Bilateral Comparison of 1.018 V and 10 V Standards between the SMU, Slovakia and the BIPM, April 2001

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A comparison of the 1.018 V and 10 V voltage reference standards of the BIPM and the Slovak Institute of Metrology (SMU, Bratislava, Slovakia) was carried out in April 2001. Two BIPM 732B Zener diode-based travelling standards, BIPM6 and BIPM7, were transported by freight to the Bundesamt für Eich- und Vermessungswesen (BEV Vienna, Austria) and then taken by car to the SMU. The BIPM measurements were carried out at 1.018 V and 10 V using the Josephson array voltage standard (JAVS) of the laboratory. The results of all measurements were corrected for the dependence of the output voltage on ambient temperature and pressure.

Figure 1 and 2 show the measured values obtained for the two standards by the two laboratories. The values and uncertainties were calculated for the reference date from linear least-squares fits.

Table 1 lists the results of the 1.018 V comparison and the contributions to the uncertainty budget. Experience has shown that flicker or 1/f noise dominates the stability characteristics of Zener-diode standards and it is not appropriate to use the standard deviation of the mean to characterize the dispersion of the measured values. For the present standards, the relative value of the flicker floor voltage is about 1 part in 10^8 .

Table 2 lists the same information for the 10 V comparison.

In estimating the uncertainty we calculated the *a priori* uncertainty based on all known sources except that associated with the stability of the standards when transported, and compared this with the *a posteriori* uncertainty estimated by the standard deviation of the mean of the results from the two travelling standards. With only two travelling standards, the uncertainty of the standard deviation of the mean is comparable to the value of the standard deviation of the mean itself. If the *a posteriori* uncertainty is significantly different from the *a priori* uncertainty, we assume that a standard has changed in an unusual way and we used the larger of these two estimates in calculating the final uncertainty.

In Table 1 and 2, the following elements are listed:

- (1) the predicted value U_{Z_SMU} of each Zener, computed using a linear least squares fit to all of the data from the SMU and referenced to the mean date of the SMU's measurements;
- (2) the Type A uncertainty arising from instability of the Zener, computed as the standard uncertainty of the predicted value from the linear drift model, or an estimate of the 1/f noise voltage level;
- (3) the uncertainty component arising from the measuring equipment of the SMU. This uncertainty is completely correlated between the different Zeners used for a comparison;
- (4-6) the corresponding quantities for the BIPM;
- (7) the uncertainty due to the combined effects of the uncertainties of the pressure and temperature coefficients and to the difference of the mean pressures and temperatures in the participating laboratories; although the same equipment is used to measure the coefficients for all Zeners, the uncertainty is dominated by the Type A uncertainty of each Zener, so that the final uncertainty can be considered as uncorrelated among the different Zeners used in a comparison;
- (8) the difference $(U_{Z_SMU} U_{Z_BIPM})$ for each Zener, and
- (9) the uncorrelated part of the uncertainty;
- (10) the result of the comparison, which is the mean of the differences of the calibration results for the different standards;

the uncertainty of the transfer, estimated by two methods;

- (11) the *a priori* uncertainty, which is the standard deviation of the mean value of the results from the different Zeners, counting only the uncorrelated uncertainties of the individual results;
- (12) the *a posteriori* uncertainty, which is the standard deviation of the mean of the different results;
- (13) the correlated part of the uncertainty;
- and
- (14) the total uncertainty of the comparison, which is the root-sum-square of the correlated part of the uncertainty and of the larger of (11) and (12).

Table 3 and 4 summarize the uncertainties due to the measuring equipment of the SMU and of the BIPM, respectively.

The final result of the comparison is presented as the differences between the values assigned to a 1.018 V and a 10 V standard by each laboratory. The difference between the value assigned by the SMU at the SMU, U_{SMU} , and that assigned by the BIPM at the BIPM, U_{BIPM} , for a 1.018 V standard on the reference date is

$$U_{\text{SMU}(1.018 \text{ V})} - U_{\text{BIPM}(1.018 \text{ V})} = -0.091 \text{ }\mu\text{V}; u_{\text{c}} = 0.042 \text{ }\mu\text{V} \text{ on } 2001/04/13,$$

where u_c is the combined standard uncertainty,

and for a 10 V standard on the reference date is

$$U_{\text{SMU}(10 \text{ V})} - U_{\text{BIPM}(10 \text{ V})} = -0.04 \text{ }\mu\text{V}; u_{\text{c}} = 0.86 \text{ }\mu\text{V} \text{ on } 2001/04/12,$$

The difference between the values assigned to the travelling standards at 1.018 V by the two laboratories approaches the expanded uncertainty of the comparison at the 95% confidence level.

The combined uncertainties at 10 V is mainly due to the difference between the results obtained on the two Zeners. The mean difference is quite the same as that measured in May 1999 during on-site comparisons of measurements of 10 V Zeners.



Figure 1. Voltage of BIPM6 as a function of time, with linear least-squares fit to the BIPM measurements



Figure 2. Voltage of BIPM7 as a function of time, with linear least-squares fits to the BIPM measurements

Table 1. Results of the SMU(Slovakia)/BIPM bilateral comparison of 1.0180 V standards using two Zener travelling standards: reference date 13 April 2001. Uncertainties are 1 σ estimates. The uncorrelated uncertainty is $w = [r^2 + t^2 + v^2]^{1/2}$, the expected transfer uncertainty is $x = [w_6^2 + w_7^2]^{1/2}/2$ and the correlated uncertainty is $y = [s^2 + u^2]^{1/2}$.

PM/
4.083
046 r
S
4.209
010 <i>t</i>
u
008 v
.127
048 w
x
<i>y</i>

Table 2. Results of the SMU(Slovakia)/BIPM bilateral comparison of 10 V standards using two Zener travelling standards: reference date 12 April 2001. Uncertainties are 1 σ estimates. The uncorrelated uncertainty is $w = [r^2 + t^2 + v^2]^{1/2}$, the expected transfer uncertainty is $x = [w_6^2 + w_7^2]^{1/2}/2$ and the correlated uncertainty is $y = [s^2 + u^2]^{1/2}$.

			BIPM6	BIPM7	
1	SMU	$(U_{\rm Z_SMU} - 10 \text{ V})/\mu \text{V}$	-2.84	-20.21	
2		Type A uncertainty/µV	0.11	0.10	r
3		equipment uncertainty/µV	0.	03	s
4	BIPM	$(U_{\rm Z BIPM} - 10 \text{ V})/\mu\text{V}$	-3.84	-19.31	
5		Type A uncertainty/µV	0.11	0.10	t
6	6	equipment uncertainty/µV	0.	01	и
7	pressure ar	nd temperature	0.07	0.06	v
	c	orrections uncertainty/µV			
8		$(U_{\text{Z}_{\text{SMU}}} - U_{\text{Z}_{\text{BIPM}}})/\mu\text{V}$	0.82	-0.90	
9	un	correlated uncertainty/µV	0.17	0.15	w
10		$< U_{\rm SMU} - U_{\rm BIPM} > /\mu V$	-0	.04	
11	expecte	ed transfer uncertainty/µV	0	.11	x
12	$s_{\rm M}$ of diff	erence for two Zeners/ μV	0	.86	
13		correlated uncertainty/µV	0	.03	У
14	compa	rison total uncertainty/µV	0	.86	

Table 3: estimated standard uncertainties for Zener calibrations with the SMU equipment.

	Uncertainty/nV	
	1.018 V	10 V
thermistor measurement	1.0	3
pressure measurement	2.5	25
thermal electromotive forces	17	17
detector/EMI	10	10
leakage resistance	0.1	1
frequency	0.2	2
total	19.9	30

Table 4: estimated standard uncertainties for Zener calibrations with the BIPM equipment.

	Uncertainty/nV	
	1.018 V	10 V
thermistor measurement	1.3	4
pressure measurement	0.4	4
thermal electromotive forces	3.0	3
detector/EMI	3.0	1
leakage resistance	3.0	0
frequency	0.0	0
total	5.4	6