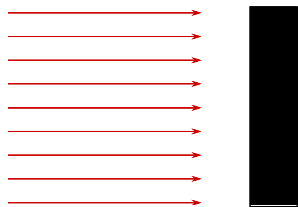
- Metals: Al, Mo, W, Pt, etc.
- Oxides:  $\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{In}_2\text{O}_3$ ,  $\text{ZnO}$ , etc.
- Nitrides:  $\text{TiN}$ ,  $\text{AlN}$ , etc.
- Compounds composed of 3 elements:  
 $\text{Mg}(\text{OH})_2$ ,  $\text{GeSbTe}$ , etc
- Compounds composed of 4 elements:  $\text{AgInSbTe}$ , etc
- Boundary thermal resistance between  
metal layer and nonmetal layer  
 $\text{Mo/SiO}_2$ ,  $\text{Mo/Al}_2\text{O}_3$ ,  $\text{Mo/In}_2\text{O}_3$ , etc.

# Major factors contributing uncertainty of dynamic thermophysical quantity measurement

- Heating      Heating function  
Impulse, step, sinusoidal, etc.  
Intensity variation in time domain

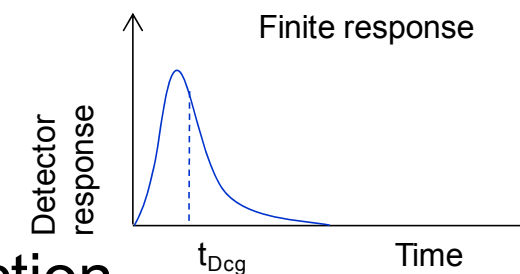


- Geometry      Heat conduction equation  
Shape and dimensions of the specimen  
Heating method and position  
Temperature detection method and position



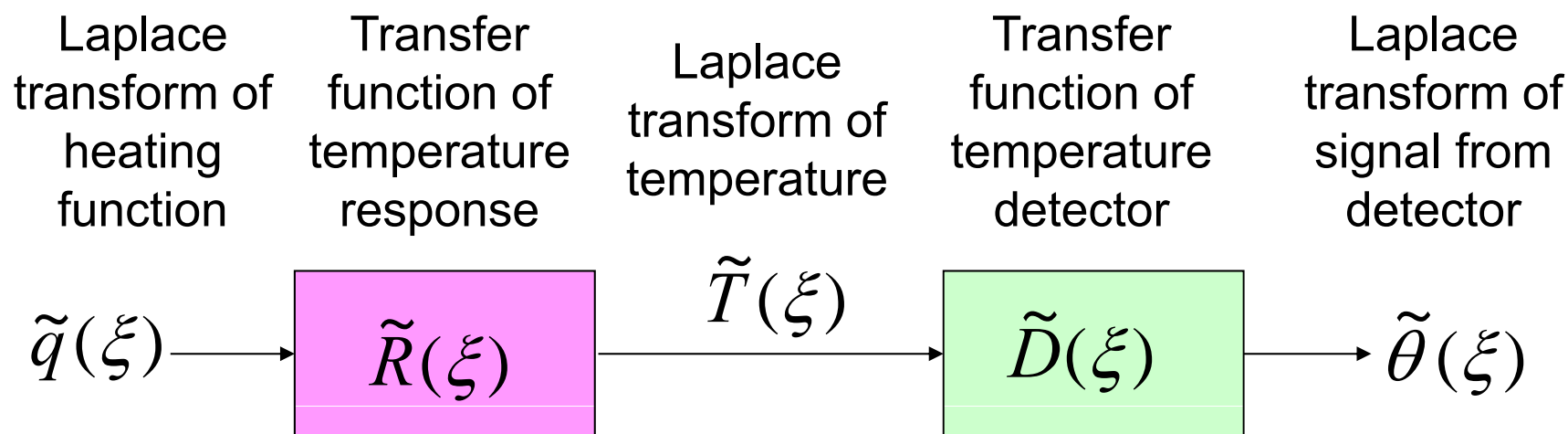
- Response of temperature detection  
Nonlinearity  
Response time

Impulse response function



# Block diagram of dynamic thermophysical quantity measurement

- Heating
- Heat diffusion
- Response of detector

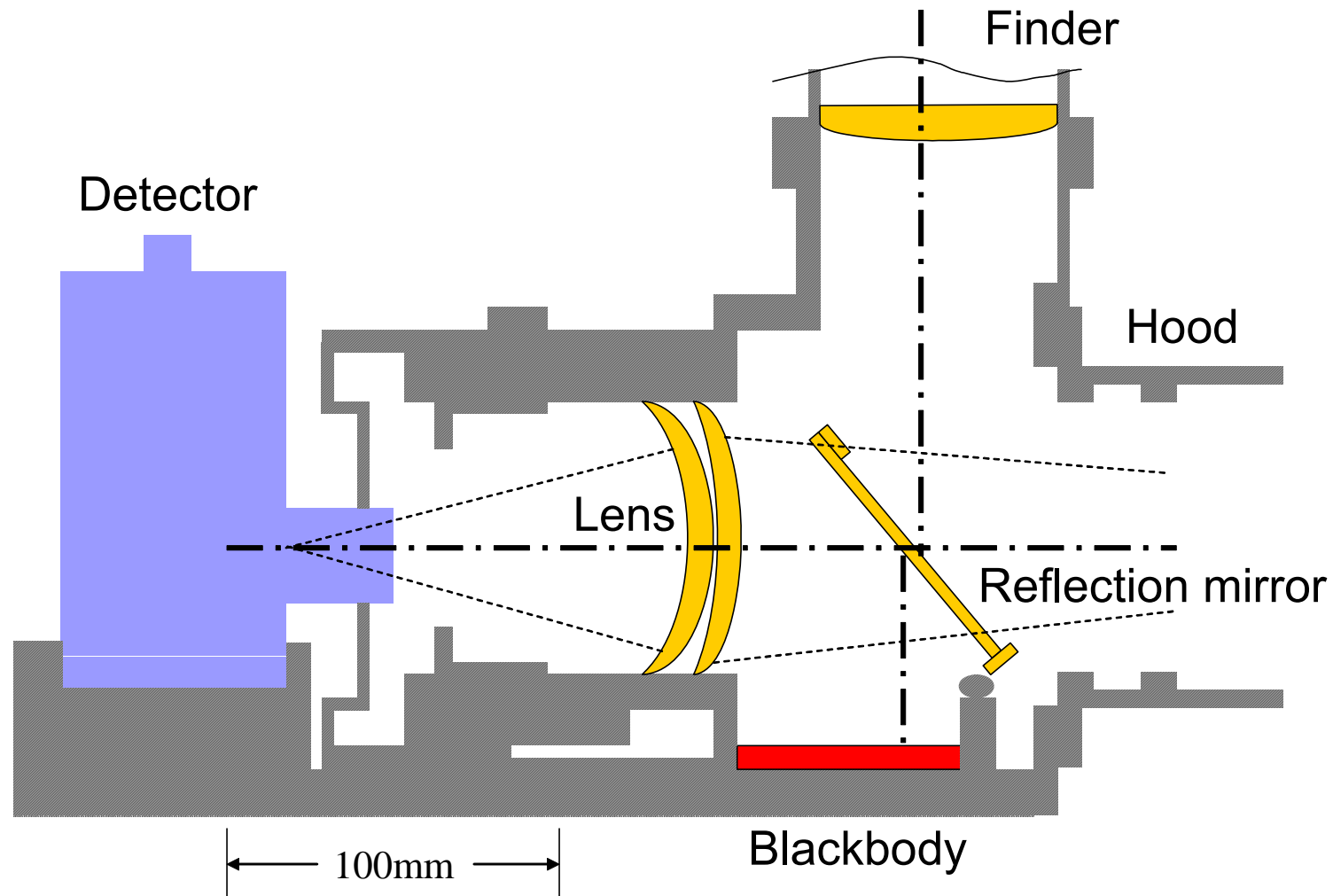


$$\tilde{\theta}(\xi) = \tilde{D}(\xi) \cdot \tilde{R}(\xi) \cdot \tilde{q}(\xi)$$

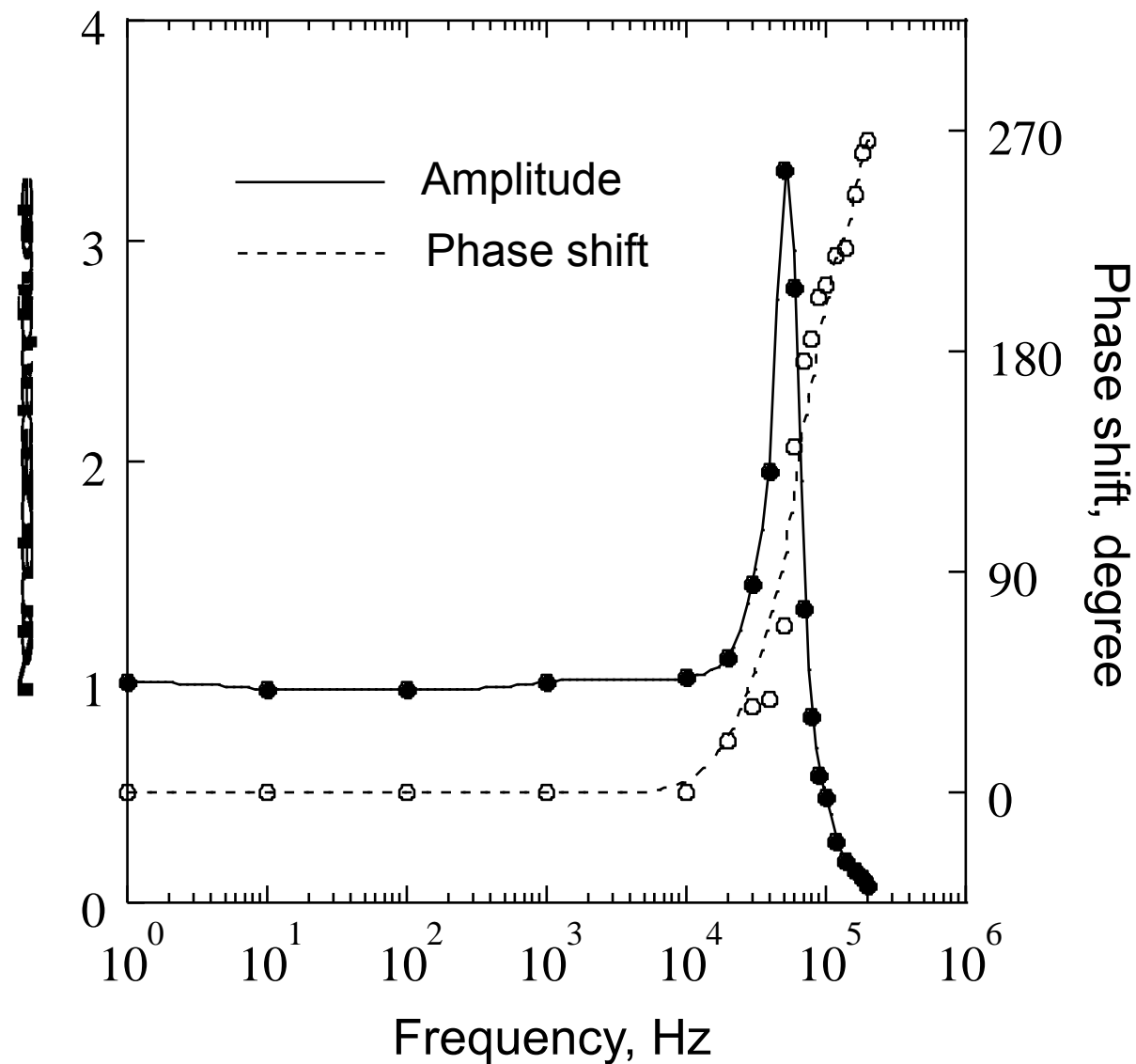
$$\tilde{R}(\xi) = \frac{\tilde{\theta}(\xi)}{\tilde{D}(\xi) \cdot \tilde{q}(\xi)}$$



# Infrared radiation thermometer for laser flash thermal diffusivity measurements



# Frequency response of the infrared radiation thermometer



# Frequency response of the infrared radiation thermometer

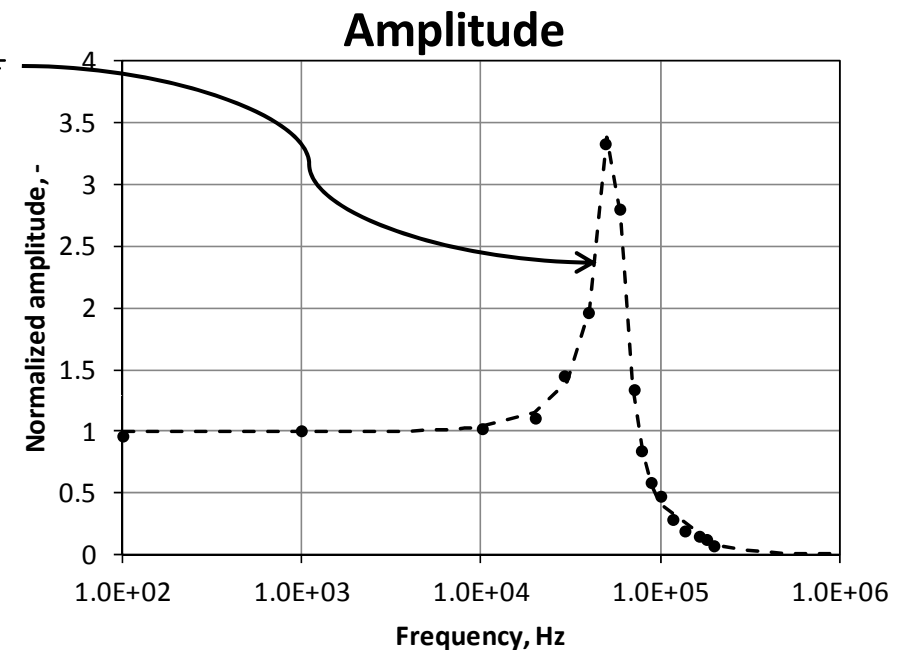
$$F_D(\omega) = \tilde{D}(i\omega) = \frac{\omega_n^2}{(i\omega)^2 + 2\eta(i\omega)\omega_n + \omega_n^2} = \frac{\omega_n^2}{\omega_n^2 - \omega^2 + 2i \cdot \eta \cdot \omega \cdot \omega_n}$$

$$= \frac{\omega_n^2 \cdot (\omega_n^2 - \omega^2)}{(\omega_n^2 - \omega^2)^2 + 4(\eta \cdot \omega \cdot \omega_n)^2} - i \cdot \frac{2\eta \cdot \omega \cdot \omega_n^3}{(\omega_n^2 - \omega^2)^2 + 4(\eta \cdot \omega \cdot \omega_n)^2}$$

$$|F_D(\omega)| = \frac{\omega_n^2}{\sqrt{(\omega_n^2 - \omega^2)^2 + 4(\eta \cdot \omega \cdot \omega_n)^2}}$$

$$\omega_n = 54.6 \text{ kHz}$$

$$\eta = 0.135$$



## Transfer function of detector

$$\tilde{D}(\xi) = \frac{\omega_n^2}{\xi^2 + 2\eta\xi\omega_n + \omega_n^2} \quad \begin{array}{l} \omega_n = 54.6 \text{ kHz} \\ \eta = 0.135 \end{array}$$

$$\bar{D} = \int_0^\infty D(t) dt = \lim_{\xi \rightarrow 0} \int_0^\infty \exp(-\xi t) D(t) dt = \lim_{\xi \rightarrow 0} \tilde{D}(\xi) = 1$$

$$\begin{aligned} t_{Dcg} &= \frac{\int_0^\infty t \cdot D(t) dt}{\bar{D}} = \lim_{\xi \rightarrow 0} \int_0^\infty \exp(-\xi t) \cdot t \cdot D(t) dt = \lim_{\xi \rightarrow 0} \left[ -\frac{d\tilde{D}(\xi)}{d\xi} \right] \\ &= \lim_{\xi \rightarrow 0} \left[ -\frac{d}{d\xi} \left( \frac{\omega_n^2}{\xi^2 + 2\eta\xi\omega_n + \omega_n^2} \right) \right] = \lim_{\xi \rightarrow 0} \left[ \frac{\omega_n^2 \cdot (2\xi + 2\eta\omega_n)}{(\xi^2 + 2\eta\xi\omega_n + \omega_n^2)^2} \right] \end{aligned}$$

$$= \frac{2\eta}{\omega_n} = \frac{2 * 0.135}{5.46 * 10^4 \text{ Hz}} = 4.9 * 10^{-6} \text{ s}$$

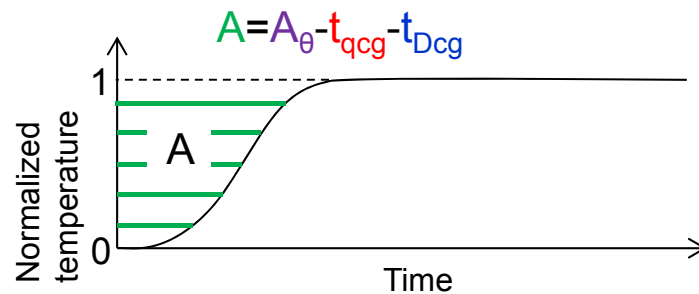
# Analysis of observed areal heat diffusion time

$$\begin{aligned}
 A_\theta &= \int_0^\infty [1 - \theta(t)/\theta_{\max}] dt = \lim_{\xi \rightarrow 0} \int_0^\infty \exp(-\xi t) [1 - \theta(t)/\theta_{\max}] dt \\
 &= \lim_{\xi \rightarrow 0} \left[ \frac{1}{\xi} - \frac{\tilde{\theta}(\xi)}{\theta_{\max}} \right] = \lim_{\xi \rightarrow 0} \left[ \frac{1}{\xi} - \frac{\tilde{D}(\xi) \cdot \tilde{R}_{rf}(\xi) \cdot \tilde{q}_f(\xi)}{\bar{D} \cdot R_{rf \max} \cdot \bar{q}} \right] \\
 &= \lim_{\xi \rightarrow 0} \left[ \frac{1}{\xi} - \frac{(1 - \xi \cdot t_{Dcg}) \cdot \bar{D} \cdot \tilde{R}_{rf}(\xi) \cdot (1 - \xi \cdot t_{qcg}) \cdot \bar{q}}{\bar{D} \cdot R_{rf \max} \cdot \bar{q}} \right] \\
 &= \lim_{\xi \rightarrow 0} \left[ \frac{1}{\xi} - \frac{\tilde{R}_{rf}(\xi)}{R_{rf \max}} \right] + t_{Dcg} + t_{qcg} = A_T + t_{Dcg} + t_{qcg}
 \end{aligned}$$

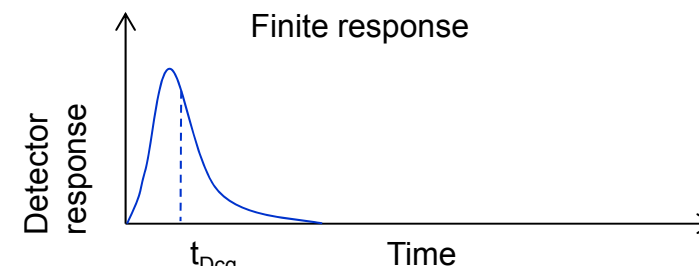
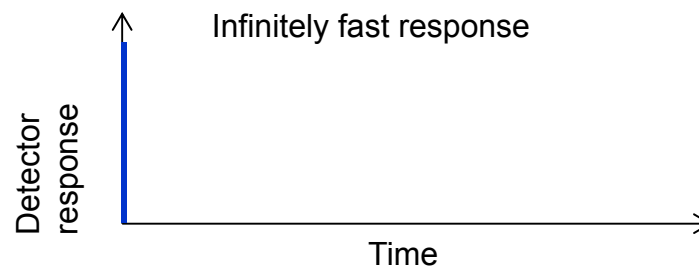
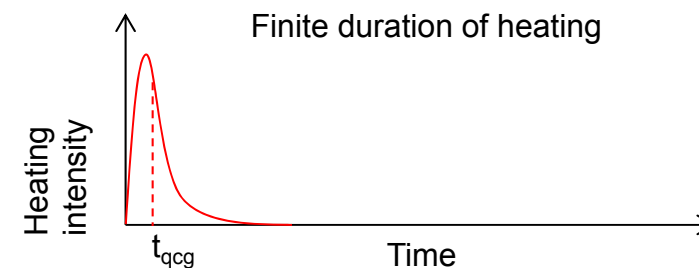
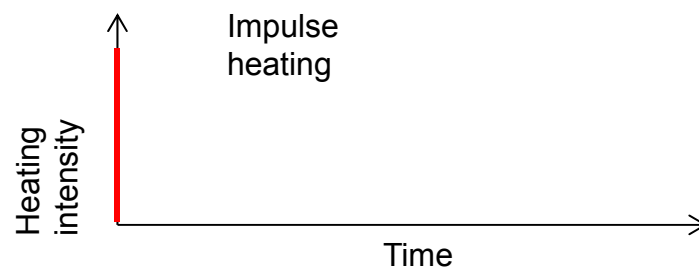
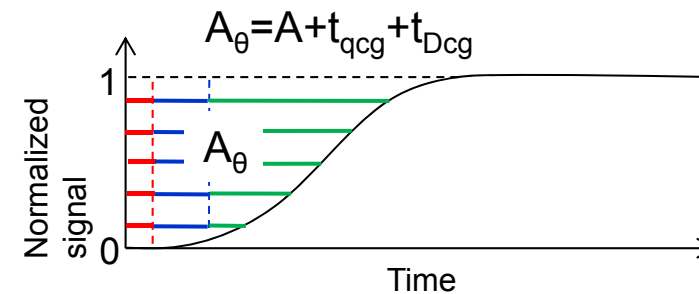
$$A_T = A_\theta - t_{Dcg} - t_{qcg}$$

# Correction of observed areal heat diffusion time for finite duration of the heating function and finite response of temperature detector

Ideal signal



Observed signal



# Uncertainty evaluation for pulsed light heating methods

1. Heat diffusion time:  $\tau_0$   Evaluated by transfer function and areal heat diffusion time

- Heating
- Heat conduction equation

Shape and dimensions of the specimen

Boundary conditions

Heating method and position

Temperature detection method and position

- Temperature detection
  - Nonlinearity
  - Response time

Thermal diffusivity at  $T$

$$\alpha = \frac{d^2}{\tau_0}$$

2. Thickness of the specimen:  $d$

3. Steady temperature of the specimen:  $T$

## Summary

- Light pulse heating methods have been developed to measure thermal diffusivity from bulk materials thicker than 1 mm to films thinner than 100 nm.
- One dimensional heat diffusion can be analyzed by the response function method and the areal heat diffusion time method.
- Uncertainty of finite heating distribution, evaluation of heat diffusion in material and finite response of detector can be universally analyzed by transfer functions and areal heat diffusion time.