

Comb generation for metrology

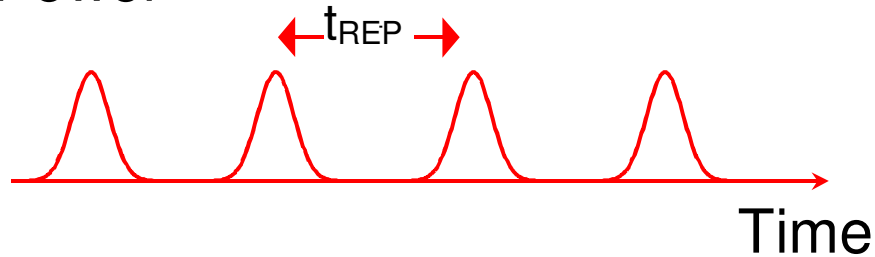
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- Femtocombs in frequency metrology
- Possible noise contributions and countermeasures
- Supercontinuum generation
- Outlook

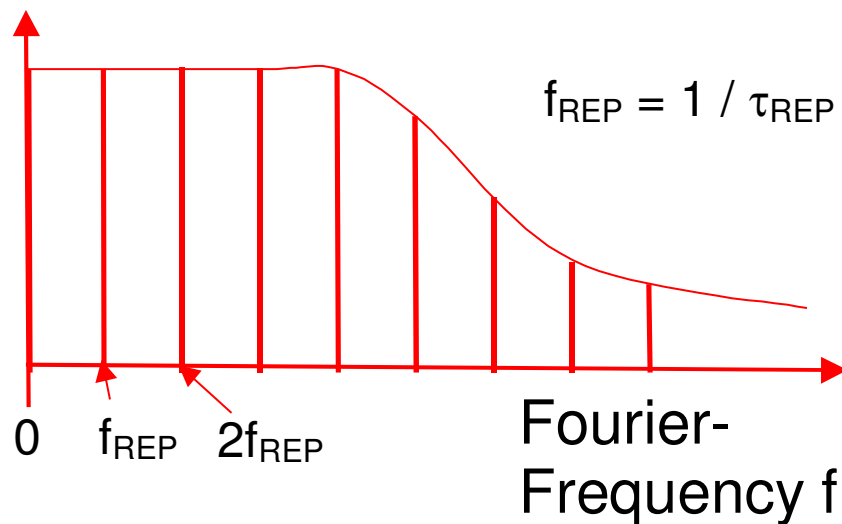
Periodic train of light pulses, e. g. from a LED

Power



Time domain

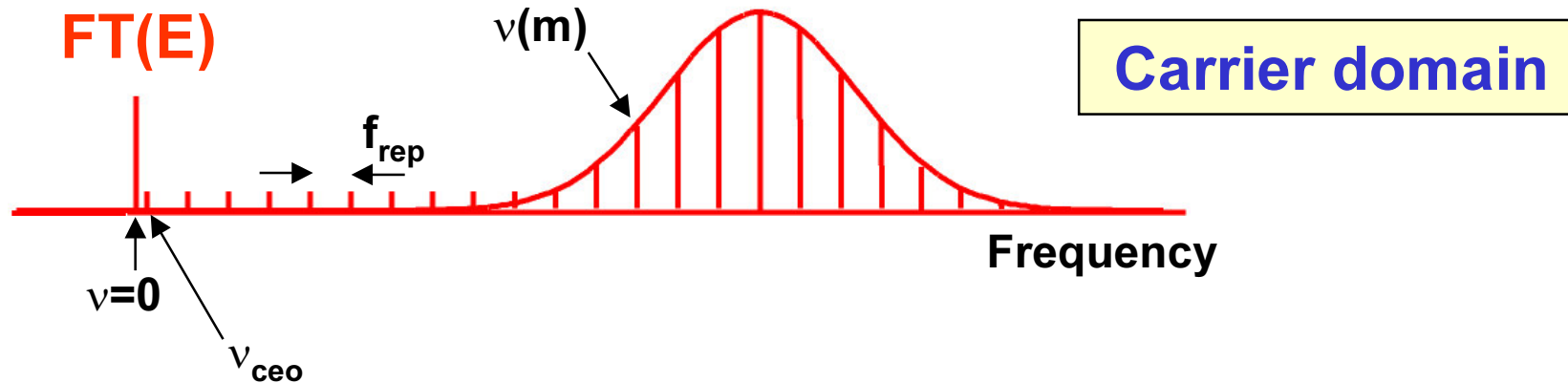
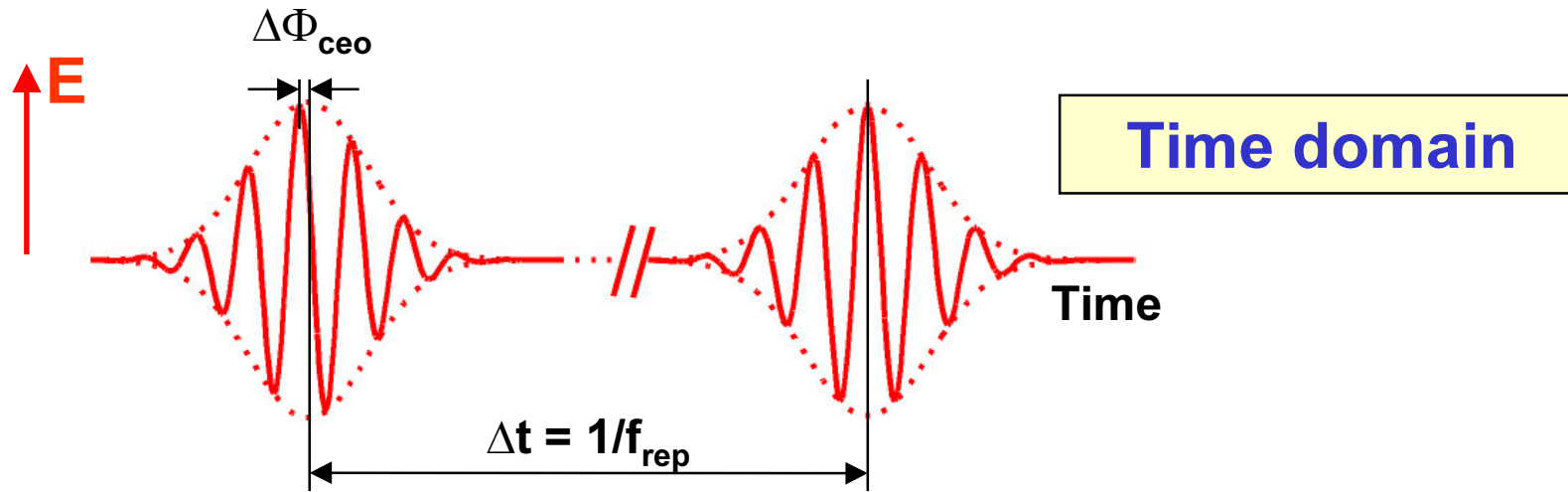
FT (Power)



Baseband domain

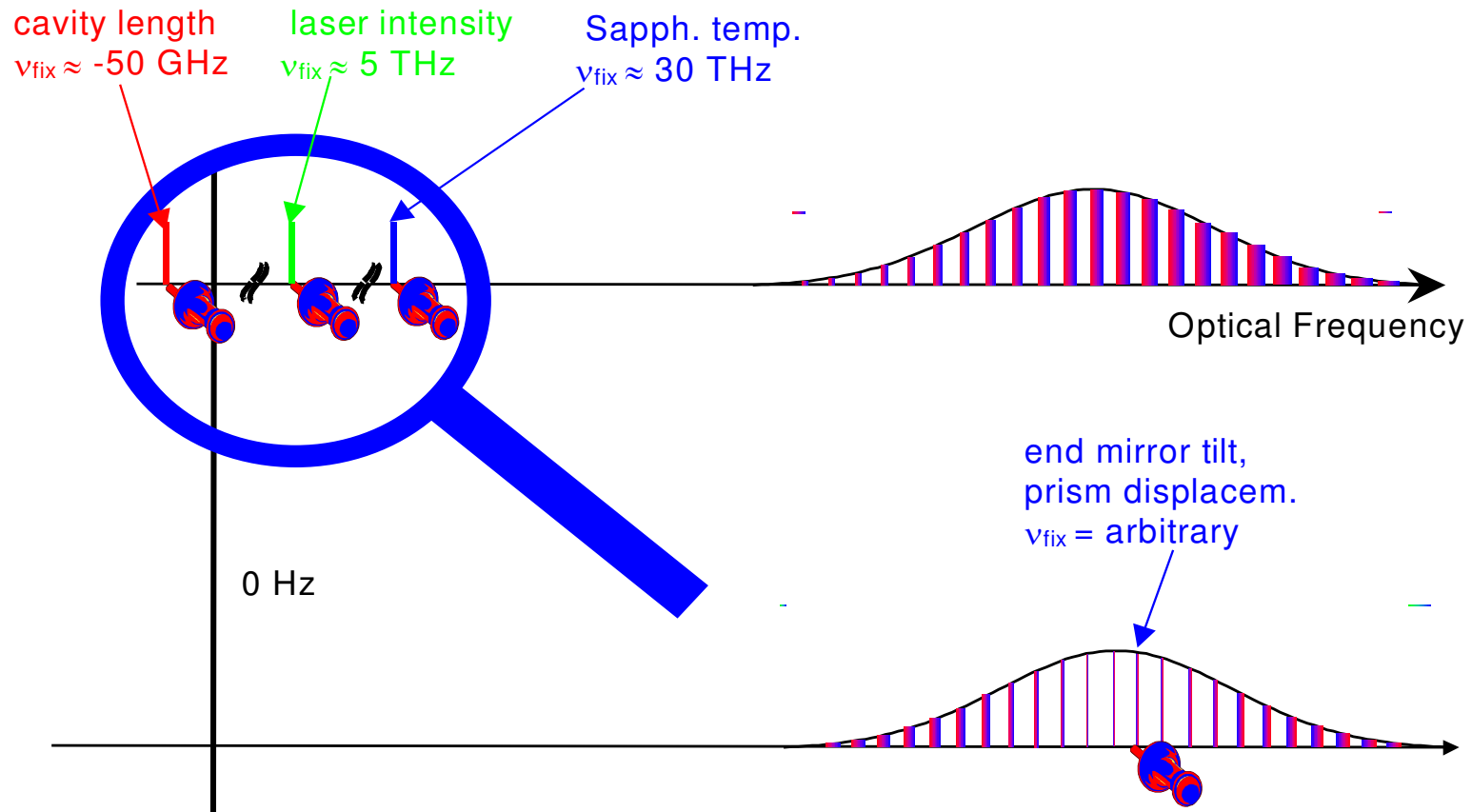
In general no comb spectrum in carrier domain !

Periodic train of light pulses with coherent carrier

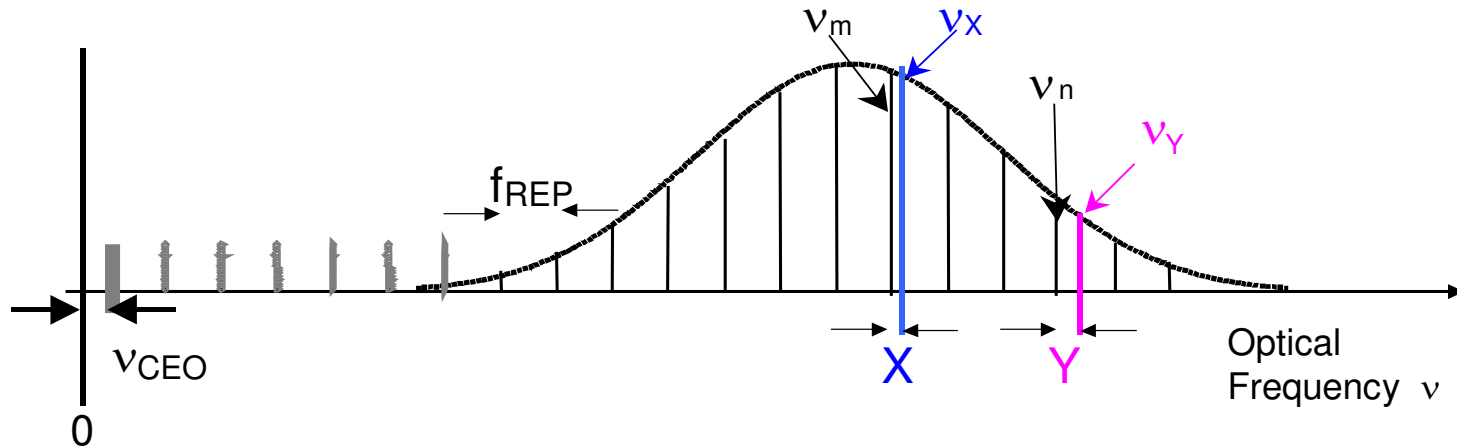


$$\nu(m) = \nu_{\text{ceo}} + m f_{\text{rep}}, \quad \text{Elastic tape picture}$$

Fixed point of 'elastic tape'

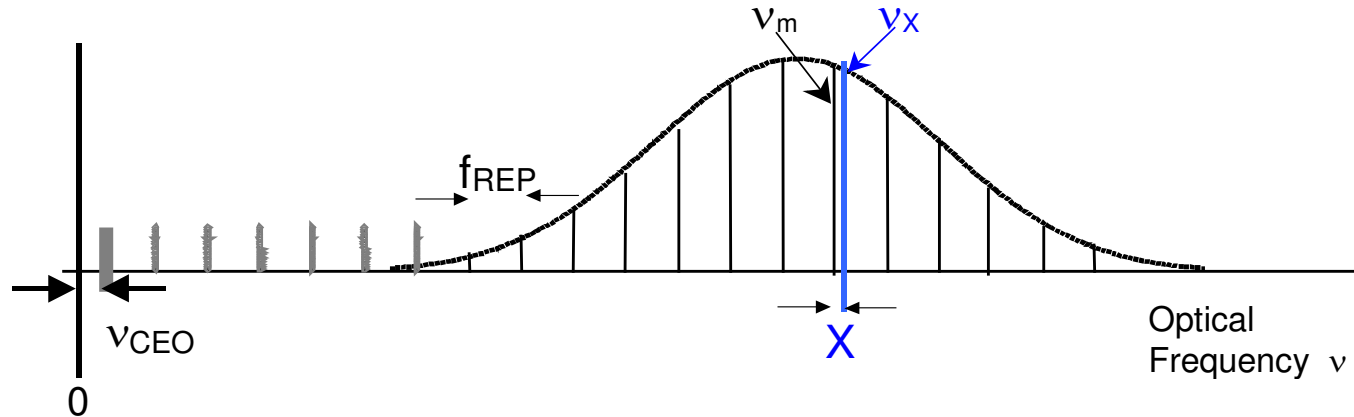


Applications of Femtocombs in Frequency Metrology



Task	Detection of	Applications
Link the difference of 2 optical frequencies to MW	beat-note X beat-note Y f_{REP}	MW generation IR-metrology IR-synthesis
Link 1 optical frequency to MW	CEO-frequency beat-note X f_{REP}	absolute frequency measurement optical frequency synthesis MW generation
Link 2 optical frequencies	CEO-frequency beat-note X beat-note Y	optical frequency ratios optical frequency synthesis

Phase-coherent measurement: detection of phase angles



$$\nu_X = \nu_m + X = \nu_{\text{ceo}} + m f_{\text{rep}} + X$$

Assumption: $\varphi_m(\mathbf{t}) = \varphi_{\text{ceo}}(\mathbf{t}) + m \varphi_{\text{rep}}(\mathbf{t}) + \Phi(\mathbf{t}, m)$

Elastic tape picture holds even for phases, $\Phi(\mathbf{t}, m) < \infty$

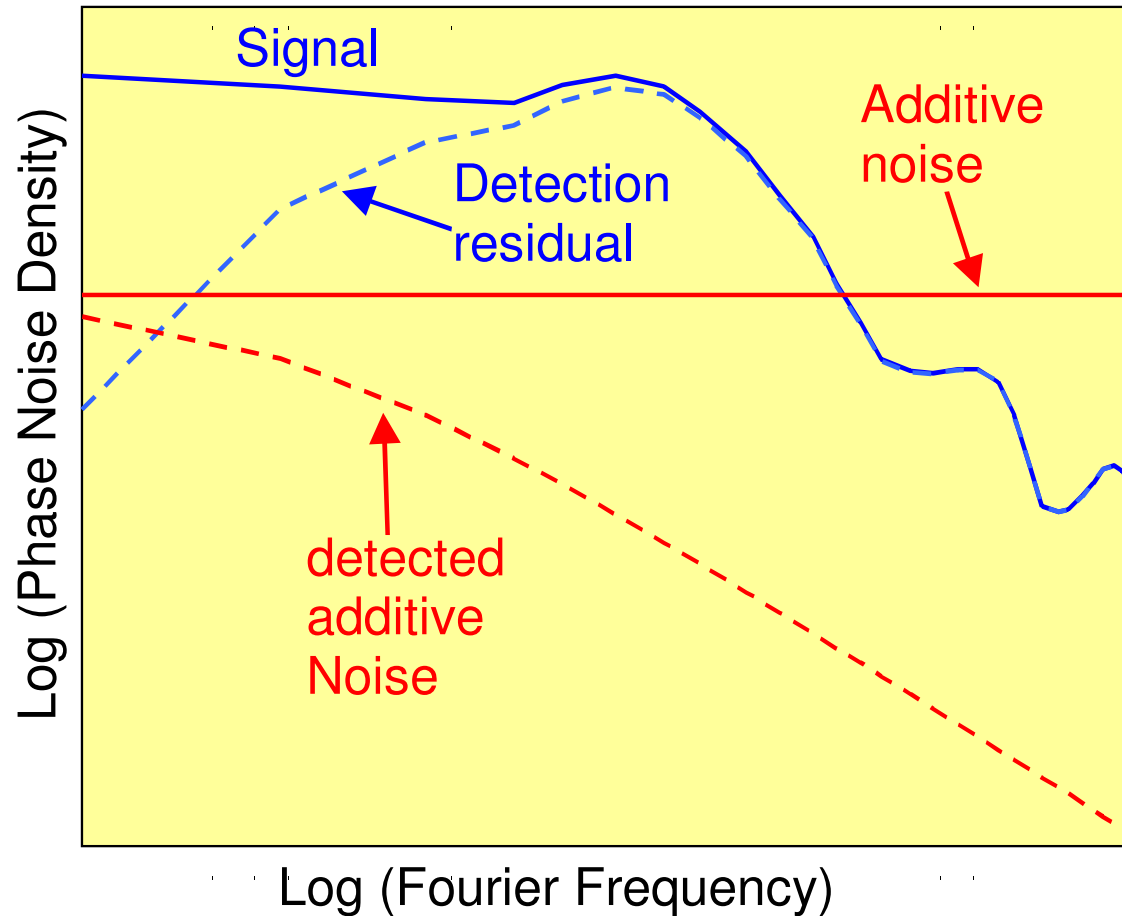
⇒ Detection of $\varphi_m(\mathbf{t})$, $\varphi_{\text{CEO}}(\mathbf{t})$, $\varphi_{\text{REP}}(\mathbf{t})$

Detection of φ_m , φ_{CEO} , φ_{REP}

Possible noise contributions

- optimum bandwidth \Rightarrow detection residual
- additive noise, e. g. electronic noise, shot noise
- noise cross conversion, e.g. AM \rightarrow PM
- external multiplicative noise, e. g. thermal delay time noise

Noise contributions (schematic)



Signal \equiv fluctuations of references and femtocomb !

Detection of φ_m , φ_{CEO} , φ_{REP}

Possible noise contributions

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Data processing

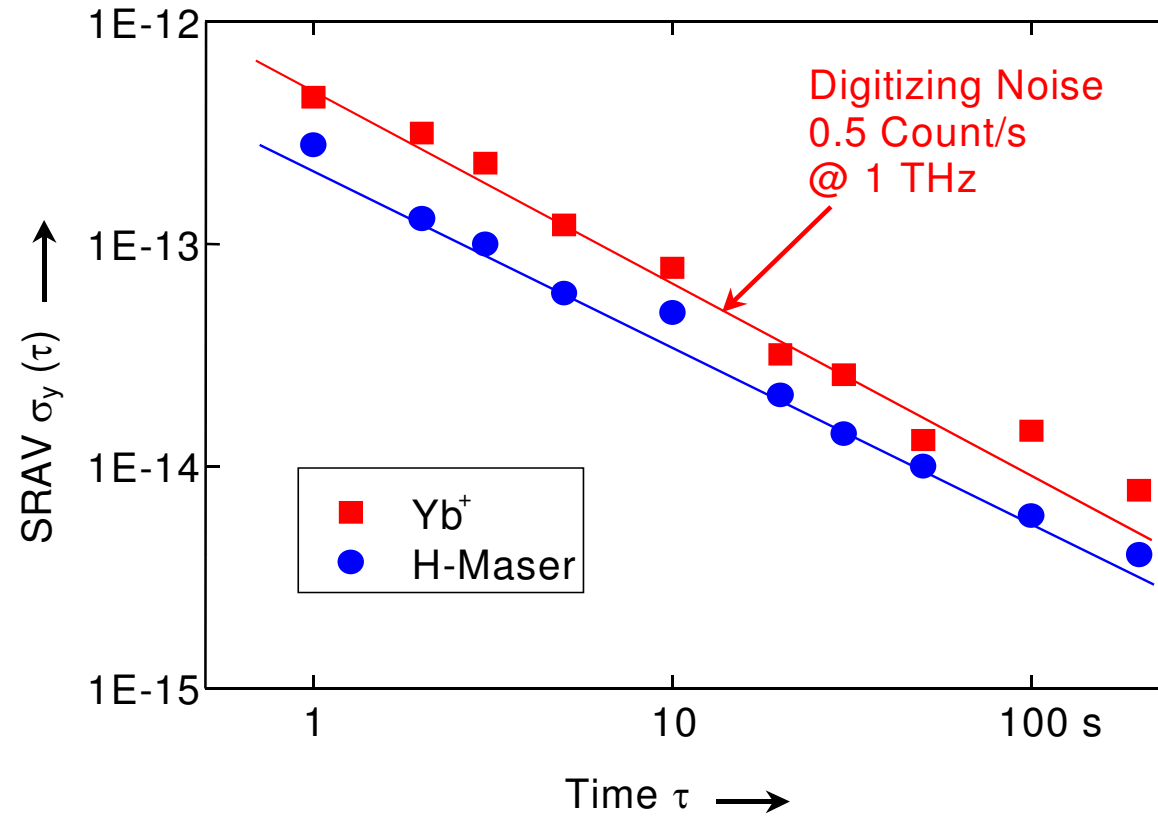
Possible noise contributions

- Counting & digitizing noise
- Servo cross conversion
- Imperfect compensation of detection residuals due to different filtering during detection process

Countermeasures

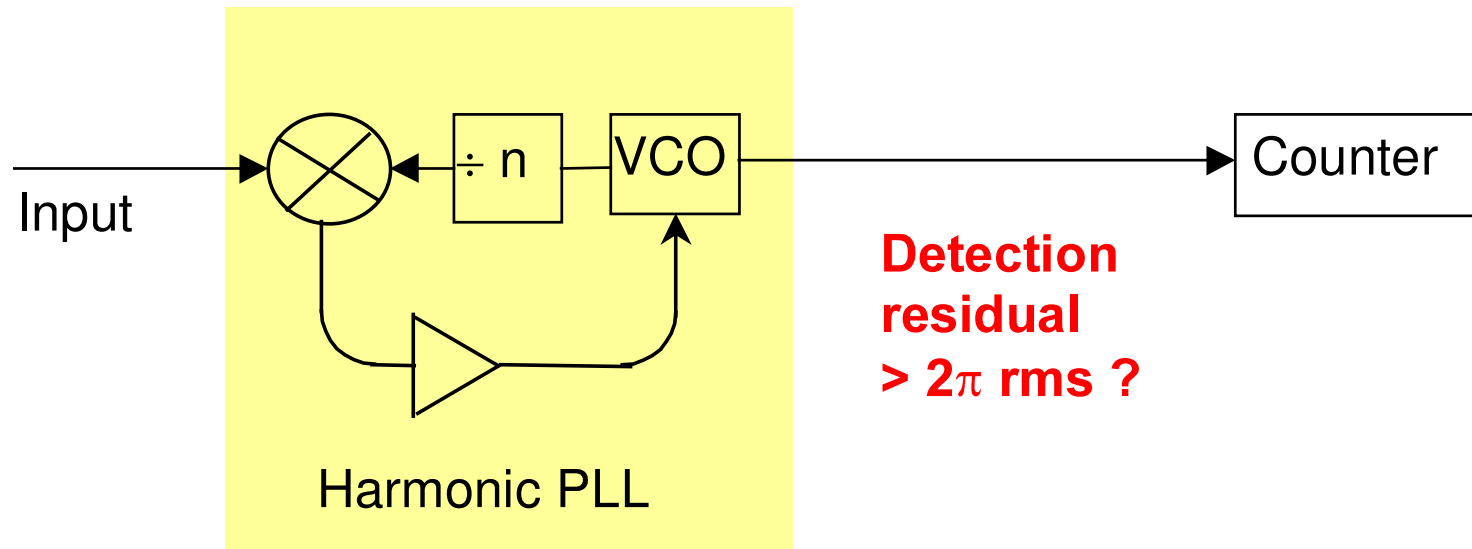
- Phase interpolation
- Totalizing frequency counters
- Broadband detection of all instantaneous phase angles with optimum post-filtering of processed signal (**transfer concept**)

Countig of REP : Digitizing noise



\Rightarrow Phase interpolation essential !

Phase interpolation by frequency multiplication



\Rightarrow Totalizing frequency counter essential !

Data processing

Possible noise contributions

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Countermeasures

- Phase interpolation
- Totalizing frequency counters
- Broadband detection of all instantaneous phase angles with optimum post-filtering of processed signal (**transfer concept**)

Detection of φ_m , φ_{CEO} , φ_{REP}

Elastic tape picture for Fourier components of phase fluctuations:

$$\varphi_m(t) = \varphi_{\text{CEO}}(t) + m \varphi_{\text{REP}}(t) + \text{const} \Rightarrow \tilde{\varphi}_m(f) = \tilde{\varphi}_{\text{CEO}}(f) + m \tilde{\varphi}_{\text{REP}}(f) + \text{const}$$

Elastic tape model in general **NOT valid for detected quantities**

$$H_m(f) \tilde{\varphi}_m(f)$$

$$H_{\text{CEO}}(f) \tilde{\varphi}_{\text{CEO}}(f)$$

$$H_{\text{REP}}(f) \tilde{\varphi}_{\text{REP}}(f)$$

H complex transfer functions $\neq 1$,
e. g. PLL loop filter, delay times
 $H_m(f) \neq H_{\text{CEO}}(f) \neq H_{\text{REP}}(f)$

Real-time data processing (transfer concept)

Example: Measurement of ν_X / f_{MW}

ν_X optical frequency

f_{MW} microwave reference

Measured quantities: $H_X X$, $H_Y Y$, $H_{CEO} \varphi_{CEO}$

$X = \varphi_X - \varphi_m$, $Y = \varphi_{REP} - \varphi_{MW}$

Real time data processing:

$$\Sigma = H_X X + H_{CEO} \varphi_{CEO} + m H_Y Y$$

Narrow-band post filtering:

$$H_X(f) = H_Y(f) = H_{CEO}(f) = 1, \text{ f small}$$

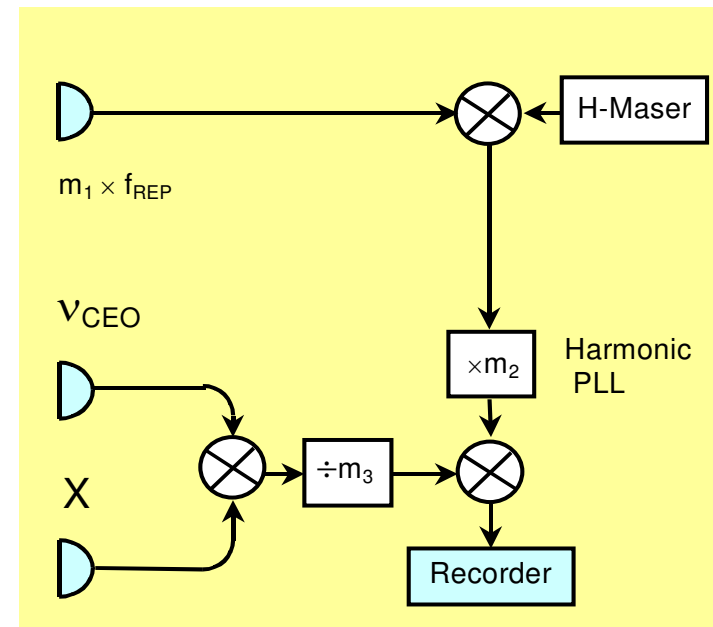
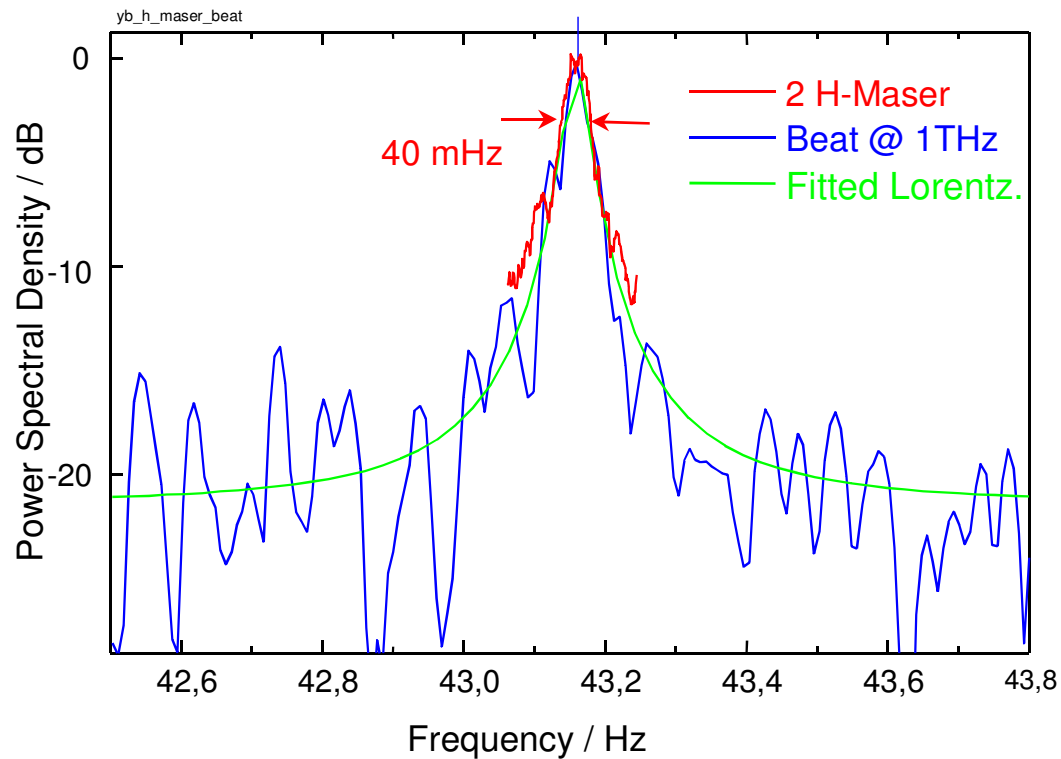
Elastic tape: $\varphi_{CEO} + m \varphi_{REP} - \varphi_m = \text{const}$

$$\Sigma = \varphi_X - m \times \varphi_{MW}$$

**\Rightarrow independent of femtocomb
detection residuals cancel out !**

Transfer between microwave and optical range

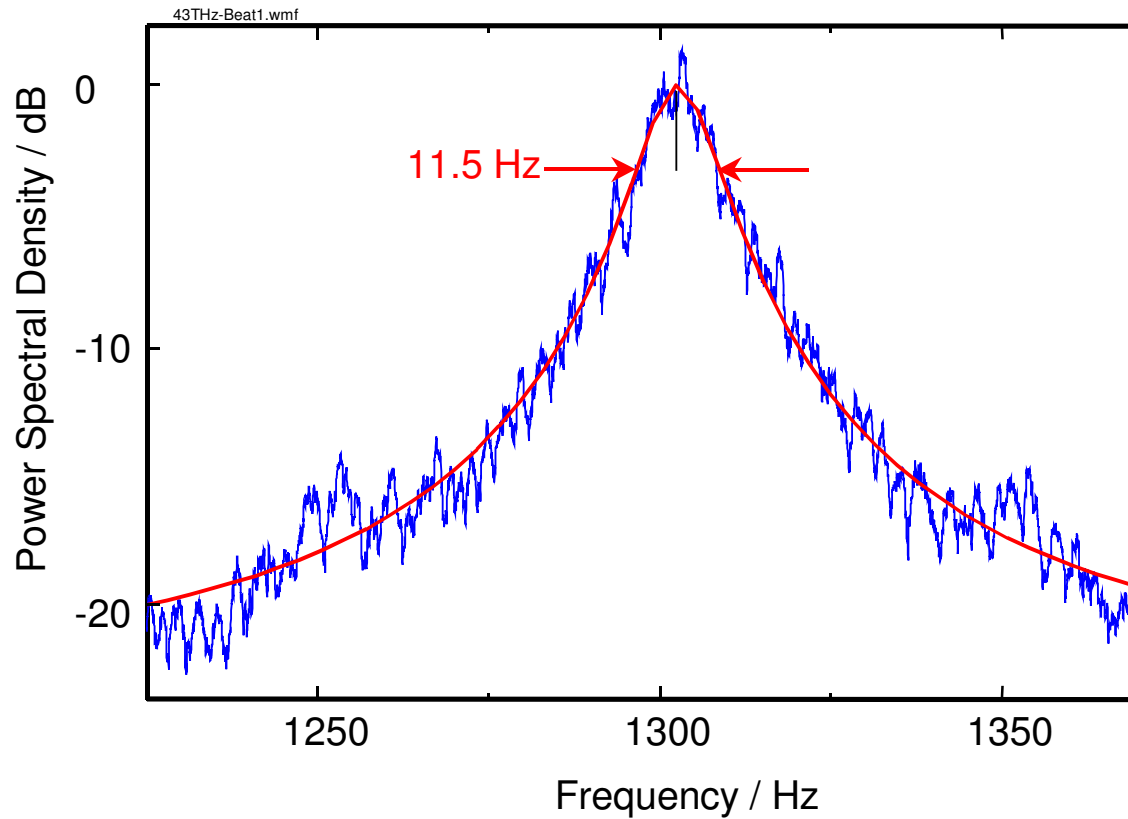
Virtual frequency: 989 GHz



Phase locking of beat: optical or MW synthesizer

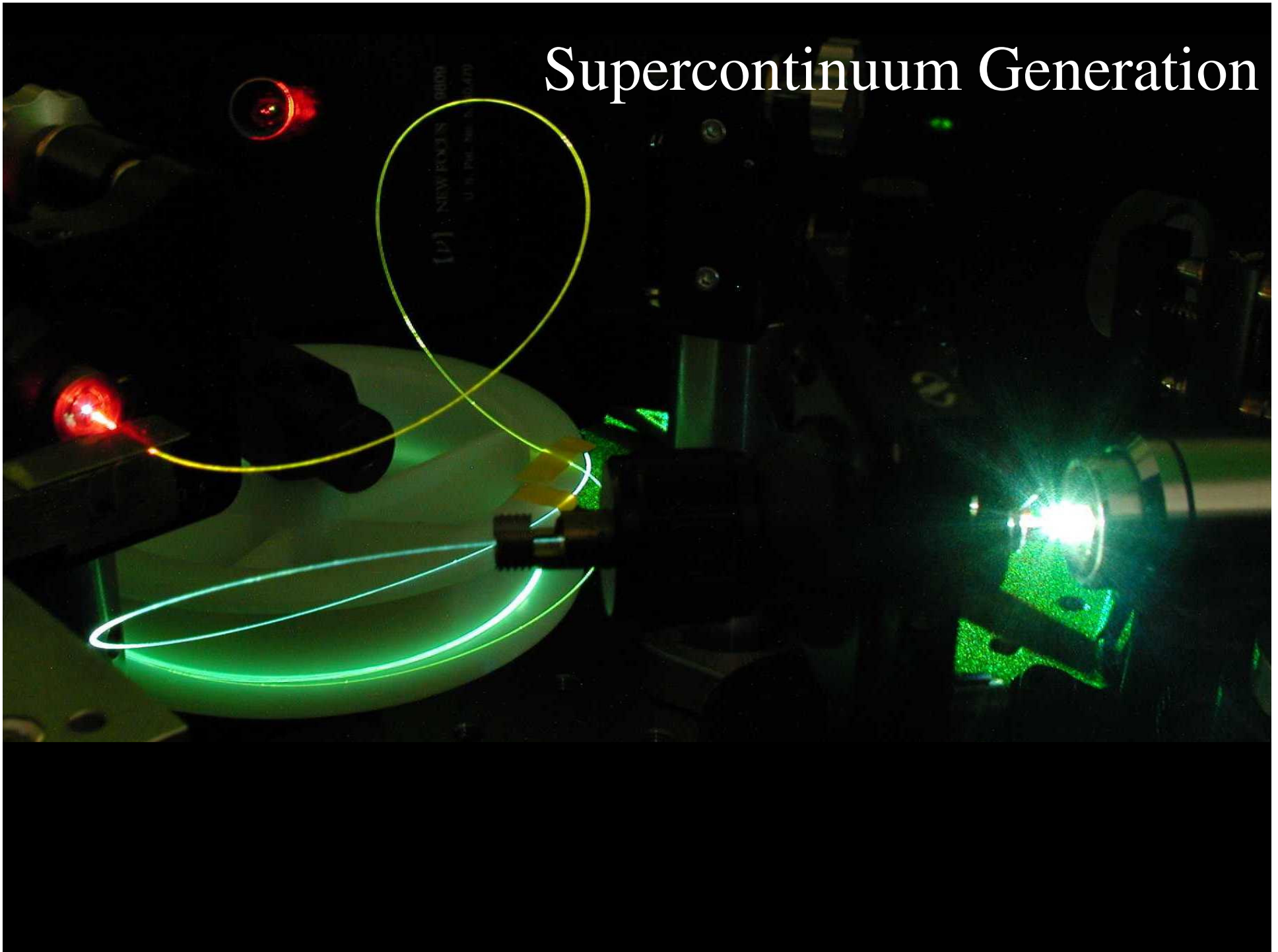
Transfer between two optical frequencies (I_2 and Yb^+ clock laser)

Virtual frequency: 43 THz



**phase-locking:
optical synthesizer**

Supercontinuum Generation

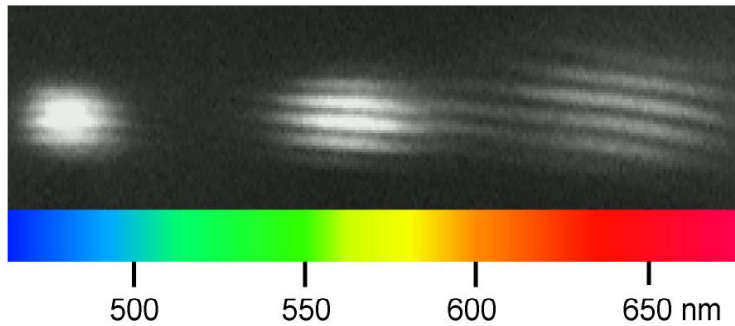


Noise in microstructure fibers

Is supercontinuum generation in MS fibers a deterministic process ?

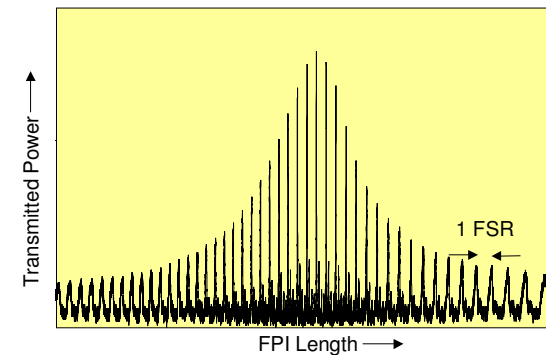
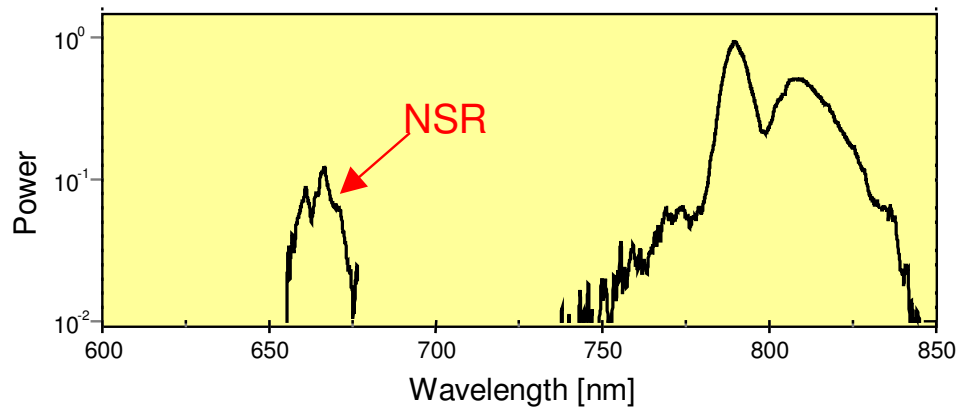
Propagation time noise due to fluctuations of pump pulse parameters ?

Is supercontinuum generation a deterministic process ?

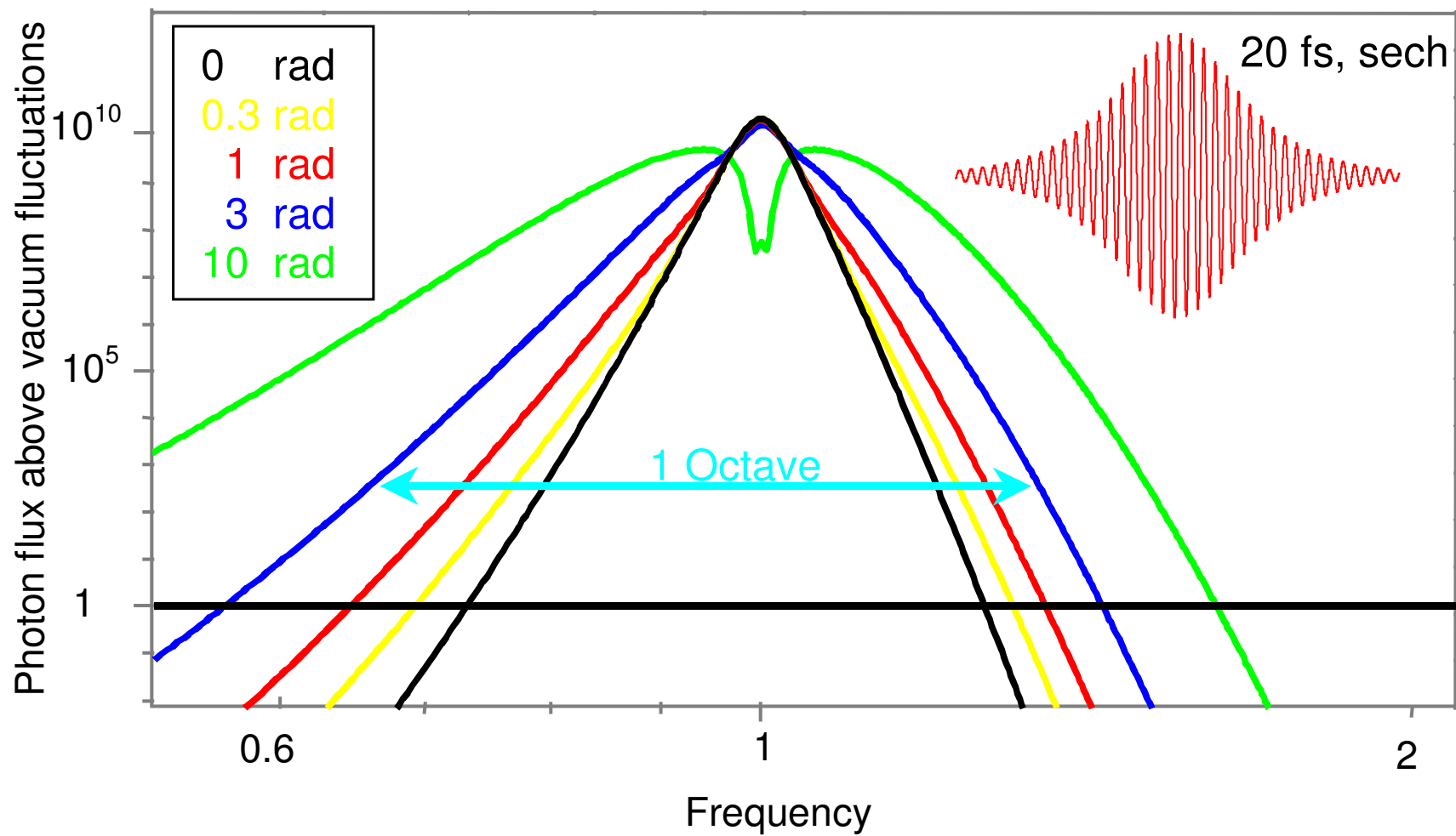


Interference of subsequent pulses

Comb spectra even for discrete spectral components (NSR)



Self-phase-modulation as seeding process



Noise of propagation time

AM $\rightarrow \Delta\tau_{\text{Prop}}$ - coefficient: 4000 rad / 100% 1)

$$\Delta P / P \approx 10^{-3} (1 \text{ s}),$$

BW 20 MHz (cavity dumper)
Shot-noise -150 dBc / Hz

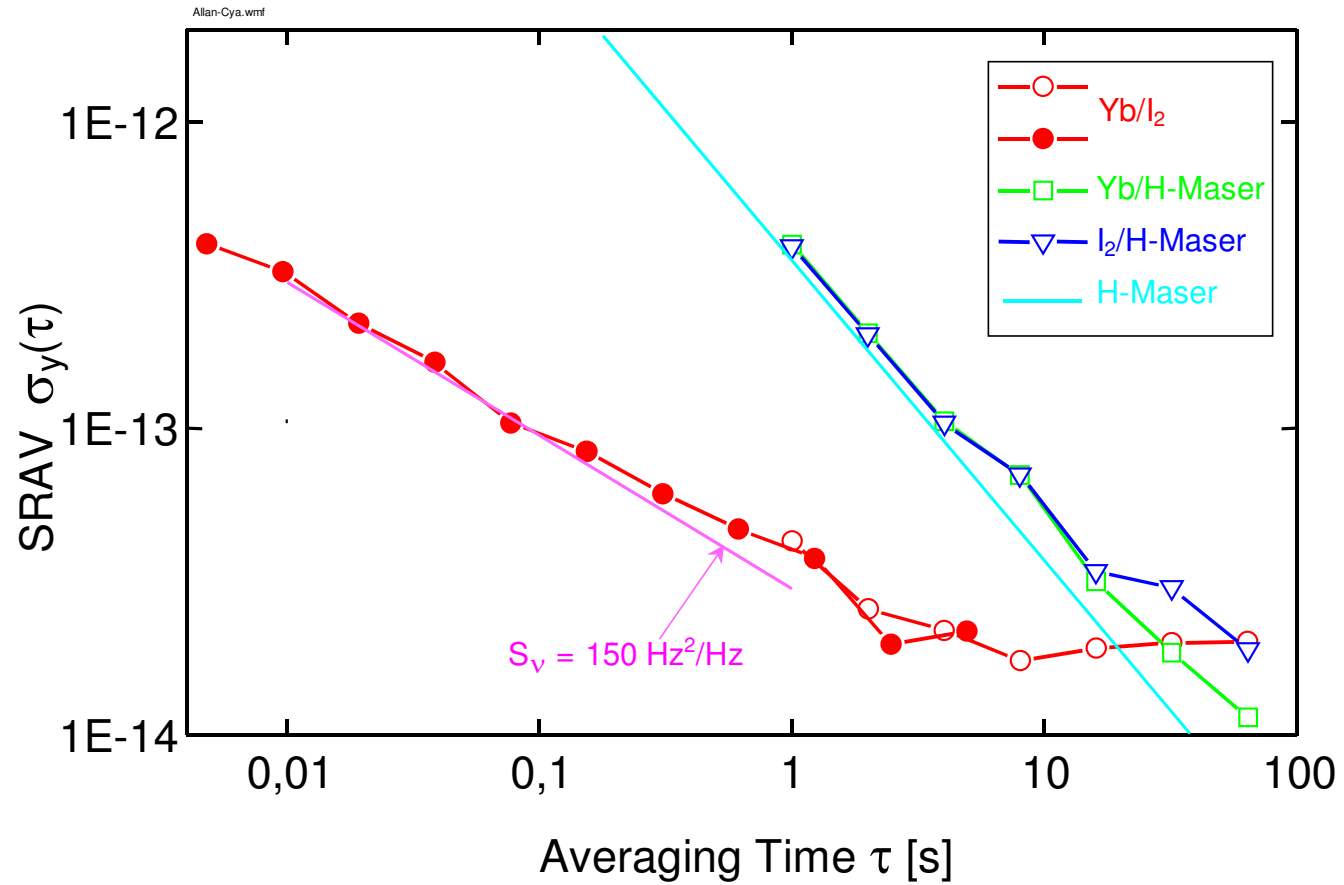
$$\Delta P / P \approx 10^{-1} (10^4 \text{ s})$$

$$\Rightarrow \sigma_y(1 \text{ s}) \approx 10^{-15}$$

$$\sigma_y(10^4 \text{ s}) \approx 10^{-17}$$

T. M. Fortier et al, Optics Lett. 27, 445 (2002)

Short-term instability



Summary / Outlook

- No cycle slipping - no principal frequency uncertainty
- Supercontinuum generation is deterministic for short pulses
- Instability $< 10^{-15}$ (1s) realistic for arbitrary frequencies
- Experiments on a 10^{-17} level feasible, e. g. alpha dot

Acknowledgement

PTB

J. Stenger, N. Haverkamp, B. Lipphardt,
G. Wilpers, H. Schnatz, Ch. Tamm, S. Weyers

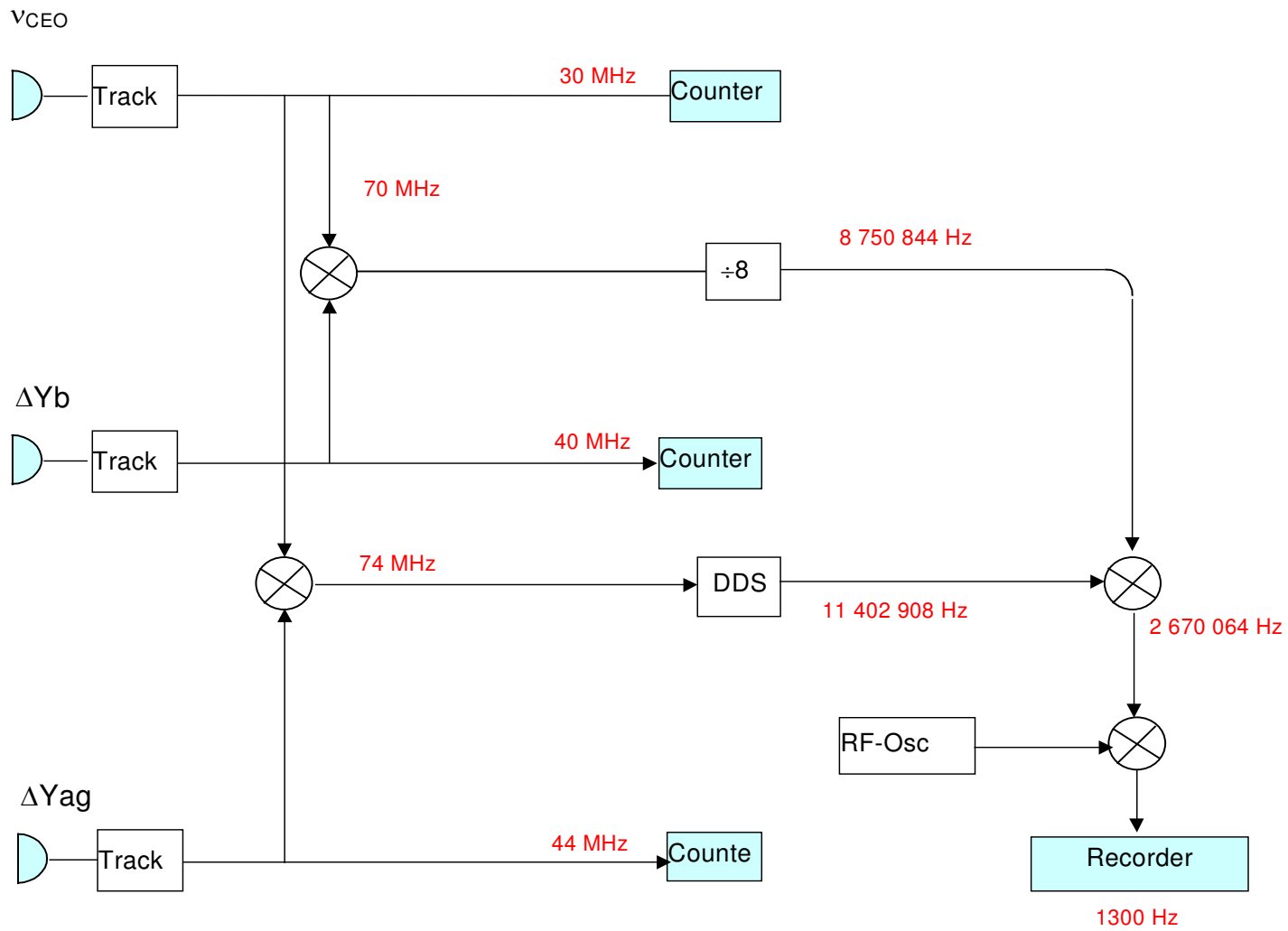
Lucent Technologies:

J.K. Ranka, R.S. Windeler, A.J. Stentz



DFG

SFB 407



H - maser linewidth vs. frequency multiplication factor

