

Guide to the Realization of the ITS-90

Fixed Points: Influence of Impurities

APPENDIX 1: *Derivation of an approximate relation between the equilibrium distribution coefficient and thermodynamic quantities*



APPENDIX 1

Derivation of an approximate relation between the equilibrium distribution coefficient and thermodynamic quantities

At an equilibrium solid-liquid phase transition, the chemical potentials of the host material A in the liquid (μ_{lA}) and solid phases (μ_{sA}) have to be equal:

$$\mu_{lA} = \mu_{sA} , \quad (\text{A1.1})$$

where their general expressions are:

$$\mu_{lA} = \mu_{lA}^0 + RT \ln \left(\frac{a_{lA}}{a_{lA}^0} \right) , \quad (\text{A1.2})$$

$$\mu_{sA} = \mu_{sA}^0 + RT \ln \left(\frac{a_{sA}}{a_{sA}^0} \right) . \quad (\text{A1.3})$$

In these expressions, a is the symbol for the chemical activity, and the zero marks the reference values. If the pure host material A is used as the reference, one has

$$a_{sA}^0 = a_{lA}^0 = 1 , \text{ and} \quad (\text{A1.4})$$

$$\Delta\mu_A^0 = \mu_{lA}^0 - \mu_{sA}^0 = \Delta G_{MA} , \quad (\text{A1.5})$$

with ΔG_{MA} being the free enthalpy of fusion of material A. For ideal solutions, the chemical activity a is equal to the concentration c . In a binary system, the concentrations of the components A and B are directly linked: $c_{sA} = 1 - c_{sB}$ and $c_{lA} = 1 - c_{lB}$. From Equations (A1.1) to (A1.5) it follows in this case:

$$\Delta G_{MA} = RT \ln \left(\frac{1 - c_{sB}}{1 - c_{lB}} \right) . \quad (\text{A1.6})$$

For small concentrations of component B, the following approximation can be used:

$$\ln \left(\frac{1 - c_{sB}}{1 - c_{lB}} \right) \approx (c_{lB} - c_{sB}) . \quad (\text{A1.7})$$

The application of the Gibbs-Helmholtz equation ($\Delta G = \Delta H - T\Delta S$) to the melting yields

$$\Delta G_{MA} = \Delta H_{MA} - T\Delta S_{MA} , \quad (\text{A1.8})$$

where ΔH_{MA} is the enthalpy of fusion and $\Delta S_{MA} = \Delta H_{MA}/T_{MA}$ is the entropy of fusion (T_{MA} melting temperature of the pure material A). Since the equilibrium distribution coefficient is defined by $k_0^B = c_{SB} / c_{IB}$, Equations (A1.6) to (A1.8) yield

$$k_0^B = 1 - \frac{\Delta H_{MA}(T_{MA} - T)}{RTc_{IB}T_{MA}} . \quad (A1.9)$$

For small concentrations of component B, it is furthermore possible to assume that $T \approx T_{MA}$ and ΔH_{MA} is independent of concentration and temperature, i.e. Equation (A1.9) can be simplified further:

$$k_0^B = 1 - \frac{\Delta H_{MA}(T_{MA} - T)}{RT_{MA}^2 c_{IB}} = 1 - A \frac{(T_{MA} - T)}{c_{IB}} . \quad (A1.10)$$

In Equation (A1.10), A is the first cryoscopic constant. Since the ratio $(T - T_{MA})/c_{IB}$ is practically equal to the slope of the liquidus line $m_1^B = \partial T_1 / \partial c_{IB}$, one obtains finally the following approximate relation

$$m_1^B = \partial T_1 / \partial c_{IB} = -(1 - k_0^B) / A . \quad (A1.11)$$

In summary, the following assumptions were made for deriving Equation (A1.11) at low concentrations of component B: (i) ideal solution, (ii) Relation (A1.7), (iii) $T \approx T_{MA}$, and (iv) ΔH_{MA} is independent of concentration and temperature.

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