

# Guide to the Realization of the ITS-90

## Fixed Points: Influence of Impurities

APPENDIX 1: *Derivation of an approximate relation between the equilibrium distribution coefficient and thermodynamic quantities*



## APPENDIX 1

### Derivation of an approximate relation between the equilibrium distribution coefficient and thermodynamic quantities

At an equilibrium solid-liquid phase transition, the chemical potentials of the host material A in the liquid ( $\mu_{lA}$ ) and solid phases ( $\mu_{sA}$ ) have to be equal:

$$\mu_{lA} = \mu_{sA} , \quad (\text{A1.1})$$

where their general expressions are:

$$\mu_{lA} = \mu_{lA}^0 + RT \ln \left( \frac{a_{lA}}{a_{lA}^0} \right) , \quad (\text{A1.2})$$

$$\mu_{sA} = \mu_{sA}^0 + RT \ln \left( \frac{a_{sA}}{a_{sA}^0} \right) . \quad (\text{A1.3})$$

In these expressions,  $a$  is the symbol for the chemical activity, and the zero marks the reference values. If the pure host material A is used as the reference, one has

$$a_{sA}^0 = a_{lA}^0 = 1 , \text{ and} \quad (\text{A1.4})$$

$$\Delta\mu_A^0 = \mu_{lA}^0 - \mu_{sA}^0 = \Delta G_{MA} , \quad (\text{A1.5})$$

with  $\Delta G_{MA}$  being the free enthalpy of fusion of material A. For ideal solutions, the chemical activity  $a$  is equal to the concentration  $c$ . In a binary system, the concentrations of the components A and B are directly linked:  $c_{sA} = 1 - c_{sB}$  and  $c_{lA} = 1 - c_{lB}$ . From Equations (A1.1) to (A1.5) it follows in this case:

$$\Delta G_{MA} = RT \ln \left( \frac{1 - c_{sB}}{1 - c_{lB}} \right) . \quad (\text{A1.6})$$

For small concentrations of component B, the following approximation can be used:

$$\ln \left( \frac{1 - c_{sB}}{1 - c_{lB}} \right) \approx (c_{lB} - c_{sB}) . \quad (\text{A1.7})$$

The application of the Gibbs-Helmholtz equation ( $\Delta G = \Delta H - T\Delta S$ ) to the melting yields

$$\Delta G_{MA} = \Delta H_{MA} - T\Delta S_{MA} , \quad (\text{A1.8})$$

where  $\Delta H_{MA}$  is the enthalpy of fusion and  $\Delta S_{MA} = \Delta H_{MA}/T_{MA}$  is the entropy of fusion ( $T_{MA}$  melting temperature of the pure material A). Since the equilibrium distribution coefficient is defined by  $k_0^B = c_{SB} / c_{IB}$ , Equations (A1.6) to (A1.8) yield

$$k_0^B = 1 - \frac{\Delta H_{MA}(T_{MA} - T)}{RTc_{IB}T_{MA}} . \quad (\text{A1.9})$$

For small concentrations of component B, it is furthermore possible to assume that  $T \approx T_{MA}$  and  $\Delta H_{MA}$  is independent of concentration and temperature, i.e. Equation (A1.9) can be simplified further:

$$k_0^B = 1 - \frac{\Delta H_{MA}(T_{MA} - T)}{RT_{MA}^2 c_{IB}} = 1 - A \frac{(T_{MA} - T)}{c_{IB}} . \quad (\text{A1.10})$$

In Equation (A1.10),  $A$  is the first cryoscopic constant. Since the ratio  $(T - T_{MA})/c_{IB}$  is practically equal to the slope of the liquidus line  $m_1^B = \partial T_1 / \partial c_{IB}$ , one obtains finally the following approximate relation

$$m_1^B = \partial T_1 / \partial c_{IB} = -(1 - k_0^B) / A . \quad (\text{A1.11})$$

In summary, the following assumptions were made for deriving Equation (A1.11) at low concentrations of component B: (i) ideal solution, (ii) Relation (A1.7), (iii)  $T \approx T_{MA}$ , and (iv)  $\Delta H_{MA}$  is independent of concentration and temperature.

*Last updated 1 January 2018*