

Sound field reconstruction and beamforming based on measurements of the acousto-optic effect

Guest lecture

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Outline

- Introduction
- ✓ The propagation of light
- ✓ The acousto-optic effect
- Application 1: Visualization of sound fields
 - Tomography
 - Acousto-optic tomography
- Application 2: Beamforming
 - Conventional beamforming
 - Spatial aliasing
 - Acousto-optic beamformer



Introduction





• The measurement of sound with conventional techniques requires the immersion of the transducers into the sound field.



The propagation of light

Electromagnetic wave equation:

 ${\bf E}$: Electric field

n

 ρ

 c_0-c

 c_0

 $[kg/m^3]$

[%]

- \boldsymbol{n} : refractive index
- c_0 : speed of light in vacuum

OBS Light travels slower in dense media

1

0

0

• What happens	if the	properties	of the	medium	are	not	constant?
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~1.0003

~1.2

0.03

The refractive index changes _____ The propagation of light is influenced

5			
	Vacuum	Air	Water

$\nabla^2 \mathbf{E} - \frac{1}{c^2} \frac{\partial^2 \mathbf{E}}{\partial t^2} = 0$



~1.3

~1000

~23









The propagation of light

• What does it influence the refractive index in air?

- Temperature
- Pressure
- Humidity

• ...

+ DFM

6

The propagation of light

• What does it influence the refractive index in air?

Pressure

Temperature

Humidity

> Example: Road mirages

Large temperature gradients above the pavement bend the light

rays coming from the sky.





...







The acousto-optic effect

Physical principle:





The acousto-optic effect

- In air and within the audible frequency range, the acousto-optic effect changes the phase of light (ϕ) , but not its amplitude.
 - Can we still use the electromagnetic wave equation?
 - (T: is the oscillation period of light)
 - Let us assume the following solution to the electromagnetic wave equation:
- (E.g. when light propagates along the x-direction)

$$j\frac{\partial^2\phi}{\partial x^2} - \left(\frac{\partial\phi}{\partial x}\right)^2 - \left(\frac{n}{c_0}\right)^2 \left(j\frac{\partial^2\phi}{\partial t^2} - \left(\omega_o + \frac{\partial\phi}{\partial t}\right)^2\right) = 0 \quad \checkmark \quad \nabla^2 \mathbf{E} - \left(\frac{n}{c_0}\right)^2 \frac{\partial^2 \mathbf{E}}{\partial t^2} = 0$$
$$\phi(x, y, t) = k_0 n_0 L_0 + k_0 \frac{n_0 - 1}{\gamma p_0} \int_L p(x, y, t) dt$$

 $\left|\frac{1}{n}\frac{\partial n}{\partial t}T\right| \ll 1$

 $\mathbf{E} = \mathbf{E}_0 e^{j(\omega t + \phi(x, y, t))}$

How can we measure the acousto-optic effect?

 We can measure the phase of a beam of light using a laser Doppler vibrometer (LDV)

Mechanical
$$v_{LDV}(t) = rac{\mathrm{d}L}{\mathrm{d}t}$$





How can we measure the acousto-optic effect?

We can measure the phase of a beam of light using a laser Doppler vibrometer (LDV)

Mechanical
vibrations
$$v_{LDV}(t) = \frac{dL}{dt}$$

Acousto-optic effect
 $v_{LDV}(t) = \frac{n_0 - 1}{\gamma p_0 n_0} \frac{d}{dt} \left(\int_L p(x, y, t) dt \right)$

T.

Application 1: Sound field visualization

 Can we use the apparent velocity measured with the LDV to visualize an acoustic field?

$$v_{LDV}(t) = \frac{n_0 - 1}{\gamma p_0 n_0} \frac{\mathrm{d}}{\mathrm{d}t} \left(\int_L p(x, y, t) \mathrm{d}t \right)$$



The sound pressure can be reconstructed using tomographic techniques



Tomography







Acousto-optic tomography The phase of the light integrates the 0.6acoustic field: Laser beam: $\phi \propto \int_{U} p(x, y) dx$ 0.4 $\phi = k_0 n_0 L + k_0 \frac{n_0 - 1}{\gamma p_0} \int_0^L p(x, y) dx$ 0.2 $y \ [m]$ 0 Projection of the sound field -0.2-0.4Radon Transform: $R_p(x', \theta) = \int_0^L p(x, y) dx$ -0.6-0.6 -0.4 -0.20 0.20.40.6x [m]With a laser Doppler vibrometer: $v_{LDV}(t) = \frac{n_0 - 1}{\gamma n_0 n_0} \frac{\mathrm{d}}{\mathrm{d}t} \left(R_p(x', \theta) \right)$





Acousto-optic tomography

- The acoustic field cannot directly be $v_{LDV}(t) = \frac{n_0 1}{\gamma p_0 n_0} \frac{d}{dt} (R_p(x', \theta))$ measured.
- The Radon transform of the acoustic field can be obtained with an LDV,

$$R_p(x',\theta) = \frac{\gamma p_0 n_0}{n_0 - 1} \int v_{LDV}(t) \mathrm{d}t$$







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- A single line scan is not enough.
- Complete reconstruction of an arbitrary sound field requires:
 - Parallel lines scanning over a plane.



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- The acoustic field cannot directly be measured.
- The Radon transform of the acoustic field can be obtained with an LDV,

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- A single line scan is not enough.
- Complete reconstruction of an arbitrary sound field requires:
 - Parallel lines scanning over a plane.
 - Take projections in different directions.

$$v_{LDV}(t) = \frac{n_0 - 1}{\gamma p_0 n_0} \frac{\mathrm{d}}{\mathrm{d}t} \left(R_p(x', \theta) \right)$$





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• Projecting the acoustic field into different directions yields a very well defined inverse problem, $\begin{bmatrix} R_p(x'_1, \theta_1) & R_p(x'_1, \theta_2) & \dots & R_p(x'_1, \theta_n) \\ R_p(x'_1, \theta_1) & R_p(x'_1, \theta_1) & \dots & R_p(x'_1, \theta_n) \end{bmatrix}$

$$R_{p}(x',\theta) = \begin{bmatrix} R_{p}(x'_{1},\theta_{1}) & R_{p}(x'_{1},\theta_{2}) & \dots & R_{p}(x'_{1},\theta_{n}) \\ R_{p}(x'_{2},\theta_{1}) & R_{p}(x'_{2},\theta_{2}) & \dots & R_{p}(x'_{2},\theta_{n}) \\ \vdots & \vdots & \ddots & \vdots \\ R_{p}(x'_{m},\theta_{1}) & R_{p}(x'_{m},\theta_{2}) & \dots & R_{p}(x'_{m},\theta_{n}) \end{bmatrix}$$







Sound field visualization









x'[m]



Sound field visualization





Measured Radon transform



x'[m]



Tomography vs Microphone array

Tomographic reconstruction

Microphone array







- Spatial res.: 2 cm
- Angular res.: 10°
- Planar array of 60 microphones
- Spatial resolution: 7.5 cm



Tomography vs Microphone array

Tomographic reconstruction









- Spatial res.: 2 cm
- Angular res.: 10°
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- Spatial resolution: 7.5 cm





Application 2: Beamforming





Conventional beamforming



	Region	Key feature		
techniques	Farfield	Phase		
	Nearfield	Phase and amplitude		



Conventional beamforming



Example: Delay and Sum Beamforming (DSB)





More advanced beamforming techniques

DTU

- To improve the beamforming output:
 - Design an optimum array layout/geometry
 - Optimize weighting coefficients (w_m)



- What do these techniques improve?
 - Resolution
 - Maximum sidelobe level (MSL)
 - Frequency range of analysis, etc.





Spatial aliasing



 Beamforming techniques are based on a finite number of input signals
 This inevitably causes spatial aliasing!

> E.g. DSB when $\theta = 0$

$$b_{DS}(0) = \left| \frac{1}{M} \sum_{m=0}^{M-1} \tilde{p}_m e^{-jkmd\sin(0)} \right|^2 \\ = \left| \frac{1}{M} \sum_{m=0}^{M-1} \tilde{p}_m \right|^2$$





Spatial aliasing



 Beamforming techniques are based on a finite number of input signals
 This inevitably causes spatial aliasing!



• Theoretical solution: Use an infinite number of transducers ($d \rightarrow 0$)

$$\lim_{M \to \infty} \sum_{m=0}^{M-1} \tilde{p}_m d = \int_0^{L_0} P(x, y, \omega) \mathrm{d}l \quad \stackrel{?}{\longleftrightarrow} \quad v_{LDV}(t) = \frac{n_0 - 1}{\gamma p_0 n_0} \frac{\mathrm{d}}{\mathrm{d}t} \left(\int_L p(x, y, t) \mathrm{d}l \right)$$



Spatial aliasing



- Beamforming techniques are based on a finite number of input signals
 This inevitably causes spatial aliasing!
- 90 $0 \, dB$ \triangleright E.g. DSB when $\theta = 0$ 5 60 -1030 - 15 20 - 25 $= \left| \frac{1}{M} \sum_{m=0}^{M-1} \tilde{p}_m \right|^2$ - 30 -60- 35 -9040 5 10 15 20 Frequency [kHz]
- Theoretical solution: Use an infinite number of transducers ($d \rightarrow 0$)

$$\lim_{M \to \infty} \sum_{m=0}^{M-1} \tilde{p}_m d = \int_0^{L_0} P(x, y, \omega) dl \quad \longleftrightarrow \quad V_{LDV}(\omega) = j\omega \frac{n_0 - 1}{\gamma p_0 n_0} \left(\int_{\mathbf{L}} P(x, y, \omega) dl \right)$$







$$V_{LDV}(\omega) = j\omega \frac{n_0 - 1}{\gamma p_0 n_0} \left(\int_{\mathbf{L}} P(x, y, \omega) dl \right) \implies b_{AO} = \left| \frac{1}{L_0} \int_0^L P(x, y, \omega) dl \right|^2$$
$$= \left| \frac{1}{L_0} \frac{\gamma p_0 n_0}{n_0 - 1} \frac{V_{LDV}(\omega)}{j\omega} \right|^2$$

DTU

Acousto-optic beamformer

















Thanks for your attention!





Measuring the acousto-optic effect







