

DEFINING THE SI SECOND VIA OPTION 2: CHALLENGES AND OPPORTUNITIES

Jérôme Lodewyck, Tetsuya Ido

INTRODUCTION

OPTION 2: DEFINING THE SECOND WITH MULTIPLE TRANSITIONS

1 **Definition** based on weights w_i

- N : normalisation constant for continuity
- N and w_i univocally fix the definition
- (1 relation) + ($n - 1$ independent ratios) $\equiv n$ frequencies

$$\prod_{k=1}^n \nu_k^{w_k} \equiv N \text{ Hz}$$

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2 **Realization** using “recommended frequencies” N_i :

- calculable from the global fit of frequency ratios $\rho_{i,j}$
- initially independent of the choice of weights

$$N_i = N \prod_{k=1}^n \rho_{i,k}^{w_k}$$

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$$\prod_{k=1}^n N_k^{w_k} = N, \quad \forall \rho_{i,j}.$$

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- uncertainty on the recommended frequency δN_i
(akin uncertainty on SRS)

$$N_i = N \prod_{k=1}^n \rho_{i,k}^{w_k}$$

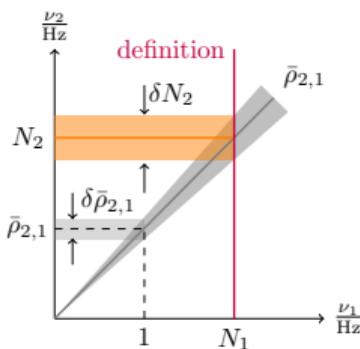
$$\prod_{k=1}^n N_k^{w_k} = N, \quad \forall \rho_{i,j}.$$

$$\frac{\nu_i}{\text{Hz}} = N_i \pm \delta N_i$$

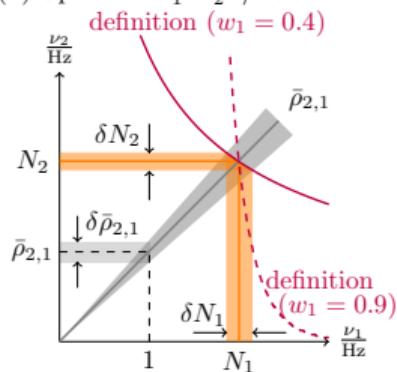
UNDERSTANDING OPTION 2: GRAPHICAL REPRESENTATION

Realizing the unit

(a) Option 1: ν_1/Hz fixed



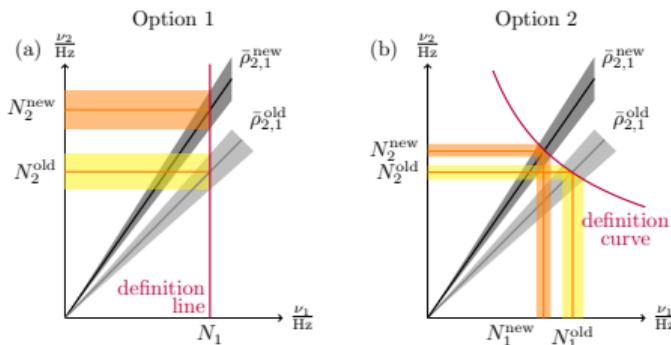
(b) Option 2: $\nu_1^{w_1} \nu_2^{w_2}/\text{Hz}$ fixed



- The definition is represented by an exactly known curve in the $\{\nu_i/\text{Hz}\}$ space:
 - Straight line for option 1
 - Curve with finite slope for option 2
- Frequency ratios are represented by a slope with an uncertainty
- Recommended frequencies N_i for the realization are at the intersection point
- Option 2 “balances” the uncertainty on N_i over all transitions.

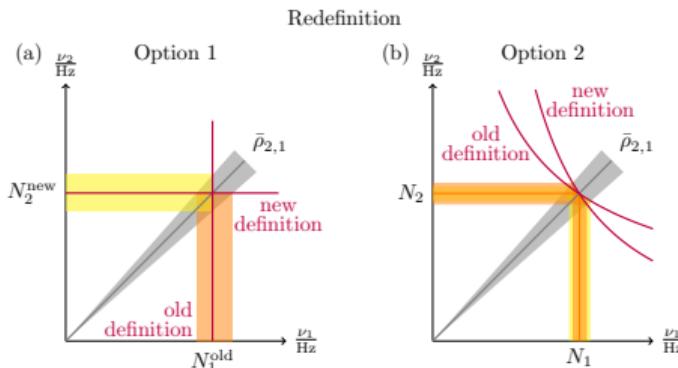
UNDERSTANDING OPTION 2: GRAPHICAL REPRESENTATION

Update of frequency ratios



UPDATE OF FREQUENCY RATIOS

- The definition is constant
- New recommended frequencies at the intersection of new frequency ratios and the definition



FUTURE REDEFINITIONS

- Recommended frequencies are constant
- The definition pivots around the intersection
- “Option 2b”: the weights could be updated on a regular basis directly by the CIPM to follow the progress in optical frequency standards

CHOICE OF WEIGHTS

UNCERTAINTY ON RECOMMENDED FREQUENCIES

- Option 1: $\delta N_{i_0} = 0$ for PFS, while $\delta N_i^2 \simeq u_i^2 + u_{i_0}^2$ for SRS
- Option 2: balance δN_i over all transitions

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CHOICE OF WEIGHTS

- $\frac{\delta N_i}{N_i}$ small compared to the clock uncertainty u_i for all i .
- $\Rightarrow w_i \propto \frac{1}{u_i^2}$: *most precise clocks must have a larger weights*

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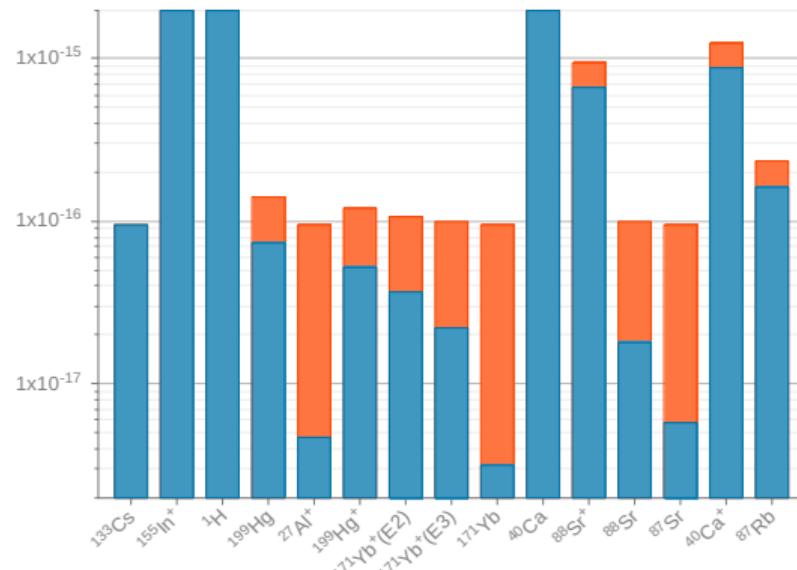
DERIVING u_i

- Least squares over residues: $s_{j,k} = \frac{u_j^2 + u_k^2}{u_{j,k}^2} - 1$, with $u_{j,k}$ coming from the global fit.
- Uncertainties representative of clocks involved in frequency ratio measurements
- Need at least two connections.

EXAMPLE: 2021 CIPM FIT OF FREQ. RATIOS

Uncertainties ($/10^{-18}$) in the **realization** of the unit → For the **current SI second** (^{133}Cs)

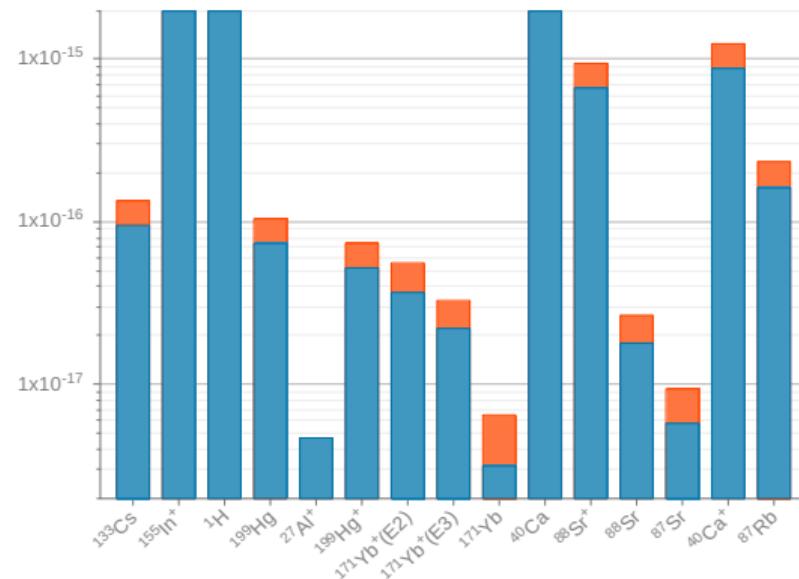
Species	u_i	N_i	$\delta N_i / N_i$
^{133}Cs	95	9192631770.000000	0
$^{155}\text{In}^+$	2161	1267402452901041.283	2163
^1H	3001	1233030706593513.654	3000
^{199}Hg	74	1128575290808154.319	121
$^{27}\text{Al}^+$	4.7	1121015393207859.159	96
$^{199}\text{Hg}^+$	53	1064721609899146.964	109
$^{171}\text{Yb}^+ \text{E2}$	37	688358979309308.239	102
$^{171}\text{Yb}^+ \text{E3}$	22	642121496772645.119	97
^{171}Yb	3.2	518295836590863.630	96
^{40}Ca	6276	455986240494138.191	6276
$^{88}\text{Sr}^+$	669	444779044095486.342	667
^{88}Sr	18	429228066418007.006	98
^{87}Sr	5.8	429228004229872.992	96
$^{40}\text{Ca}^+$	884	411042129776400.360	885
^{87}Rb	163	6834682610.9043126	172



EXAMPLE: 2021 CIPM FIT OF FREQ. RATIOS

Uncertainties ($/10^{-18}$) in the **realization** of the unit → For **option 1** with $^{27}\text{Al}^+$

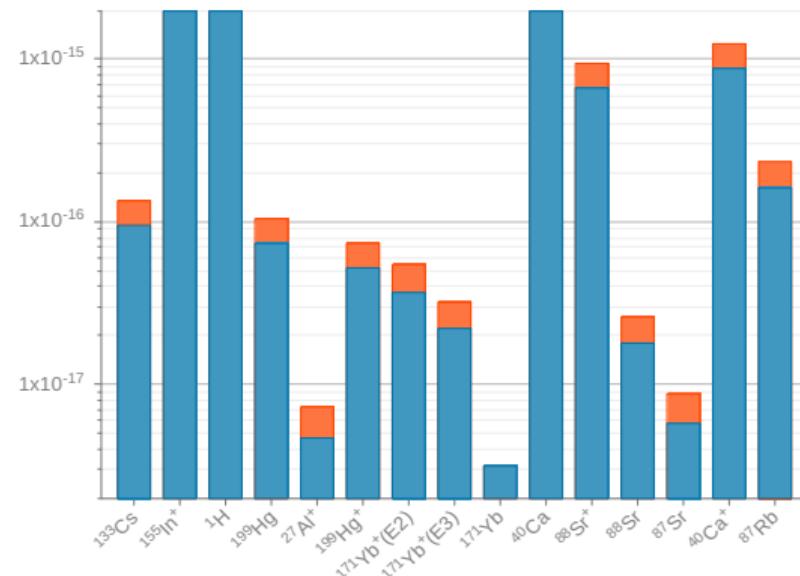
Species	u_i	N_i	$\delta N_i / N_i$
^{133}Cs	95	9192631770.000000	96
$^{155}\text{In}^+$	2161	1267402452901041.283	2162
^1H	3001	1233030706593513.654	3002
^{199}Hg	74	1128575290808154.319	74
$^{27}\text{Al}^+$	4.7	1121015393207859.159	0
$^{199}\text{Hg}^+$	53	1064721609899146.964	52
$^{171}\text{Yb}^+ \text{E2}$	37	688358979309308.239	42
$^{171}\text{Yb}^+ \text{E3}$	22	642121496772645.119	24
^{171}Yb	3.2	518295836590863.630	5.6
^{40}Ca	6276	455986240494138.191	6277
$^{88}\text{Sr}^+$	669	444779044095486.342	672
^{88}Sr	18	429228066418007.006	19
^{87}Sr	5.8	429228004229872.992	7.5
$^{40}\text{Ca}^+$	884	411042129776400.360	885
^{87}Rb	163	6834682610.9043126	166



EXAMPLE: 2021 CIPM FIT OF FREQ. RATIOS

Uncertainties ($/10^{-18}$) in the **realization** of the unit \rightarrow For option 1 with ^{171}Yb

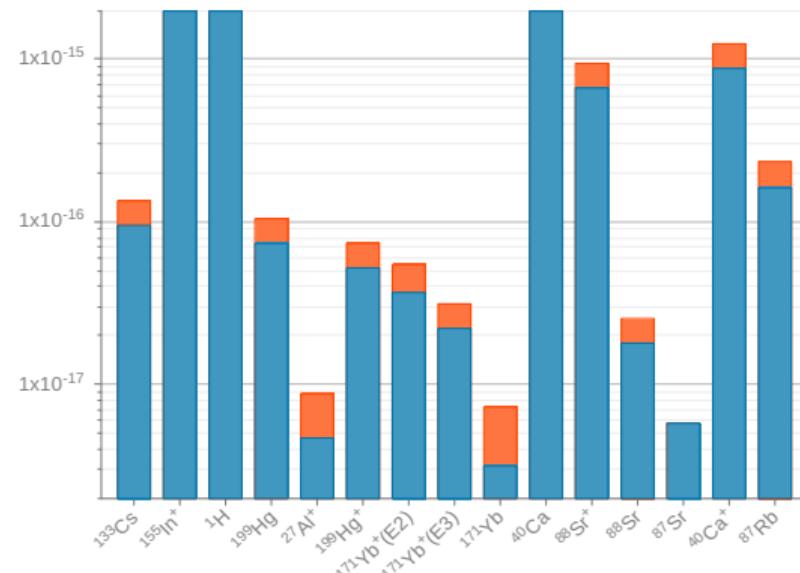
Species	u_i	N_i	$\delta N_i / N_i$
^{133}Cs	95	9192631770.000000	96
$^{155}\text{In}^+$	2161	1267402452901041.283	2162
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^{199}Hg	74	1128575290808154.319	74
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$^{199}\text{Hg}^+$	53	1064721609899146.964	52
$^{171}\text{Yb}^+ \text{E2}$	37	688358979309308.239	41
$^{171}\text{Yb}^+ \text{E3}$	22	642121496772645.119	24
^{171}Yb	3.2	518295836590863.630	0
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EXAMPLE: 2021 CIPM FIT OF FREQ. RATIOS

Uncertainties ($/10^{-18}$) in the **realization** of the unit → For **option 1** with ^{87}Sr

Species	u_i	N_i	$\delta N_i / N_i$
^{133}Cs	95	9192631770.000000	96
$^{155}\text{In}^+$	2161	1267402452901041.283	2162
^1H	3001	1233030706593513.654	3002
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$^{88}\text{Sr}^+$	669	444779044095486.342	672
^{88}Sr	18	429228066418007.006	18
^{87}Sr	5.8	429228004229872.992	0
$^{40}\text{Ca}^+$	884	411042129776400.360	885
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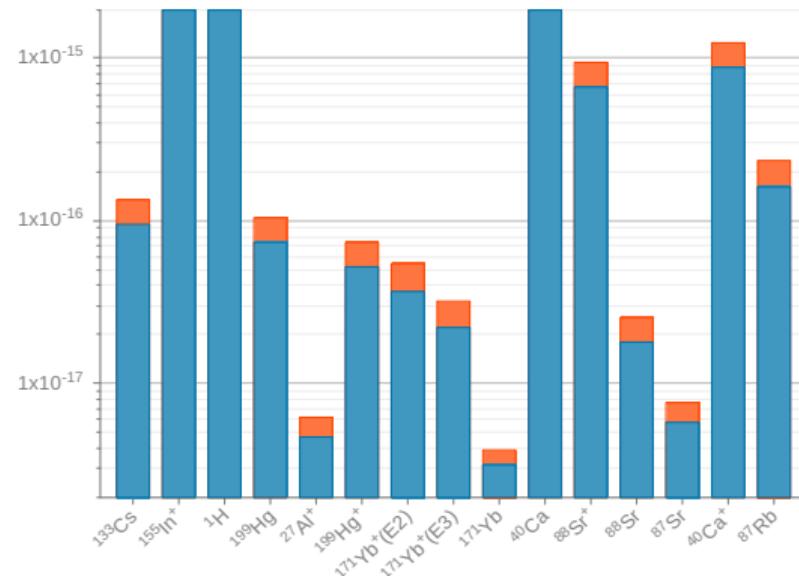


EXAMPLE: 2021 CIPM FIT OF FREQ. RATIOS

Uncertainties ($/10^{-18}$) in the **realization** of the unit

→ For option 2

Species	u_i	N_i	w_i	$\delta N_i / N_i$
^{133}Cs	95	9192631770.000000	0.001	96
$^{155}\text{In}^+$	2161	1267402452901041.283	0.000	2162
^1H	3001	1233030706593513.654	0.000	3002
^{199}Hg	74	1128575290808154.319	0.001	74
$^{27}\text{Al}^+$	4.7	1121015393207859.159	0.249	4.1
$^{199}\text{Hg}^+$	53	1064721609899146.964	0.002	52
$^{171}\text{Yb}^+ \text{E2}$	37	688358979309308.239	0.004	41
$^{171}\text{Yb}^+ \text{E3}$	22	642121496772645.119	0.011	23
^{171}Yb	3.2	518295836590863.630	0.549	2.2
^{40}Ca	6276	455986240494138.191	0.000	6277
$^{88}\text{Sr}^+$	669	444779044095486.342	0.000	672
^{88}Sr	18	429228066418007.006	0.017	18
^{87}Sr	5.8	429228004229872.992	0.166	5.1
$^{40}\text{Ca}^+$	884	411042129776400.360	0.000	885
^{87}Rb	163	6834682610.9043126	0.000	166

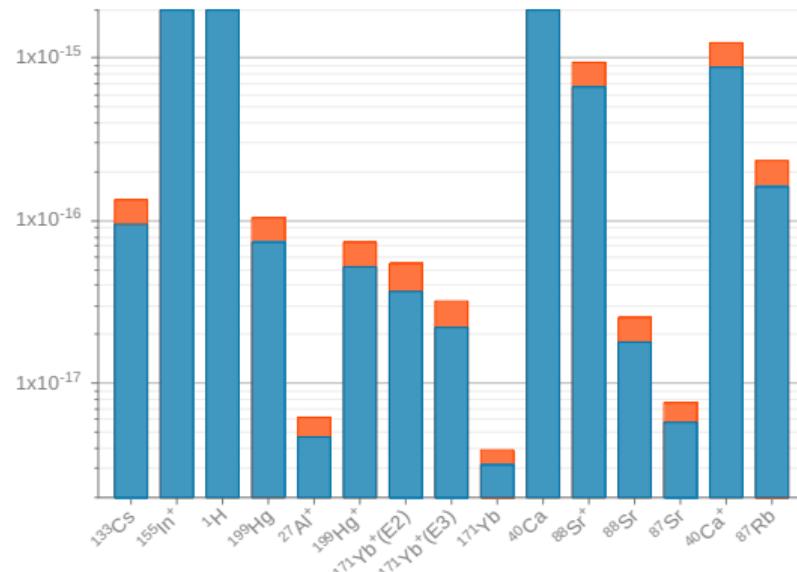


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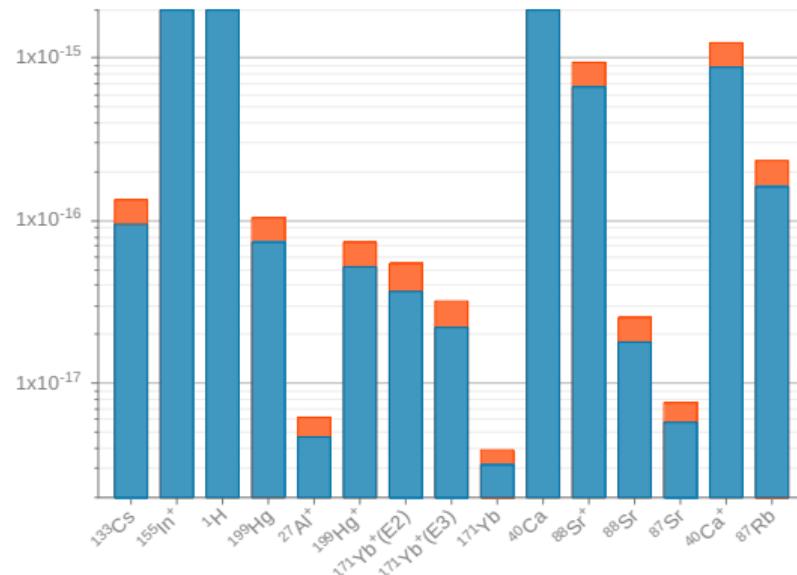
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Combined ^{87}Sr and $^{27}\text{Al}^+$				2.7
Combined ^{171}Yb and $^{27}\text{Al}^+$				1.4
Combined ^{87}Sr and ^{171}Yb				1.5
Combined ^{87}Sr , ^{171}Yb , and $^{27}\text{Al}^+$				0.5



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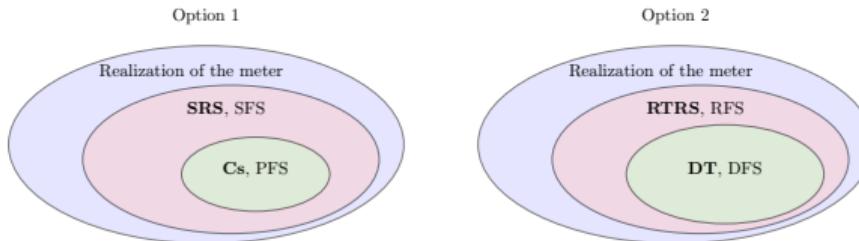
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- 2021: ^{87}Sr , ^{171}Yb , $^{27}\text{Al}^+$, (^{88}Sr , $^{171}\text{Yb}^+$)
- 2025: significant contributions of $^{171}\text{Yb}^+$, $^{88}\text{Sr}^+$, $^{155}\text{In}^+$

TERMINOLOGY

TRANSLATING THE CONCEPTS OF PRIMARY AND SECONDARY FREQUENCY STANDARDS



3 CATEGORIES OF FREQUENCY STANDARDS

Option 1

- Transitions for the realization of the meter
 - Secondary Representations of the Second
 - Cs transition / transition "x"
- =
- =
- <

Option 2

- Transitions for the realization of the meter
- Recommended Transitions for the Realization of the Second
- Defining transitions

PROS & CONS

PROS

- **Easier consensus:** balanced weights, chosen with quantitative criteria
- **Promoting variety of frequency standards:** encourage improvement of various FS and freq. ratios vs. focus of resources on a single species.
- **Ready to be implemented:** relies on the global fit of frequency ratios
- **Mitigate risks:** mistakes and obsolescence of FS have less impact on the realization uncertainty, albeit more likely to occur.
option 2: higher probability and low impact vs option1: lower probability and high impact
- **(Option 2b) Adapt to the evolution of optical frequency standards:** weights are updated based on a quantitative indicator.

PROS & CONS

CONS (AND ANSWERS!)

- **Added realization uncertainty with the PFS of option 1 alone** ; but:
 - $\delta N_i / N_i < u_i$, and improving with new freq. ratio measurements.
 - Lower realization uncertainty than option 1 for SRS, and combinations thereof (e.g. TAI)
 - N ; derived from redundant freq. ratio measurements.
- **Industrial need** ; but: performance/market driven, current development of Rb, optical clocks, independent of the definition.
- **Difficult to explain** ; but: concept of average (without maths) easy to understand.
- **Physical interpretation of N** ; but the value of N is an historical accident
- **(Option 2b) Different from the current formulation of the definitions of units**

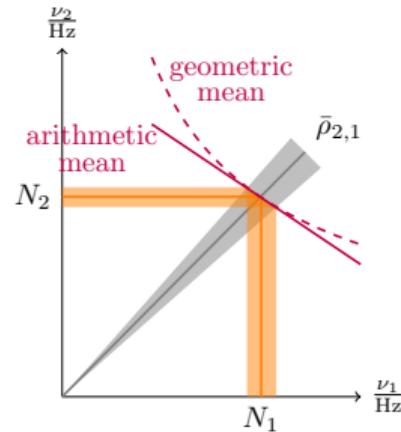
ALTERNATIVES FORMULATIONS

OTHER MEANS

- Arithmetic mean (C. Calosso, N. Nemitz)
- Harmonic mean (U. Sterr)

All these means are practically equivalent, but:

- The geometric mean is formally the “right” choice
- Other means can be more understandable



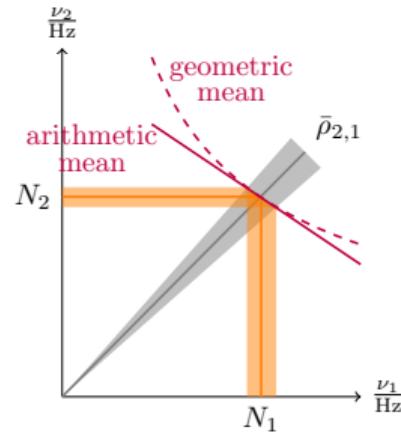
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CONTINUITY CONSTANT N

$$\prod_{k=1}^n N_k^{w_k} = N$$

$$\forall \rho_{i,j}$$

- Replacing N with $\{N_i\}$ would give physical significance to the continuity constant (C. Calosso, N. Nemitz)
- But hide the fact that continuity implies one degree of freedom, and may bring confusion as the N_i vary.

CONCLUSION

OPTION 2:

- Definition involves several transitions based on their performances.
- Realization based on recommended frequencies (\Leftrightarrow current SRS)
- Fair balancing of uncertainties over all transitions
- Readily implementable with current tools (fit of frequency ratios, steering of TAI, ...)

REFERENCES

- *On a definition of the SI second with a set of optical clock transitions* Jérôme Lodewyck, Metrologia **56** 055009 (2019)
- *A definition of the SI second based on several optical transitions* Jérôme Lodewyck, J. Phys.: Conf. Ser. **2889** 012026 (2024)
- *Properties of a definition of the SI second based on several optical transitions* Jérôme Lodewyck, and Tetsuya Ido arXiv:2503.13278
- *An Accessible Formulation for Defining the SI Second Based on Multiple Atomic Transitions* Claudio Calosso, Nils Nemitz arXiv:2503.01778